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BLACKWATER GOLD PROJECT

EARLY WORKS EROSION AND SEDIMENT CONTROL PLAN

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ABBREVIATIONS

Artemis	Artemis Gold Inc.
Blackwater Gold Project	the Project
BMP	best management practice
BW Gold	Blackwater Gold Ltd.
CEMP	Construction Environmental Management Plan
CD	collection ditch
DD	diversion ditch
EA	Environmental Assessment
EM	Environmental Monitor
ENV	Ministry of Environment and Climate Change Strategy
ESC	Erosion and Sediment Control
ESCP	Erosion and Sediment Control Plan
FSR	Forest Service Road
IDF	inflow design flood
KP	Knight Piésold Ltd.
masl	metres above sea level
MDMER	Metal and Diamond Mining Effluent Regulations
NTUs	nephelometric turbidity units
PMP	Probable Maximum Precipitation
RIB	Rapid Infiltration Basin
RUSLE	Revised Universal Soil Loss Equation
RUSLEFAC	Revised Universal Soil Loss Equation for Applications in Canada
SCP	sediment control pond
TARP	Trigger Action Response Plan
TSF	Tailings Storage Facility
TSS	total suspended solids
USLE	Universal Soil Loss Equation

1.0 INTRODUCTION

1.1 PROJECT OVERVIEW AND PURPOSE

BW Gold Ltd. (BW Gold), a wholly owned subsidiary of Artemis Gold Inc. (Artemis), is developing the Blackwater Gold Project (the Project) located approximately 110 km southwest of Vanderhoof in central British Columbia. The Project is a large gold-silver deposit, which is proposed to be developed as a conventional truck-shovel open pit mine with a gold processing plant. Project access is via the Kluskus Forest Service Road (FSR), which joins Highway 16 west of Vanderhoof, Kluskus-Ootsa FSR and the Mine Access Road.

The Project underwent a coordinated provincial and federal environmental assessment (EA) that was initiated in 2012 and ended successfully in 2019 with the issuance of a provincial Environmental Assessment Certificate and federal Decision Statement. Condition 13 of EA Certificate #M19-01 Schedule B Table of Conditions requires that the proponent develop measures to address erosion and sediment control during construction, while Condition 29 requires the proponent to develop a plan to avoid sedimentation in waterbodies during construction and maintenance of the transmission line. BW Gold applied for a *Mines Act* Permit and *Environmental Management Act* Permit for the early works construction activities through a joint application; this application requires a description of Best Management Practices (BMPs) for the plant site sediment and erosion control structures and road works. BW Gold received *Mines Act* Permit M-246 approving the Early Works Program on June 22, 2021 and *Environmental Management Act* Permit 110602 on June 24, 2021.

This Erosion and Sediment Control Plan (ESCP) has been developed to support site preparation and grading activities proposed as part of the early work activities at the site. This plan should be read in conjunction with the Construction Environmental Management Plan (ERM, 2021) and all summary letters and design drawings prepared to support the early works activities.

1.2 OBJECTIVES AND SCOPE

This ESCP has been developed to proactively manage water, erosion, and sedimentation throughout the early works phases of the project. The ESCP adheres to the following guidance documents:

- *Technical Guidance 3 – Environmental Management Act – Developing a Mining Erosion and Sediment Control Plan* (B.C. Ministry of Environment, 2015a).
- *Technical Guidance 7 – Environmental Management Act – Assessing the Design, Size and Operation of Sedimentation Ponds Used in Mining* (Ministry of Environment, 2015b).
- *Developing Management Plans for Mines in British Columbia – Erosion and Sediment Control Plan* (B.C. Ministry of Energy, Mines and Petroleum Resources, 2020).
- *Dam Safety Guidelines 2007 (2013 Edition)* (Canadian Dam Association, 2013).
- *Revised Universal Soil Loss Equation for Application in Canada. A Handbook for Estimating Soil Loss from Water Erosion in Canada* (Wall et al., 2002).
- *Health, Safety and Reclamation Code for Mines in British Columbia* (B.C. Ministry of Energy, Mines, and Low Carbon Innovation, 2021).
- *Forest Road Engineering Guidebook* (B.C. Ministry of Forests, 2002).

The intent of this document is to outline strategies and design objectives, with appropriate flexibility, to allow the facilities to be field-fit to suit the conditions encountered during early works activities (i.e., an adaptive management approach). The ESCP describes BMPs that will be implemented prior to and during early works construction activities – it is not meant to be prescriptive. Specific measures to be implemented for each work area will be presented on detailed design drawings prepared for construction. The overall objective of the ESCP is to manage contact water within the project footprint, so as to prevent runoff from potentially impacting adjacent watercourses.

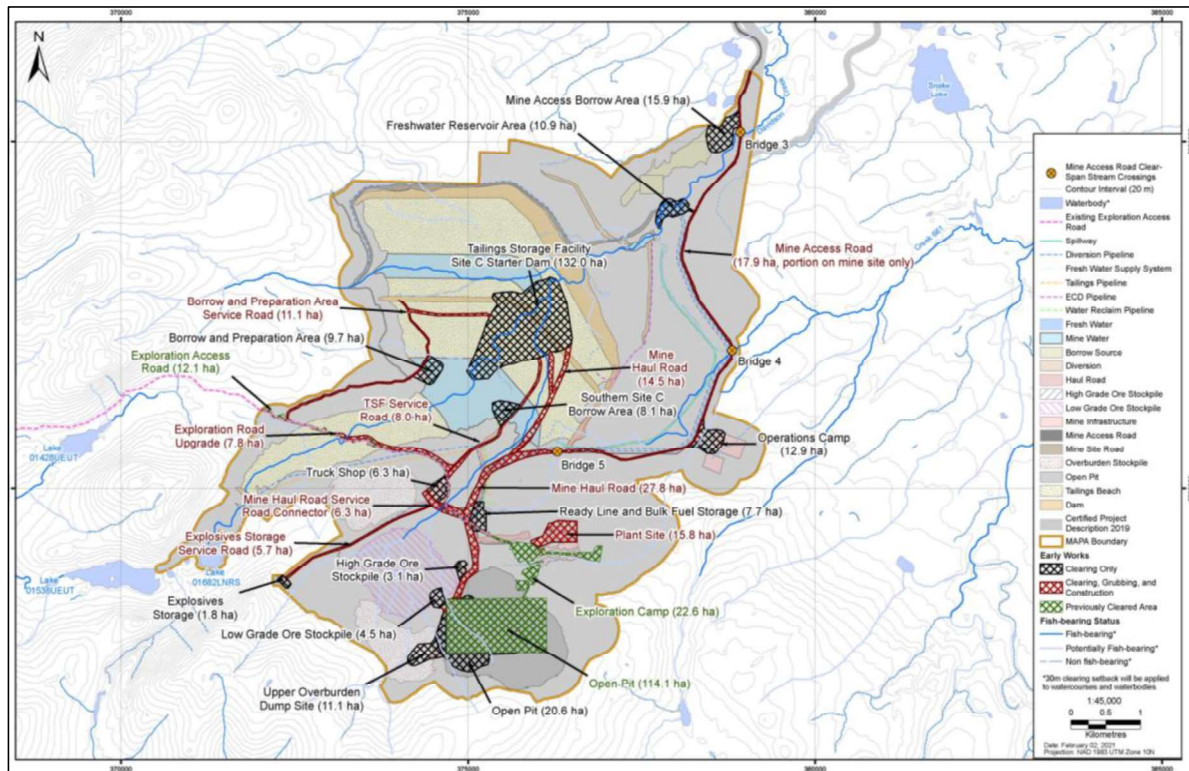
The term “contact water” is used to describe water that has come into contact with mine facilities and/or any construction disturbed areas, road runoff, borrow areas, or vegetation cleared areas. Conversely, “non-contact water” is used to describe water that has not come into contact with any project facilities or disturbed areas. Contact water during construction requires treatment for sedimentation only, which is done through BMPs.

1.3 EARLY WORKS ACTIVITIES

The Early Works activities are comprised of the following:

- Clearing, grubbing, grading, and construction of the mine access road and associated bridges
- Clearing, grubbing, grading, and construction of mine site roads
- Clearing, grubbing, ditching and sediment pond construction, site levelling, soil, and overburden removal at the Plant Site
- Tree clearing at the following locations:
 - Open Pit
 - Upper Overburden Dump Site
 - Mine Access Borrow Area
 - Southern Site-C Borrow Area
 - Tailings Storage Facility (TSF) Site C Starter Dam
 - Borrow and Preparation Area
 - Freshwater Reservoir Area
 - High Grade Ore Stockpile
 - Low Grade Ore Stockpile
 - Explosives Storage
 - Truck Shop and Mine Offices
 - Operations Camp

Early works activity areas are shown on Figure 1.1.



Note(s):

1. From ERM, 2021.

Figure 1.1 Mine Site Early Works

1.4 EARLY WORKS SCHEDULE

A high-level schedule for the Early Works activities is provided in Table 1.1.

Table 1.1 Early Works Activities Schedule

Project Activity / Milestone	Timing
Receipt of Early Works permits	Q2 2021
Construction start date	Q2 2022
Logging	Q2 2022
Construction of Mine Access Road and mine site haul roads	Q2-Q4 2022
Plant site erosion and sedimentation control works	Q2 2022
Plant Site earthworks	Commence Q2 2022

Note(s):

1. From ERM, 2021.
2. Q – quarter.

1.5 PERMIT CONDITIONS

1.5.1 MINES ACT PERMIT M-246

Section C of Permit M-246 outlines the requirements for implementation of an Environmental Management System comprised of Environmental Management Plans and Standard Operating Procedures. Section C.4 of the permit includes the following conditions related to this ESCP:

- a) *The Permittee must implement the surface water monitoring program in the Early Works Erosion and Sediment Control Plan (Document 1.5 of Permit M-246). The Permittee must track changes to surface water, seepage, and groundwater quality and quantity on the mine site. The Permittee must ensure that the program is capable of providing early warning about the onset of ARD or an increase in contaminant loading.*
- b) *The Permittee must ensure that detection limits are sufficient to compare to water quality standards and permit requirements established by the British Columbia Ministry of Environment and Climate Change Strategy (ENV).*
- c) *The Permittee must ensure that an effective QA/QC program for the surface water, groundwater and seepage monitoring programs is included and implemented as part of the Early Works Erosion and Sediment Control Plan. The Permittee must ensure that this includes detection limits, performance criteria that define acceptable levels of precision and accuracy and reporting of any missed sampling events.*
- d) *The Permittee must ensure that monitoring results of surface water, groundwater, and seepage quality and quantity are kept up to date in a dedicated database available for review by an Inspector of Mines upon request. The Permittee must ensure that water quality monitoring results, including interpretation of results, are reported and assessed in the Annual Reclamation Report. The Permittee must ensure that any significant changes or trends in water quality or quantity are discussed, and those that require additional evaluation and management are identified in the report.*

Section C.5 of the permit includes the following conditions related to this ESCP:

- a) *The Permittee must implement the Early Works Erosion and Sediment Control Plan (Document 1.5 of the permit).*
- b) *The Permittee must ensure that the Early Works Erosion and Sediment Control Plan is reviewed annually with updates reported in the Annual Reclamation Report. The Permittee must provide all substantive changes to the Chief Permitting Officer prior to implementation.*
- c) *The Permittee must ensure inspections are conducted at stream crossings, contact and non-contact water management structures and snow dumps daily during rain events and the snowmelt period on the mine site. Where excessive sediment laden runoff is observed, the Permittee must implement immediate remedial action.*
- d) *The Permittee must appropriately characterize any significant releases of sediment laden water, defined as an unauthorized discharge to the receiving environment, with respect to extent and loading, and report it to the Chief Inspector.*
- e) *The Permittee must ensure the characterization of unauthorized discharges of sediment-laden run-off must include, at a minimum, flow, total suspended solids, turbidity, pH, conductivity, temperature, dissolved oxygen, and total and dissolved metals, of both the effluent and the receiving water.*

Early works activities are outlined in Section 1.3 of this report: the activities are not anticipated to result in changes to groundwater quality and quantity or cause metal leaching or acid rock drainage. Exposed or excavated overburden material to support early works is not expected to present a risk of metal leaching or acid rock drainage, as excavations will occur at shallow depths and not in bedrock (ERM, 2021). All overburden samples collected in the area of the Plant Site, TSF, and Mine Access Road were classified as non-potentially acid generating (ERM, 2021).

The environmental monitoring program for the early works activities is described in Section 6 of this ESCP: monitoring in contact water will be restricted to turbidity and total suspended solids during the early works activities.

1.5.2 ENVIRONMENTAL MANAGEMENT ACT PERMIT 110602

Permit 110602 authorizes BW Gold to discharge treated stormwater effluent to ground from early stage construction activities from a Sediment Control Pond (SCP) through an Infiltration Basin. The Authorized Works described in the Permit are the SCP, Rapid Infiltration Basins, discharge pipes and related appurtenances. Terms and conditions of the permit include:

- Regular inspection and maintenance of the Authorized Works.
- In the event of an emergency or other condition which prevents normal operation of the Authorized Works or leads to an unauthorized discharge, remedial action must be taken immediately to restore the normal operation and to prevent any unauthorized discharges.
- Emergencies or other conditions that prevent normal operation, and remedial actions taken, must be reported immediately to the EnvironmentalCompliance@gov.bc.ca email address.
- Effluent must not be discharged from the SCP emergency overflow spillway unless there is an event greater than the 1-in-10-year storm. The permittee must notify the director within 24 hours at EnvAuthorizationsReporting@gov.bc.ca in the event that effluent is discharged from the emergency overflow spillway.
- The hydrological site investigation that is outlined in the Rapid Infiltration Conceptual Design must be completed prior to the construction of the SCP, and the Information obtained during the site investigation must be used to inform the design and land area requirements for the Rapid Infiltration Basins. Any changes to the design of the Rapid Infiltration Basins after the site investigation is completed must be submitted to the director 60 days prior to the start of construction of the Rapid Infiltration Basins.
- All aspects of the ESCP during the Early Works must be implemented, maintained, and complied with, and any modifications made to the ESCP must be submitted to the director within 30 days of the modification.
- Visual monitoring of the SCP must be conducted daily while it is discharging to the Rapid Infiltration Basins, and visual monitoring of the Rapid Infiltration Basins must be conducted daily when there is effluent in the basins.
- A Decommissioning Plan for the SCP must be developed and submitted to the director 90 days prior to the decommissioning of the pond.

2.0 ENVIRONMENTAL SETTING AND SITE CONDITIONS

2.1 EXISTING SITE CONDITIONS

The information presented in this section is from the *2020 Hydrometeorology Report* (Knight Piésold Ltd., (KP) 2021a) and the 2020 Hydrology and Water Temperature Baseline Report (KP, 2020).

2.1.1 WATERSHEDS

The Blackwater deposit lies within the upper reaches of the Davidson Creek and Creek 661 catchment areas. The terrain within these catchments is predominantly gently inclined, except along the incised portions of Davidson Creek. Davidson Creek flows northeast from the Project site towards lower Chedakuz Creek, the confluence of the two creeks is approximately 800 m downstream of Tatelkuz Lake. Creek 661 flows northeast from the Project site into upper Chedakuz Creek upstream of Tatelkuz Lake.

Chedakuz Creek drains Tatelkuz Lake and flows north-west, passing under a bridge at the Kluskus FSR approximately 2 km downstream from the lake. An unnamed catchment drains Snake Lake, which is located between the Davidson Creek and Creek 661 catchments. The Snake Lake catchment area drains directly into Tatelkuz Lake, while Creek 661 flows northeast from the Project site into Chedakuz Creek upstream of Tatelkuz Lake.

Turtle Creek, located to the north of Davidson Creek, drains another catchment running parallel to Davidson Creek towards Chedakuz Creek. Turtle Creek flows close to Davidson Creek near the base, before flowing north under the Kluskus FSR to its confluence with Chedakuz Creek downstream of the Kluskus FSR. Chedakuz Creek flows north-west from this point for approximately 25 km to the Nechako Reservoir.

Along the south-west side of the Project site, Fawnie Creek, Matthews Creek and Creek 705 all flow south-west from the deposit area. Creek 705 is a tributary of Fawnie Creek, which flows towards Laidman Lake and joins with Matthews Creek. Fawnie Creek continues to Johnny Lake, into Entiako Provincial Park, and ultimately forming a portion of the flow of the Entiako River into the Nechako Reservoir.

2.1.2 TOPOGRAPHY AND TERRAIN AND NATURAL HAZARDS

The Project is situated on the Nechako Plateau of British Columbia, part of the Interior Plateau east of the Coast Mountain Range. The area is characterized by gently undulating, northwest-trending hills cut by small to medium-sized drainages. The elevation of the Blackwater property ranges from just over 1,000 metres above sea level (masl) in low-lying areas northeast of the proposed mine site to 1,800 masl on the southwest side of the property at the summit of Mount Davidson, which is the highest peak in the Fawnie Range. The Blackwater deposit is located on the northern flanks of the mountain.

2.1.3 CLIMATE AND HYDROLOGY

2.1.3.1 MEAN ANNUAL PRECIPITATION

Two climate stations are installed in the Blackwater Project study area: Blackwater Low and Blackwater High. Blackwater Low was installed in July 2011 at an elevation of 1,050 masl and Blackwater High was installed in July 2012 at an elevation of 1,470 masl. Precipitation data from Vanderhoof were used to

develop an estimate of long-term precipitation conditions for Blackwater Low and Blackwater High. The mean annual precipitation estimates are 564 mm for Blackwater High and 489 mm for Blackwater Low.

2.1.3.2 MONTHLY PRECIPITATION DISTRIBUTION

The monthly distribution of precipitation was estimated for the purpose of water management planning. Mean monthly precipitation values range from a low of 30 mm in March to 68 mm in June for Blackwater High, and 24 mm in March to 59 mm in June for Blackwater Low (KP, 2021a). Approximately 41% of the annual precipitation at the project site falls as snow (primarily between November and March). The remaining 59% of the annual precipitation falls as rain, which may occur in any month of the year, but largely falls in the period of April to October (KP, 2021a). The monthly precipitation statistics for Blackwater High are summarized in Table 2.1.

Table 2.1 Mean Monthly Precipitation Statistics

Unit	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Total Precipitation (mm)	51	35	30	33	44	68	64	52	51	65	65	56
Rain (mm)	3	3	7	24	43	68	63	52	50	47	14	2
Ratio of Rainfall (%)	6	8	24	72	98	100	100	100	97	76	24	5
Snowfall (mm)	48	32	23	9	1	0	0	0	2	15	42	46
Ratio of Snowfall (%)	94	92	76	28	2	0	0	0	3	24	76	95

Note(s):

1. Blackwater high station.
2. From KP, 2021a.

2.1.3.3 INTENSITY-DURATION-FREQUENCY DATA

Estimates of extreme precipitation are required for a number of design aspects; the 24-hour extreme precipitation for different return period events and probable maximum precipitation (PMP) are summarized in Table 2.2.

Table 2.2 Estimated Annual Extreme Precipitation

Return Period (years)	24-Hour Extreme Rainfall (mm)	Scaling Vanderhoof (mm)
2	37	32
10	50	56
100	66	86
200	71	95
1,000	82	115
PMP	195	288

Note(s):

1. Blackwater high station. Table 2.15 from KP, 2021a.
2. Scaling Vanderhoof values recommended to be used as design values for the project.

2.1.3.4 MEAN ANNUAL RUNOFF

The annual stream hydrographs in the Blackwater Gold Project area are typically characterized by a very pronounced period of high flows during the spring freshet, followed by an extended period of steady low flows, with limited autumn storms. All creeks are affected by ice formation during the winter and the smaller systems typically freeze over for extended periods during cold snaps. Estimates of mean monthly and annual unit runoffs are summarized in Table 2.3.

Table 2.3 Mean Monthly and Annual Unit Runoff

Station	Area (km ²)	Mean Monthly Unit Discharge (L/s/km ²)												MAUD (L/s/km ²)	MAUR (mm)	MAD (L/s)
		Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec			
H1	9	0.8	0.8	1.1	5.6	24.9	8.6	3.7	1.0	1.4	2.1	2.0	1.0	4.4	139	39
H2	44	2.1	2.0	2.3	7.7	30.1	16.7	8.9	3.6	3.4	4.1	3.0	2.3	7.2	227	316
H2B	46	2.2	2.1	2.6	8.6	32.4	18.7	10.3	4.2	3.9	4.9	3.4	2.5	8.0	252	368
H4B	61	2.7	2.6	3.1	6.7	24.1	14.9	8.6	3.3	3.9	4.8	3.7	3.1	6.8	215	418
H5	593	1.7	1.6	1.9	5.6	15.3	9.7	6.0	3.3	2.2	2.4	2.3	1.9	4.5	142	2663
H6	55	2.3	2.2	2.7	3.8	11.6	9.1	3.7	3.3	2.7	3.5	3.8	2.6	4.3	135	233
H7	42	0.8	0.7	0.9	6.5	27.3	13.4	6.4	1.1	2.2	3.1	1.2	1.0	5.4	170	227
H10	7	3.2	3.1	3.6	12.0	46.3	27.0	14.2	5.4	5.1	6.2	4.6	3.5	11.2	353	79
H11	15	0.7	0.6	0.8	4.6	15.8	11.9	4.2	2.7	2.5	2.9	1.5	0.9	4.1	129	60
L1-Outlet	392	1.5	1.4	1.7	5.4	15.3	9.6	5.6	3.1	2.0	2.1	2.1	1.7	4.3	136	1687

Note(s):

1. Table 3.4 from KP, 2021a.
2. MAUD - mean annual unit discharge.
3. MAUR - mean annual unit runoff.
4. MAD -mean annual discharge.

2.1.3.5 WET MONTH RUNOFF

Wet monthly flow values were estimated for the project area on the basis of the variability of the long-term flow series developed for the H5 hydrology monitoring station. The return period ratios are shown in Table 2.4. These values were estimated by fitting statistical distribution to the monthly flow values. Generally, the greatest variability of flows occurs during the freshet period, and the lowest variability occurs during the summer months.

Table 2.4 H5 Wet Monthly Return Period Streamflow Relationships

Month	Return Period Mean Monthly Discharge (L/s)				
	Mean	Wet Return Period			
		5 Yr	10 Yr	20 Yr	50 Yr
January	1,012	1,218	1,317	1,393	1,469
February	955	1,168	1,219	1,248	1,269
March	1,145	1,322	1,563	1,845	2,300
April	3,293	4,456	6,012	7,819	10,722
May	9,044	11,627	14,523	17,682	22,411
June	5,762	7,220	9,232	11,591	15,423
July	3,531	4,290	5,567	7,156	9,916
August	1,976	2,430	3,052	3,781	4,963
September	1,298	1,590	1,986	2,448	3,194
October	1,443	1,680	2,102	2,636	3,580
November	1,374	1,522	1,916	2,458	3,513
December	1,117	1,287	1,483	1,701	2,032
Mean Annual	2,663	3,318	4,164	5,147	6,733

Note(s):

1. Table 3.5 from KP, 2021a.

3.0 RISK DETERMINATION

3.1 SURFACE PREPARATION ACTIVITIES

Construction activities that have the potential to cause erosion and sedimentation are briefly described below:

- **Clearing and Grubbing:** Clearing operations include slashing, cutting, stockpiling, and removal (or burning) of trees and brush. Grubbing operations include the removal of the tree stumps and root masses left behind during clearing operations. Grubbing operations may cause localized soil exposure in areas where roots and stumps were removed.
- **Stripping:** Stripping is the removal of the organic mat from the construction site to expose the underlying mineral soil.
- **Stockpiles:** Stockpiles may include material removed from excavations, stripping, clearing, and borrow pits. The creation of stockpiles may disturb the vegetated soil surface, and create exposed slopes.
- **Road Construction:** access roads are constructed to accommodate construction equipment on the Project site. Construction of roads may involve cut slopes, fill slopes, ditches, or culvert installation.
- **Culvert Installation:** Culverts are installed to connect drainage courses and surface drainage flow. Installation of culverts may cause flow concentrations, create cut slopes, disturb the soil surface on slope faces, and create scour zones at the culvert inlet or outlet.
- **Ditch Construction:** Where channels or ditches are constructed to direct and transport water along or transverse to the road alignment, the original drainage pattern may be altered, concentrating flows and increasing flow velocity and erosion potential. Ditch construction creates exposed slopes that can be subject to erosion.
- **Borrow Excavations:** Borrow excavations can either be landscape borrows or dugout borrows.
- **Snow clearing and storage:** snow removal from roads and construction areas may contain suspended solids, which have the potential to enter watercourses during the snowmelt period.

There are numerous potential sources of erosion and sediment transport resulting from construction activities at the site. The key areas of concern at the site include:

- Heavy rainfall events and freshet runoff can create erosion and sedimentation in areas that did not have previously known erosion.
- Heavily trafficked areas and land disturbance caused by heavy mobile equipment can be a continuous source of soil displacement and compaction. With compaction, infiltration is reduced, and surface water has a greater potential for erosion. Proper planning prior to the commencement of heavy equipment and construction work can limit the disturbed footprint and mitigate erosion potential. During unusually heavy rain events oversaturated soils can exacerbate the problem.

3.2 SOIL LOSS ESTIMATION

The Universal Soil Loss Equation (USLE) is a mathematical model developed in the 1960s by the U.S. Department of Agriculture Soil Conservation Service to predict soil erodibility (Wall et al., 2002). The USLE and its derivatives (Revised or Modified Soil Loss Equation (RUSLE or MUSLE)), are based on erosion plot and rainfall simulator experiments, primarily for crops in the Eastern United States. The Revised Universal

Soil Loss Equation for Application in Canada (RUSLEFAC) was developed to specifically reflect Canadian conditions (Wall et al., 2002).

General conditions such as climate, soil, topography, vegetation, and land use practices affect erosion (Wall et al., 2002). The USLE or RUSLE equation to estimate the potential, long-term, average annual soil loss per hectare is (Wischmeier and Smith, 1978, presented in Wall et al. 2002):

$$A = R \times K \times L \times S \times C \times P$$

Where:

A = potential, long-term, average annual soil loss per hectare [tonnes/ha/year]

R = rainfall factor [MJ•mm/ha/hr]

K = soil erodibility factor [tonnes•hr/MJ/mm]

L = slope length factor [dimensionless]

S = slope steepness factor [dimensionless]

C = cropping-management factor [dimensionless]

P = support practice factor [dimensionless]

The potential soil loss calculated for each worksite/area will be compared to guidelines for assessing potential soil erosion classes summarized in Table 3.1 (Wall at al., 2002). The suggested soil loss tolerance in Canada is 6 tonnes/ha/year.

Table 3.1 RUSLEFAC - Soil Loss Classes

Soil Erosion Class	Potential Soil Loss [tonnes/ha/year]
1 - Very Low	<6
2 - Low	6 – 11
3 - Moderate	11 – 22
4 - High	22 – 33
5 - Severe	>33

Note(s):

1. Table 1.1 from Wall et al. (2002).

The potential for surface erosion during the early works within the plant site was estimated using RUSLEFAC as 17 tonnes/ha/year, corresponding to a moderate soil erosion class.

4.0 EROSION AND SEDIMENT CONTROL MEASURES

4.1 EROSION MANAGEMENT AND SEDIMENT CONTROL STRATEGIES

The key strategy to control erosion and sedimentation is to protect the soil surface from rain and runoff (water management) and to capture eroded soil on site. These will be addressed through:

- Documentation of baseline conditions and erosion risk potential.
- Minimizing the extent and duration of exposure through planning and scheduling of erosion and sediment control (ESC) measure selection, installation, inspection, repair/modification, and decommissioning for every part of the construction schedule.
- Prioritizing drainage control, then erosion control, then sediment control - protecting areas to be disturbed from runoff by intercepting runoff and diverting it away from disturbed areas and keeping runoff velocities low.
- Retaining sediment on site by planning the location where sediment deposition will occur and constructing containment systems before other land-disturbance occurs.
- ESC performance monitoring and routine inspection of ESC measures, documentation of inspections, and prompt response to problems (maintenance and replacement of ESC measures as needed).
- Permanent site stabilization and decommissioning of ESC measures.

Erosion control should be viewed as the primary means in preventing the degradation of downstream aquatic resources, while sediment control should be viewed as a contingency plan. A greater emphasis will be placed on erosion control measures, especially in areas of elevated erosion potential; however, measures to address both erosion control and sediment control are required. Erosion control measures prevent exposed soils from being entrained by water or wind, while sediment controls address the removal of sediment suspended in water once erosion has occurred. Erosion and sediment control measures applied in series create a resilient system capable of protecting the natural environment from sediment impacts.

This ESCP describes design elements and provides guidance for control of all water originating from, or brought into, the mine site area during construction. Water will be controlled in a manner that minimizes erosion in areas disturbed by early works construction activities and prevents the release of untreated construction water, which could adversely affect the water quality of receiving waters.

Water management in the early stages of construction will focus on diverting non-contact water away from working areas, retention of the understory vegetation (brush and root networks) as much as possible during winter logging, and interception of contact water using BMPs. Disturbed areas will be seeded using quick establishing, weed-free seed mixes (native and approved non-native) for initial soil stabilization followed by planting of native vegetation in accordance with Reclamation and Closure practices to facilitate progressive closure and reclamation of the project where final slopes are created.

Erosion management and sediment control at the project will be a process of establishing diversion and collection ditches to manage surface water runoff, constructing the SCP, stabilizing disturbed land surfaces to minimize erosion, establishing temporary vegetation cover, and reclaiming the final slopes in accordance with the Reclamation and Closure Plan.

Potential effects from the construction activities in the absence of planned mitigation measures include:

- Increased surface erosion from disturbed and rehabilitated areas
- Increased sediment load entering the natural water system
- Siltation or erosion of watercourses and water bodies

The ESCP addresses these potential hazards for effective management of surface water and contact runoff during the early stages of construction. Sediment mobilization and erosion will be minimized by:

- Limiting the extent of land disturbance to the practical minimum.
- Scheduling activities to retain understory vegetation (brush and root networks) to the extent practicable during logging and removal of trees, until the transition to major works construction.
- Reducing water velocities across the ground using surface roughening and re-contouring, particularly on exposed surfaces and in areas where water concentrates.
- Progressively rehabilitating disturbed land and constructing drainage controls to improve stability of rehabilitated land.
- Protecting natural drainages and watercourses by working outside of riparian areas, or in conformance to management plans or BMPs within riparian management areas, if approved, and constructing appropriate sediment control devices.
- Installing rock riprap, rock channel lining, sediment filters, or other suitable measures on steep gradients.
- Restricting access to rehabilitated areas.
- Constructing appropriate temporary BMP measures (e.g., silt fences, hay bales) downslope of disturbed sites where more permanent sediment control measures are not appropriate, or in combination with more permanent measures.
- Implementing soil bioengineering techniques to contain sediment and enable disturbed surfaces to recover.
- Snow pile placement and management: proper siting of snow storage areas e.g., snow dumps will not be on disturbed, un-stabilized, or highly erodible sites, within waterbodies or riparian areas, or at a highpoint where runoff is likely to collect sediment and other pollutants as it melts.

The type of erosion or sediment control measure will be selected based on site-specific conditions such as:

- Site erosion potential classification
- Area of upstream soil exposure
- Terrain conditions and space constraints
- Construction method
- Anticipated concentrated rainfall amounts due to ditching or drainage pattern changes
- Level of risk to the receiving environment

4.2 PROCEDURAL CONTROLS

A work schedule that coordinates the timing of land-disturbing activities and the installation of ESC measures can be a cost-effective way to help reduce erosion risk. Runoff-control measures and diversions should be installed up-gradient of areas to be disturbed prior to grading. Principal sediment basins and traps, as needed, should be installed before any major site grading takes place, and additional sediment traps and sediment fences should be erected as grading takes place to keep sediment contained on-site at

appropriate locations. In steeper terrains, where construction of sediment basins may not be feasible, a combination of silt retention structures and filter bags may be employed, or diversion ditches may redirect flows to an area of flatter terrain where a sediment basin may be implemented.

4.3 PLANT SITE SEDIMENT CONTROL POND AND RAPID INFILTRATION BASINS

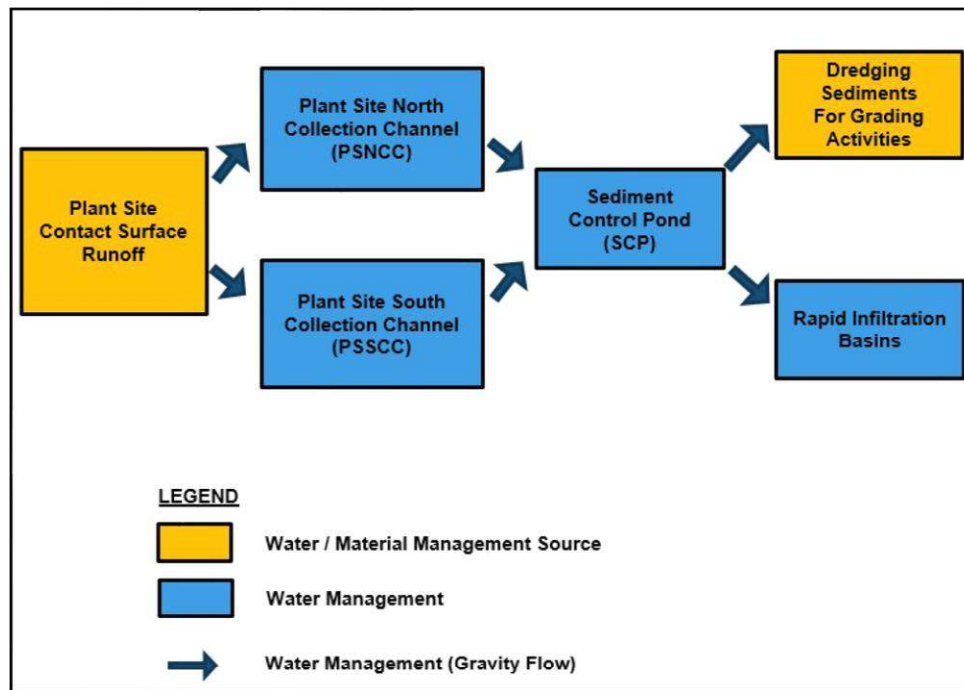
Currently the only SCP required for the Early Works Activities is for the Plant Site. Details on the SCP design and erosion control measures can be found in the *Surface Water Management and Sediment Control Design Report for the Plant Site Early Works* (KP, 2021b) and *Rapid Infiltration Concept for the Plant Site Sediment Collection Pond Discharge* (KP, 2021c). The Plant Site geotechnical site characterization report and the early works engineering work plan are included in Appendix A and Appendix B, respectively, of this report (KP, 2022a, 2022b).

The SCP is designed following the BC Ministry of Environment guidance document on size and operation of sediment ponds (ENV, 2015b). The pond will accommodate a live storage equal to the 1 in 10 year 24-hour storm event, with at least a half meter (0.5 m) of freeboard. The pond spillway has sufficient flow capacity to convey a flood event from a 1 in 200 year 24-hour storm event without overtopping.

The Plant Site North and South Collection Channels will collect surface contact runoff from the proposed Plant Site soil disturbance area. These channels will be located near the perimeter of the planned fill placement areas and will convey runoff into the SCP located at the northeast corner of the proposed disturbance area. Runoff occurring within the excavations will be conveyed to the perimeter collection channels. The SCP is designed to provide adequate residence time for sediment to settle out of suspension prior to water discharging into a Rapid Infiltration Basin (RIB) system downstream. From the RIBs, the surface contact runoff is expected to percolate and dissipate into the soil layer to avoid any overland flow into the forested area. A simplified water management plan schematic is presented on Figure 4.1.

A test pit site investigation program was completed by KP in November 2021 to characterize the subgrade material at the Plant Site Collection Channels, SCP, and RIBs (KP, 2022b). A total of 22 test pits were excavated at the Plant Site area, including four test pits at the SCP and Collection Channels and three test pits at the RIBs. The subgrade material was described according to soil type, size and shape of clasts, gradation, plasticity, colour, odour, compactness/consistency, soil structure, and moisture condition.

Infiltration testing was completed in the ablation till material in two test pits at the northern plant site RIB area: the test pit infiltration tests show an average infiltration rate of 0.004 m/hr for TP21-70 and 0.04 m/hr for TP21-71, which corresponds to an estimated annual hydraulic loading of 35 m/year and 336 m/year for TP21-70 and TP21-71, respectively (KP, 2022a). The materials encountered in the two test pits were similar, and the variability in results may be due to differences in material underlying the test pits (KP, 2022a).



Note(s):

1. From KP, 2021b

Figure 4.1 Water Management Schematic – Early Works

The RIB design incorporates an average annual hydraulic loading rate of approximately 88 m/year, which was based on the results of previous investigations at the site (KP, 2022b). The infiltration tests completed in 2021 indicate that local variability could be expected to influence operational performance of the RIBs. No changes to RIB land area requirements were recommended based on the results of the 2021 site investigation (KP, 2022b). The SCP outlet works will incorporate sufficient flow isolation and control components to manage hydraulic loading to the individual RIBs. Larger scale infiltration testing will be incorporated in the initial performance monitoring of the constructed RIBs, and the results will be considered in the operations, maintenance, and surveillance plans for the Plant Site SCP and RIBs.

The RIBs will be visually assessed during operation to determine if they are performing as designed. As infiltration performance may vary within each RIB, the amount of flow directed into each basin will be adjusted with the entry valves as required to maximize efficiency. If the infiltration rate is lower than expected during operations, additional contingency measures will be implemented, which may include:

- Pumping excess flow to an adjacent RIB if enough capacity exists.
- Construction of additional RIBs downgradient of the existing basins: connection valves will be placed to facilitate the implementation of additional RIBs if required.

The use of RIBs may require seasonal or annual removal of accumulated deposits or sediment on the basins to allow proper infiltration. The collected sediment will be deposited on the plant site pad within the secondary containment of perimeter collection channels where BMP will be applied. To avoid bonded ice surface forming at the bottom of the RIBs, and to facilitate infiltration during winter conditions, the construction of a ridge and furrow system may be implemented at the bottom of the RIBs.

A decommissioning plan for the Plant Site SCP will be developed and submitted to the director 90 days prior to the decommissioning of the pond. The plan will include:

- The pump out procedure for the effluent that cannot be discharged through the primary outlet.
- The sediment dewatering procedure.
- The decommissioning of the ponds, ditches, liners and outlets.

It is anticipated that the Plant Site SCP will be utilized during the construction and operations phases, with discharge pumped to the TSF during operations.

4.4 BEST MANAGEMENT PRACTICES

Installation of temporary erosion and sediment control features or BMPs will be the first step towards controlling erosion and sedimentation during construction. All temporary ESC features will require maintenance and inspection after each significant rainfall. These temporary features will be reclaimed after achieving soil and sediment stabilization.

BMPs reduce erosion potential by stabilizing exposed soil or reducing surface runoff flow velocity. Generally, two types of erosion control BMPs are used:

- Source control BMPs for protection of exposed surfaces
- Conveyance BMPs for control of runoff

Procedural BMPs are planning strategies that will be used and include:

- Scheduling of work
- Minimizing exposed soils wherever possible
- Maximizing work during favourable weather
- Preserving and using existing drainage systems wherever possible
- Installing BMPs early

Typical BMPs are described in this section.

4.4.1 CULVERTS

Culverts will be constructed along access and haul road alignments to allow for flow of water and drainage channels beneath the road. Culverts will be combined with Check Dams and Collection Ditches to pass surface runoff beneath the roads. Spacing of culverts along haul road alignments is dependent on both the grade and skew of the road, and the erosion hazard level.

4.4.2 DIVERSION DITCHES

Diversion ditches (DD) will be constructed upgradient of disturbed areas to intercept clean surface water runoff and convey it around areas to be disturbed to avoid excessive sheet flow. All diversion ditches will discharge through a stabilized outlet designed to handle the expected runoff velocities and volumes from the ditch without scouring. Each diversion ditch type will provide a minimum freeboard of 0.5 m between the top of flow and the ditch crest.

Two types of diversion ditches may be required: Type 1 (DD1) ditch in soil and Type 2 (DD2) ditch in rock. Whether ditch cross section type DD1 or DD2 is built will depend on site conditions during construction. Dimensions for the two types of diversion ditches are presented in Table 4.1.

Table 4.1 Diversion Ditch Dimensions

Dimension	DD1	DD2
Bottom width (mm)	500	500
Side slopes	2H:1V	0.5H:1V
Minimum Depth (mm)	500	500
Riprap thickness (mm)	300	-

Note(s):

1. V-shaped diversion ditches may also be constructed; design criteria will be provided in design reports and drawings.
2. If riprap is unavailable, a bituminous geomembrane or HDPE liner will be considered.

Type 1 Diversion Ditches (DD1) will require filter fabric to be placed along the base and sides of the ditch prior to placement of riprap. Fabric is placed continuously to maintain intimate contact with the base soil. Fabric is installed so that upstream strips overlap downstream strips by a minimum of 500 mm. Riprap (if available in sufficient quantity) will be placed so as to form a dense, uniform, well-graded mass with few voids, and some hand placement may be necessary to obtain good size distribution. As an alternative to riprap, the diversion ditches may be lined with a bituminous geomembrane or HDPE liner, or check dams will be used along with a monitoring, surveillance, and contingency program.

Diversion ditches will be inspected and maintained regularly and before and after major precipitation events to remove any blockages to flow (accumulated sediment, debris, etc.) that may reduce the design capacity. Typical diversion ditch designs are shown on Drawing C3803.

4.4.3 COLLECTION DITCHES

A runoff collection ditch (CD) intercepts contact water runoff from disturbed areas and diverts it to a stabilized area where it can be effectively managed. Collection ditches are used within construction areas to collect runoff and convey it to appropriate sediment control measures. Where fine grained soils are exposed, appropriate erosion protection materials will be installed based on the estimated magnitude of flow and the flow velocity. General locations and conditions may include:

- Below disturbed slopes to divert sediment-laden water to control facilities.
- At or near the perimeter of the construction area to prevent sediment-laden runoff from leaving the site.
- Below disturbed areas to prevent erosion if stabilization measures cannot be implemented immediately.

Collection ditches may be either temporary or permanent structures. Two types of collection ditches may be required: Type 1 (CD1) ditch in soil and Type 2 (CD2) ditch in rock. Whether ditch cross section type CD1 or CD2 is built will depend on site conditions. Dimension for the two types of collection ditches are presented in Table 4.2. Each collection ditch type will provide a minimum freeboard of 0.5 m between the top of flow and the ditch crest.

Table 4.2 Collection Ditch Dimensions

Dimensions	CD1	CD2
Bottom width (mm)	500	500
Side slopes	2H:1V	0.5H:1V
Minimum Depth (mm)	500	500
Riprap thickness (mm)	300	-

Note(s):

1. V-shaped collection ditches may also be constructed; design criteria will be provided in design reports and drawings.
2. If riprap is unavailable, a bituminous geomembrane or HDPE liner will be considered.

Type 1 Collection Ditches (CD1) will require filter fabric to be placed along the base and sides of the ditch prior to placement of riprap. Fabric is placed continuously to maintain intimate contact with the base soil. Fabric will be installed so that upstream strips overlap downstream strips by a minimum of 500 mm. Riprap (if available in sufficient quantity) will be placed so as to form a dense, uniform, well-graded mass with few voids, and some hand placement may be necessary to obtain good size distribution. As an alternative to riprap, the collection ditches may be lined with a bituminous geomembrane or HDPE liner, or check dams will be used along with a monitoring, surveillance, and contingency program.

Collection ditches will be inspected and maintained regularly and before and after major precipitation events to remove any blockages to flow (accumulated sediment, debris, etc.) that may reduce the design capacity. Typical collection ditch designs are shown on Drawing C3803.

4.4.4 ROCK CHECK DAMS

Rock check dams are small dams constructed across swales, drainage ditches, and waterways to avoid erosion by reducing flow velocity. Rock check dams accomplish this by interrupting the flow of water to form small ponds, thereby flattening the surface of the water, and reducing the velocity of flow (Government of Alberta, 2011). The obstructions induce infiltration and reduce erosion potential. Check dams are also used to distribute flows across a swale to avoid preferential paths and guide flows towards vegetation.

Rock check dams along the centreline of Collection or Diversion Ditches should form an asymmetrical triangle with the bottom of the ditch. Dam slopes of 3H:1V downstream and 2H:1V upstream will be used. The rock check dams will be spaced such that top of the middle of each downstream check dam is at the same elevation as the base of the previous dam - dam spacing and rock size will be determined by the supervising Engineer based on hydraulic conditions and gradient (Toronto and Region Conservation Authority, 2019). Rock check dams will be installed on all ditches exceeding 6.0% grade. Rock check dam construction will start from the downstream end of the ditch and be constructed upstream from that point. A minimum 100 mm deep trench must be excavated for the entire footprint of the Rock check dam, and spoiled material must be removed from the site.

Rock check dams require regular maintenance and should be inspected regularly, and before and after significant storm event (for the purpose of this plan, a significant storm event is equal to or greater than a 1 in 2 year return period precipitation event) It is important that rubble, litter, and leaves are removed from the upstream side of the dam. This is typically done when the sediment has reached a height of one-half of the original height of the dam.

4.4.5 STRAW BALE CHECK DAMS

Straw bale check dams are small, temporary dams constructed of straw bales as drop structures placed across channels to reduce a steep grade to intervals of flatter grades. Straw bale check dams are used for (Government of Alberta, 2011):

- Small open channels that drain ≤ 2 ha
- Channels with grade of $< 5\%$
- Flow velocities of < 0.3 m/s

Straw bale check dams should only be a maximum of one straw bale in height, or 0.5 m maximum. Straw bales should be machine-made; weed free cereal crop straw such as wheat, oats, rye, or barley; tightly compacted and bound with two rows of wire or synthetic string; and show no signs of weathering and be no more than year old (Government of Alberta, 2011).

Structures will be inspected at weekly intervals and after each significant rainfall event. Damaged, decayed, or dislodged straw bales will be replaced immediately and erosion repairs will be made to prevent failure of the structure. Sediment build up will be removed before it reaches one-half the check structure height. Typical configurations for a straw bale check dam are shown on Drawings C3801.

4.4.6 ENERGY DISSIPATERS

Energy dissipaters are pools used to dissipate the energy of fast flowing water and control erosion at the outlet of a ditch or a conduit to minimize erosion of natural stream channels downstream. The energy dissipator will be set at zero grade and aligned straight with the direction of flow at the outlet, and constructed flush with the surrounding grade.

These structures are used in conjunction with diversion of non-contact water around construction areas and with diversion ditches and are typically located upstream of a receiving water body (e.g., stream, pond, lake, etc.). Drawings will be provided in the early works activities design reports.

4.4.7 SEDIMENT BASINS

A sediment basin is a temporary structure that is used to detain runoff from small drainage areas where so that sediment can settle out. The basin is typically maintained until the site is permanently protected against erosion by vegetation and/or structures. Sediment basins are generally located in areas where access can be maintained for sediment removal and proper disposal. Sediment basins are typically constructed at the end of collection ditches to detain sediment-laden runoff long enough to allow the majority of the sediment to settle out to comply with water quality objectives. A sediment basin can be created by excavating a basin, utilizing an existing depression, or constructing a dam on a slight slope downward from the work area. Sediment-laden runoff from the disturbed site is conveyed to the basin via ditches, slope drains, or diversion structures. The efficacy of sediment basins is largely dictated by the extent to which they are properly sized and constructed as designed; whether the banks are stabilized immediately following construction; and the extent to which they are regularly cleaned out / maintained.

The size of the temporary sediment basins is dependent on the size of the drainage areas. The exact locations and final geometry of each basin will be field-fit to minimize disturbance. The supervising Engineer will approve the sizing and location of these basins for the early works activities prior to construction. Three sizes of sediment basin (designated SB1, SB2, and SB3) are used for different size drainage areas, as

summarized in Table 4.3. The width and length dimensions correspond to the top of the wet storage area, at the base of the outlet structure.

Table 4.3 Recommended Configuration of Sediment Basins

Specification	SB1	SB2	SB3
Drainage Area (hectares)	<0.5	0.5 - 1	1 - 2
Length (m)	15	25	50
Width (m)	3	5	10
Depth of Wet Storage Excavation (m)	1	1	1
Embankment Height of Rock Outlet (m)	0.5	1	1
Minimum Spillway Weir Length (m)	1	2	3

Note(s):

1. From ENV, 2015b.

Sediment basins will be inspected regularly and cleaned out when the sediment has accumulated to one-half of the designed wet storage volume. Upland areas contributing to the trap/basin will be stabilized as quickly as possible to avoid frequent dredging and maintenance. The outlet will be checked regularly for sediment build-up that could prevent drainage and limit the overall carrying capacity of the basin. If the outlet is clogged by sediment, it will be cleaned or replaced. The dredged sediment will be disposed of in fill areas, soil stockpiles, designated waste areas, or other locations where it can be stabilized with vegetation or contained via sediment controls (e.g., silt fencing and hay bales).

Dredging will occur during low flow periods to minimize re-suspension of sediments. A typical configuration for a sediment basin is shown on Drawing C3803.

The requirement for sediment basins is not currently anticipated for the early works activities. BW Gold will apply to ENV for a discharge permit including the location of any proposed effluent discharge in the event that sediment basins will be utilized during the early works activities.

4.4.8 SLOPE DRAINS

Slope drains consist of flexible tubing or conduit and are required to convey concentrated runoff from the top to the bottom of a cut or fill slope into the appropriate BMP when ditches are deemed impractical (i.e., at steep ditch gradients, or unfavourable side slopes for ditch construction). Additionally, slope drains may be used in conjunction with rock check dams at the inlet to reduce velocities and to drain collection ditches into stabilized outlets. The entrance section to the drains will be well-entrenched and stable so that surface water can enter freely, and the drain will extend downslope beyond the toe of the slope to a stable area. The minimum slope drain diameter will be sized according to the contributing drainage area summarized in Table 4.4.

Slope drains will be inspected and maintained regularly, and any blocked or damaged parts will be cleaned, repaired, or removed and replaced. Sediment will be removed from the upslope inflow area, particularly before and after storm events, to prevent downslope sediment transport, which may cause plugging of the drainpipe and overtopping of the structure. The dredged sediment will be disposed of in fill areas, soil stockpiles, or other locations where it can be stabilized with vegetation or contained via sediment controls (e.g., silt fencing and hay bales). Dredging (if and when required) will occur during low flow periods to minimize re-suspension of sediments.

Table 4.4 Recommended Slope Drain Sizing

Drainage Area (Hectare)	Pipe Diameter (mm)
0.2	300
0.6	450
1.0	530
1.4	600
2.0	900

Note(s):

1. From government of Alberta, 2011.

4.4.9 SURFACE ROUGHENING

Cut and fill slopes will be roughened with tracked machinery where appropriate to reduce runoff velocity and erosion, increase infiltration, and aid in the establishment of vegetative cover with seeding. The roughening will be carried out by a tracked machine moving up and down the slope surfaces to create grooves perpendicular to the slope, creating undulations on the soil surface, as shown on Drawing C3801. This procedure is simple, inexpensive, and provides immediate short-term erosion control for bare soil where vegetative cover is not yet established, as a rough soil surface provides more favorable moisture conditions which will aid in seed germination compared to hard, compacted smooth surfaces.

4.4.10 FILTER BAGS

Filter bags are generally constructed from a sturdy non-woven geotextile capable of capturing particles larger than 150 microns. Filter bags will be installed at the discharge end of pumped diversion pipelines, via fabric flange fittings, to remove fine grained materials before discharging to the environment, as needed. Filter bags are generally temporary sediment control measures. Filter bags are installed on flat, stable, non-erodible foundations, or in well vegetated areas. The pumping rate is specified by the manufacturer. Discharge from filter bags is routed to avoid erosion.

A smaller variety of filter bags, referred to as filter socks, can be installed on the discharge ends of gravity flow pipes, such as slope drains, to filter silt particles before discharging to the environment. Filter bags will be inspected daily for defects, rips, tears, sediment accumulation, and erosion of the surrounding area. When sediment fills one-half of the volume of the filter bag, the filter bag will be removed from service and replaced. Spare bags will be kept nearby to minimize time required to recommence pumping activities. Once the used bag is fully drained, the bag and its contents will be disposed of in fill areas, soil stockpiles, or designated waste areas, as the material is inert and can be used for reclamation. A typical filter bag plan and cross section is provided on Drawing C3802.

4.4.11 WATERBARS

Waterbars, shown on Drawing C3802, are ridges or ridges and channels constructed diagonally across a sloping road or right-of-way at pre-designed intervals to limit the accumulation of erosive volumes of water. Waterbars reduce sheet flow and surface erosion of areas of exposed soil and/or roads by diverting runoff towards a stable vegetated area or diversion ditch. Spacing of waterbars will be field-fit based on slope grade, general erodibility of the surface, and anticipated flows. Waterbars will not direct runoff into a ditch

that channels water toward a watercourse unless the ditch is adequately designed with check dams and armouring where appropriate.

The height (measured from the channel bottom to the top of the ridge) will be a minimum of 0.45 m, the base width of the ridge will be 1.8 m minimum, and the side slopes will be 3:1 or flatter where vehicles cross. The crossing angle will be selected to provide a positive grade less than 2%.

The approximate spacing of waterbars is summarized in Table 4.5 and will be field-fit to locate the outlet in stable natural areas, where possible. Waterbars will be periodically inspected and sediment will be removed from the flow and outlet areas as needed.

Table 4.5 Recommended Waterbar Spacing

Grade (%)	Waterbar Interval (m)
< 5	35
5 – 10	30
10 – 20	20
20 – 35	15
>35	7.5

Notes:

1. From North Carolina Department of Environment and Natural Resources, 2013.

4.4.12 DIVERSION STRUCTURES

A temporary diversion structure consists of sandbags stacked in a pyramid formation with a polyethylene sheet placed diagonally in between as shown on Drawing C3802. Temporary diversion structures are useful for diverting streams and/or concentrated overland flows to an appropriate sediment basin or other BMP where it can be effectively managed. No temporary diversion structures are proposed during the early works stage that would require authorization under the *Water Sustainability Act*.

4.4.13 SILT RETENTION STRUCTURES

Silt fences are temporary sediment control devices used to protect water quality in nearby watercourses from sediment present in stormwater runoff, by forcing low volumes of overland flow to pool, allowing sediment to settle out of suspension. Silt fences are typically installed downslope of erosion-susceptible terrain to prevent sediment-laden sheet flow from entering receiving waters. Typical sites are catch points beyond the toe of fill, or on side slopes above waterways or drainage channels. Intercepted drainage pools along the uphill side of the fence to promote sediment settling. Silt fences will also be installed and maintained along down-gradient boundaries of all snow dumps. Drainage in contact with the fence is filtered through geotextile: the small pores of the silt fence filter coarse particles (fine sand to coarse silt) and restrict water exfiltration rates. Barrier locations are field-fit based on-site features and conditions (e.g., soil types, climate, terrain features, sensitive areas, etc.), design plans, existing and anticipated drainage courses, and other available ESC measures.

Silt fencing will be trenched according to Drawing C3801 for proper anchoring. The design criteria for silt fences includes:

- The size of the drainage area shall be no greater than 0.1 ha per 30 m length of fence
- Maximum flow path length above the silt fence should be no greater than 30 m

- Maximum slope gradient above the silt fence should be no greater than 2H:1V

Silt fences will be inspected for damages, tears, clogging, or erosion of the surrounding areas. Damaged sections will be repaired or replaced to maintain their functionality.

An alternative to a silt fence is a sediment retention berm, which is a small (approximately 600 mm high) berm that is constructed using random fill material (rock, wood chips, soil, topsoil). Sediment retention berms do not require removal of the underlying vegetation; however, voids along the base of the berm must be minimized.

4.4.14 TEMPORARY SEEDING

Exposed slopes and other disturbed areas will be seeded for initial soil stabilization using weed-free, quick establishing seed mixes (native and approved non-native). The purpose of temporary seeding is to stabilize the soil and reduce damage from wind and/or water until permanent stabilization is accomplished. Seeding is applicable to areas that are exposed and subject to erosion for more than 30 days, and is usually accompanied by surface preparation, fertilizer, and mulch; however, the timing of seeding is weather and season dependent and consequently this method is not applicable at all times. Temporary seeding may be accomplished by hand or mechanical methods, or by hydraulic application (hydroseeding), which incorporates seed, water, fertilizer, and mulch into a homogeneous mixture (slurry) that is sprayed onto the soil.

4.4.15 MULCHING

Mulching is the application of a uniform protective layer of straw, wood fibre, wood chips, or other acceptable material on or incorporated into the soil surface of a seeded area to allow for the immediate protection of the seed bed. The purpose of mulching is to protect the soil surface from the forces of raindrop impact and overland flow, foster the growth of vegetation, increase infiltration, reduce evaporation, insulate the soil, and suppress weed growth. Mulching also helps to hold fertilizer, seed, and topsoil in place in the presence of wind, rain, and runoff, and reduces the need for watering. Mulching may be utilized in areas that have been seeded either for temporary or permanent cover.

There are two basic types of mulches: organic mulches and chemical mulches. Organic mulches likely to be used include straw, hay, wood fibre, wood chips, and bark chips. This type of mulch is usually spread by hand or by machine (mulch blower) after seed, water, and fertilizer have been applied. Chemical mulches, also known as soil binders or tackifiers, are composed of a variety of synthetic materials. Chemical mulches are usually mixed with organic mulches as a tacking agent to aid in the stabilization process, and are not typically used as the sole control, except in cases where temporary dust and erosion control is required. The choice of materials for mulching will be based on soil conditions, season, type of vegetation, and the size of the area.

4.4.16 ROLLED EROSION CONTROL PRODUCT

Rolled erosion control products such as blankets, nets, and matting, are manufactured or fabricated into rolls designed to reduce soil erosion and assist in the growth, establishment, and protection of vegetation. Nets are made of high tensile material woven into an open net which overlays mulch materials. Blankets are made of interlocking fibres, typically held together by a biodegradable or photodegradable netting; blankets generally have lower tensile strength than nets but cover the ground more completely. Rolled

erosion control products will be used when mulch cannot be adequately tacked and where immediate ground cover is required to prevent erosion damage and will be used to aid permanent vegetated stabilization of slopes 2:1 or greater.

An alternative to the high tensile material woven blanket is a hemp fibre erosion control blanket comprised of fibres that are 100% biodegradable and created without the use of polypropylene netting. The hemp fibre blankets can be used for slope protection (for slopes up to 1H:1V) and on culvert inlets and outlets.

The rolled erosion control products will be monitored and repaired as necessary until ground cover is established. Products will be inspected weekly at a minimum and before and after each significant rainfall event.

4.4.17 POLYETHYLENE COVER

Polyethylene sheets can be used to temporarily cover newly exposed soil in situations when time does not permit other more permanent solutions to be applied. Soil that has high erosion potential will be covered immediately if a precipitation event is forecast. Strips of polyethylene should overlap each other in a configuration that prevents water from running underneath adjacent sheets. Runoff should be directed into an appropriate non-erodible or armoured drainage channel.

4.4.18 FLOCCULANTS

Flocculants are commercial products used to increase the rate of sedimentation in a SCP by increasing aggregation of fine sediments. Flocculants can be used to enhance removal of suspended sediment, particularly in situations where the sediment-laden water cannot be detained long enough to allow particles to settle (i.e., when water is being discharged from the emergency overflow spillway when there is an event greater than the 1-in-10 year storm, when turbidity levels are high and adequate detention times cannot be provided). Flocculants used will be:

- Harmless to fish, aquatic organisms, wildlife, and plants
- Biodegradable
- Legal for use in Canada and be accompanied with a Safety Data Sheet containing toxicity information confirming that the product is not toxic to aquatic life

Flocculants will only be used after all appropriate physical BMPs have been implemented. If flocculants will be used, the written manufacturer's instructions describing correct use of the product (e.g., dosage and settling time recommendations), site preparation, application, inspection, maintenance, and storage, will be followed.

The site Environmental Manager or Environmental Monitor will monitor water quality and flocculant dosage, and will notify the ENV within 24 hours [at EnvAuthorizationsReporting@gov.bc.ca](mailto:EnvAuthorizationsReporting@gov.bc.ca) in the event that effluent is discharged from the emergency overflow spillway, in accordance with Section 3.1 of Permit 110602. ENV will also be notified within 24 hours if flocculant is used in the SCP.

5.0 PLAN IMPLEMENTATION

5.1 ROLES AND RESPONSIBILITIES

Roles and Responsibilities for the Construction activities are presented in the Project Construction Environmental Management Plan (CEMP) being prepared by ERM (2021). This information is summarized in Table 5.1.

Table 5.1 Early Works Activities Roles and Responsibilities

Role	Responsibilities
Project Sponsor	<ul style="list-style-type: none"> Overall Early Works environmental management and performance.
Project Manager/ Field Manager	<ul style="list-style-type: none"> Oversees CEMP updates, communications, and implementation. Maintains compliance with permit and approvals. Authorizes Stop Work authority to project personnel (e.g., environmental monitor(s) as per permits and approvals). Notifies regulatory agencies or authorizes notification of environmental non-compliance or environmental incidences. Provides onsite staff, including contractors, with the appropriate equipment and sufficient supplies, including spill kits and plans, emergency contact lists, Environmental Monitor(s), clean/appropriate machinery etc., that meet requirements specified in permits and the CEMP. Reduces the potential for incidents on site by regularly monitoring the implementation of mitigation measures listed in permits and the CEMP. Implements corrective actions, where non-compliances are identified, or incidents occur. Confirms that onsite staff, including contractors, are trained for their job. Reviews site environmental monitoring report(s), including incidents, daily/weekly, and final report. Submits environmental monitoring reports to regulatory bodies.
Environmental Monitor (EM)	<ul style="list-style-type: none"> Reports to the Project Manager on status of work and any environmental issues. Communicates CEMP requirements to the Project Manager, and onsite workers, including contractors. Completes or confirms completion of environmental orientation with onsite workers. Provides corrective action advice to onsite staff and the Project Manager, where appropriate. Has the authority to issue a Stop Work Order where activities are impacting, or may impact, water/sediment quality, fish/fish habitat, migratory birds, waterfowl, and other species. Maintains records of site visits and non-compliances and environmental incidents. Prepares weekly summary reports and the Completion Report. Consults with other qualified professionals when implementing mitigation hierarchies (for example archaeology, raptors, adjusting timing windows).
Construction Personnel / Subcontractors	<ul style="list-style-type: none"> Constructs works in accordance with approved engineering designs, permits and all relevant management plans. Knows and supports BW Gold's environmental and health and safety requirements. Notifies the Project Manager or Environmental Manager of any observed or potential non-compliances with permits and approvals. Immediately reports incidents to the Project Manager or Environmental Manager and initiating an appropriate response. Adheres to Stop Work Order. Corrects deficiencies and any non-compliances upon direction from Project Manager or Environmental Manager.

The project owner/sponsor holds ultimate responsibility for ensuring that the ESCP is implemented. Water management will be planned and designed by the engineering design team, comprised of professional engineers registered in good standing with the Engineers and Geoscientists British Columbia. Roles and responsibilities with respect to ESC are described in Table 5.2.

Table 5.2 Erosion and Sediment Control Roles and Responsibilities

Role	Responsibilities
Project Sponsor	<ul style="list-style-type: none"> Delegates responsibility to hired professionals (engineers, contractors, inspectors, etc.) who design, install, inspect, monitor, and decommission BMPs. Obtain applicable permits and approvals. Communicate with stakeholders and regulatory agencies, as required. Liaise with Project Engineer, Project Manager, Contractors and EMs in relation to compliance with the ESCP to prepare reports in accordance with permitting requirements.
Project Engineer	<ul style="list-style-type: none"> Develop a site wide water management plan showing the general arrangement of non-contact and contact water diversion ditches and sediment ponds. Determine permits/approvals required and applies for them on behalf of the Project Sponsor. Provide guidance on erosion and sediment control measures in accordance with established policies and best practices guidance. Review the design and implementation of ESC measures (as specified by the EM) as it relates to on-going construction work. Develop specifications and typical drawings for other water collection and conveyance structures (e.g., ditches, sumps) and stamps Issued for Construction drawings. Review the effectiveness of implemented mitigation measures in consultation with the EM. Review and approve on-site design modifications, communicates changes to appropriate approval agencies where required, and updates plans accordingly. Develops contingency plans for certain stages or activities as needed.
Environmental Monitor (EM)	<ul style="list-style-type: none"> Be a Certified Professional in Erosion and Sediment Control. Specify erosion and sediment control measures, their sizing, and placement on site, and designs measures in accordance with established policies and best practices guidelines. Prescribe field-fit erosion and sediment control measures. Supervise the implementation of the ESC measures and document the completion of the ESCP and any field fit changes to the original work plan if they were required. Conduct ongoing monitoring inspections to verify the effectiveness of the ESC measures and/or the need for additional works or contingency measures and monitor flow and water quality in the outlet of the Plant Site SCP, and infiltration in the discharge area. Report to the Project Sponsor on the compliance of the construction activities with the environmental requirements during construction. Temporarily halt work on identification of a non-compliant activity that has the potential to result in the release of a deleterious substance to a receiving waterbody. A formal Stop Work Order will be issued only if other forms of communication fail to resolve the problem, or if urgent attention needs to be focussed on resolving the problem. Recommend corrective measures to be taken to correct the non-compliant activity.
Construction Personnel / Subcontractors	<ul style="list-style-type: none"> Install/construct measures based on approved plans and according to design specifications. Ensure that their workers are appropriately trained, supervised, and have the necessary experience and competency to implement the requirements of the ESCP. Provide input on construction-related aspects of ESCP implementation including labour, equipment and materials requirements, construction procedures and field constraints. Inform the Project Sponsor and the Project Engineer if the conditions of the environment or construction practices change materially from that as anticipated under this ESCP and suggests ESC design modifications if needed. Undertake corrective and preventative measures in response to non-conformances with the ESCP and ensure that such measures are implemented in a timely manner. Corrects deficiencies and any non-compliances upon direction from Project Manager or Environmental Manager.

5.2 COMMUNICATION/TRAINING STRATEGY

All staff and subcontractors responsible for the management, implementation, monitoring, and reporting of erosion and sediment control measures will be experienced and will receive training specific to their roles in this plan prior to the commencement of their work.

5.3 ONSITE INSPECTION AND PLAN REVIEW

The success of the ESCP is dependent on monitoring of implemented BMPs. The Construction Personnel/Sub-Contractors and Environmental Monitor will inspect all erosion control measures periodically and after each significant runoff-producing rainfall event. For the purpose of this plan, a significant rainfall event will be considered as equal to or greater than the 1 in 2 year return period rainfall. Silt fences, sediment traps/basins, ditches, culverts, and SCP will be visually inspected for the following:

- Excess sediment build-up
- Structural/physical integrity
- Anticipated wear and tear

Sediment removal and proper disposal will be performed as required.

Once the ESC measures have been installed, their effectiveness will be monitored by the Environmental Monitor, and maintenance will be carried out, as necessary. All ESC measures and stream crossings, contact and non-contact water management structures, and snow dumps will be inspected by the Construction Personnel/Sub-Contractors and/or Environmental Monitor during and after significant rainstorms and during the snowmelt period during early works activities.

Immediate action will be taken by the Construction Personnel/Sub-Contractors when the need for maintenance or repair of ESC measures is identified for the ongoing performance of the measures. Monitoring will include but not be limited to the following:

- New erosion control prescriptions will be developed as needed based on encountered or anticipated erosion of disturbed soils, slopes, and ditches. Initial erosion will be inspected visually by searching for light surface material (litter or soil) movement, while sedimentation resulting from erosion will be determined by searching for deposition of soil particles at the bottom of slopes and depressions. Rilling, gullying, pedestalling, and unusual compaction are also indicators of erosion and will be recorded if and when observed.
- Sediment accumulation in ditches, check dams, and sumps will be identified, and maintenance actions will be recommended where needed.
- The physical integrity and stability of sediment pond components, including berms, outlet pipes, spillways, and downstream discharge channels.
- Sediment levels in the SCP will be measured monthly or prior to a predicted storm event to ensure that the minimum pond depth below the outlet pipe invert is present; sediment captured in traps will be removed in a timely manner.
- Revegetated areas will be monitored for evidence of wind and water erosion; remedial seeding and erosion-control measures will be applied when required.

The Environmental Monitor and Project Engineer will modify the ESCP when necessary, to reflect changing site conditions or new information which has been identified during construction. Any revisions to the ESCP will be communicated to ENV within 30 days. This plan, as a component of the Environmental Management System, will be reviewed annually, with any updates reported in the Annual Reclamation Report, in accordance with Condition C.1 (b) of Permit M-246. All substantive changes will be provided to the Chief Permitting Officer prior to implementation, in accordance with Condition C.5 (b) of Permit M-246.

BW Gold will conduct visual monitoring of the SCP daily while discharging to the RIBs and will conduct visual monitoring of the RIBs daily when there is effluent in the basins. Visual monitoring will include

monitoring for adequate infiltration, seepage, overland flow, and erosion in the area outside the SCP and RIBs. Daily inspections will be recorded and maintained on site for three years and will be made available to ENV staff upon request.

5.4 CONTINGENCY STRATEGIES AND RESPONSE

The design of erosion and sediment control measures should be viewed as a flexible process that responds to new information that is obtained throughout the construction phase. Contingency strategies for the Project will be active and adaptive, with ongoing inspection, maintenance, and re-evaluation for all BMP control measures and surrounding site conditions. If monitoring identifies that BMPs are not functioning adequately, the following steps will be taken:

- Confirm control measure/feature installed correctly
- Assess appropriate size or length/depth of control method with site circumstances
- Determine if alternate BMP/control method or contingency measures are required
- Assess if increased maintenance/inspections required

An inventory of ESC materials will be kept on site to address problems that may arise. The inventory list will be updated regularly to reflect a more accurate estimate of the quantities that should be stocked on site. The materials will provide a spectrum of measures to address a broad range of site conditions and severity.

5.5 CONSTRUCTION SEQUENCING

Construction activities will be performed in sequence to minimize the area of exposed soils. The Contractor will establish all ESC measures during the initial stages of construction to minimize sediment loading to natural watercourses. The planned order of early works construction activities is as follows:

1. Install ESC measures as shown on detail design drawings
2. Clear and strip work areas as required and link directly all ESC measures associated with each construction stage and area
3. Provide temporary erosion control measures for cut slopes
4. Construct Early Works components to design lines and grades shown on final Issued for Construction Drawings
5. Provide temporary erosion control measures for fill slopes
6. Complete final stabilization and seeding of disturbed surfaces and slopes
7. Reclaim temporary ESC measures

6.0 ENVIRONMENTAL MONITORING AND REPORTING

6.1 ON-GOING ENVIRONMENTAL MONITORING

BW Gold will continue to monitor surface water and groundwater quality as part of the baseline monitoring program that was implemented in 2011. The baseline monitoring program will transition into the surface water and groundwater program outlined in Appendix 9-E of the Joint Mines Act /Environmental Management Act Permits Application during construction and operation to meet the requirements of Section C.4 of permit M-246. The construction and operation water management and monitoring plan is designed to provide an early detection system and identify trends in surface water and groundwater quality so that potential impacts to the receiving environment can be investigated, mitigated, and avoided.

6.2 TRIGGER ACTION RESPONSE PLAN

6.2.1 SCHEDULED MONITORING

For this Early Works ESCP, a Trigger Action Response Plan (TARP) will be implemented for works in and around water, specifically clearing, grubbing, grading, and construction of the mine access road and associated bridges and mine site roads. Trigger-Response Plans are developed to plan appropriate actions used in response to observed changes in environmental conditions that are approaching or exceeding management objectives (ENV, 2019).

A performance-based approach will be used to assess the effectiveness of the ESCP. Effectiveness will be determined by the extent to which certain performance metrics – or targets – are being achieved. A receiving water target applies downstream of the construction site, in the water body to which the site drains. The key elements of a TARP (Ministry of Environment and Climate Change Strategy, 2019) are:

- Trigger: Identification of a clear threshold (location, water quality characteristic, level, frequency, duration)
- Action: Description of clear and time bound actions to be taken in response to a trigger being approached or exceeded
- Response: Clear process for determining and confirming if a trigger has been exceeded, a process for reporting the trigger exceedance; and a response that must be implemented

TSS is the parameter typically measured to assess effectiveness of ESC measures; determination of TSS requires collection of a water quality sample and analysis at an accredited laboratory. Water turbidity is often measured and used as a proxy for TSS, since *in situ* turbidity can be measured onsite with a handheld turbidity meter (in nephelometric turbidity units (NTUs)). The federal water quality guidelines for turbidity are extrapolated from the suspended sediment guidelines of a 25 mg/L and 5 mg/L change from background for short-term and long-term exposures, respectively, according to the suspended sediment and the general turbidity correlation of 3 to 1 (Canadian Council of Ministers of the Environment, 2002).

Because duration of exposure to elevated TSS and turbidity is a key factor in assessing aquatic impacts, as shown in Table 6.1, targets for construction runoff and downstream receivers will be an induced change in turbidity levels, in order to implement any needed corrective measures in a timely manner.

Table 6.1 Maximum Allowable Increase of TSS and Turbidity

Parameter	Background		
	Clear waters (TSS <25 mg/L Turbidity <8-NTU)	Turbid waters (TSS 25-100 mg/L Turbidity 8-50 NTU)	Turbid waters (TSS >100 mg/L Turbidity >50 NTU)
Total Suspended Solids (TSS)	<ul style="list-style-type: none"> Change from background of 25 mg/L at any one time for a duration of 24 hours Change from background of 5 mg/L at any one time for a duration of 30 days 	<ul style="list-style-type: none"> Change of background of 10 mg/L at any time 	<ul style="list-style-type: none"> Change from background of 10%
Turbidity	<ul style="list-style-type: none"> Change from background of 8 NTU at any one time for a duration of 24 hours Change from background of 2 NTU at any one time for a duration of 30 days 	<ul style="list-style-type: none"> Change of background of 5 NTU at any time 	<ul style="list-style-type: none"> Change from background of 10%

When turbidity levels exceed the induced change from 8 NTUs for a duration exceeding 24 hours, a water sample will be collected (an “action”) and submitted for laboratory analysis of TSS, turbidity, pH, conductivity, and total and dissolved metals, and temperature and dissolved oxygen will be measured in situ. Water quality will be sampled in the receiving watercourses upstream (to provide background levels where applicable) and downstream of the construction area runoff, within a maximum period of 30 minutes of each other, and the flow of the effluent and receiving water will be measured. The water quality results for pH, total and dissolved metals, temperature, and dissolved oxygen will be evaluated for compliance with the provincial water quality guidelines for the protection of freshwater aquatic life.

In the event that a measurement is over the target listed in Table 6.1, a preliminary investigation (“response”) will take place to confirm whether the exceedance is valid (e.g., not simply a result of passing debris) and whether the construction site itself is the source of elevated turbidity measurements.

If the elevated turbidity level is valid and is a result of construction activities, the Environmental Monitor will inform the Project Manager or Field Manager, who shall cease all work that may have a direct or indirect impact on water quality, and immediately initiate additional mitigation actions. Upon confirmation of the exceedance, and no later than 10 hours after the exceedance began (or 10 hours after first light if the exceedance occurs at night), a preliminary notification will be sent out to other relevant parties (Project Sponsor). The notification will include:

- Date and time of inspection
- Site location information
- Timing, location, magnitude, and duration of turbidity exceedance
- Any information about suspected source of sediment
- Description of the repairs, maintenance and/or modifications of ESC measures planned in order to address the elevated sediment releases causing turbidity exceedances
- Estimated timing for the completion of repairs, maintenance and/or modifications

BW Gold will immediately notify the Chief Inspector of Mines if suspension of construction occurs due to environmental concerns in compliance with Condition C.2.(b) of Permit M-246. In addition, non-compliance reports will also be submitted to ENV at EnvironmentalCompliance@gov.bc.ca.

In the event that turbidity exceedances continue despite initial efforts to rectify ESC deficiencies, updated reports will be sent to the relevant parties daily until turbidity returns to the applicable target.

Depending on the site, the nature of the construction work, and the magnitude and duration of the exceedance, stop work orders may be issued if on-going exceedances are not rectified in a timely manner.

6.2.2 INCIDENT MONITORING

A TARP will also be implemented if signs of erosion are noted on site during the construction or operations phases outside of regular monitoring events. Three levels of qualitative triggers have been defined: examples of each trigger level and roles and responsibilities for the implementation of subsequent actions are summarized in Table 6.2.

Table 6.2 Incident Monitoring Triggers and Actions

Roles	• Trigger – Minor	• Trigger – Moderate	• Trigger – Major
<p><i>First person On the Scene (First Responders) will assess conditions to determine the initial Trigger to be applied.</i></p> <p>First Responder - First person on the scene who discovered the event. Project Engineer - Personnel designated to perform inspections.</p>	<p>Examples of Minor Triggers Fresnet Preparation. Old and non-active erosion events. Small Rills, non-active. Equipment required is as per normal activities for maintenance and minor repairs. Small, easily manageable erosion events. Standing water in non-designated areas.</p> <ol style="list-style-type: none"> Note areas where erosion event has occurred, notify Supervisor. If possible redirect flows or correct event immediately. Inspectors to note culverts that may be plugged and that may need attention to be ready for spring freshet flows. Investigate source of erosion event as necessary to prevent repeats or to reduce/remove potential for larger event. 	<p>Examples of Moderate Triggers: Active ditch erosion. Existing Freshet Conditions. 24-hr storm events >32 mm rain precipitation (2-Year return period). Conditions that are active and have the potential to cause operational changes due to access restrictions or have potential for threats to infrastructure. Standing water in non-designated areas that have potential for mobility or interfere with operations</p> <ol style="list-style-type: none"> All Minor Response duties. Provide immediate actions/assistance as necessary to minimize negative effects of erosion event if safe to do so. Notify EPCW contractor of event including location, potential for damage, proximity to water body, and safety aspects. 	<p>Examples of Major Triggers Slopes with active gullies and erosion channels where large volumes of sediment including rock is entrained. Immediate threats to infrastructure. Major sedimentation threats to water bodies. 24-hr storm events >50 mm rain precipitation (10-Year return period). Prolonged heavy rainfall events > 3 days. Standing water in non-designated areas that have potential for mobility or interfere with operations in high risk/critical areas</p> <ol style="list-style-type: none"> All Moderate Response duties. Prevent entry by non-essential personnel and maintain a safe distance. If safe to do so, minimize negative effects. Release the scene to Mine Rescue upon their arrival as necessary.
Contractor	<ol style="list-style-type: none"> All Minor Response duties. Determine level of effort required to mitigate the hazard and repair the damage. Organize mitigations/repairs. Notify Environmental Manager, if associated with water bodies or in receiving environment. Notify Mine Manager if event associated inside the pit or with catch benches or with tallings storage facility. Notify department superintendent/superintendent as necessary. 	<ol style="list-style-type: none"> All Minor Response duties. Determine level of effort required to mitigate the hazard and repair the damage. Organize mitigations/repairs. Notify Environmental Manager, if associated with water bodies or in receiving environment. Notify Mine Manager if event associated inside the pit or with catch benches or with tallings storage facility. Notify department superintendent/superintendent as necessary. 	<ol style="list-style-type: none"> All Moderate Response duties. Depending on gravity of situation, initiate Mine Emergency Response Procedures. Ensure safety of the First Responder and safety of the crew by preventing non-essential personnel from entering area. Notify Engineering and Environmental Departments. Notify Project Engineer.
Environmental Monitor	<ol style="list-style-type: none"> Schedule inspections and designate inspectors in fall periods for freshet readiness in spring. Share notes of inspections with EPC Contractor and Construction Manager as necessary. Review SEPCP and revise as necessary. Ensure revisions are communicated to all affected departments. 	<ol style="list-style-type: none"> Respond to notifications for further inspection. If sedimentation into waterbody, perform up and downstream samples for water quality to determine compliance. Note: Full suite samples may be necessary. Direct environmental/erosion controls that may have to take place to mitigate impacts, reduce environmental hazard. Record event and mitigations for reporting purposes. 	<ol style="list-style-type: none"> All Moderate Response duties. Notify Environmental Manager. Prepare for and assist in receiving environment investigations and impact assessments.
Construction Manager	<ol style="list-style-type: none"> Schedule inspections and designate inspectors in fall periods for freshet readiness in spring. Share notes of inspections with Environment Monitor as necessary. 	<ol style="list-style-type: none"> Provide resources/guidance to event responders as necessary. Determine if outside agencies are required to provide assistance. Determine courses of action to prevent/mitigate damage to resources. 	<ol style="list-style-type: none"> All Moderate Response duties. Notify Environmental Manager. Notify Safety Lead. Notify Mine Manager.
Environmental Manager	<ol style="list-style-type: none"> Duties as normal. 	<ol style="list-style-type: none"> Report event to external agencies, Indigenous groups as necessary. 	<ol style="list-style-type: none"> All Moderate Response duties. Provide recommendations to senior management on risks, mitigations and impacts.
Mine Manager	<ol style="list-style-type: none"> Duties as normal. 	<ol style="list-style-type: none"> Duties as normal. 	<ol style="list-style-type: none"> Notify Corporate Executive as necessary. Ensure all necessary funding and resources are provided in an efficient manner.

6.3 SEDIMENT CONTROL POND DISCHARGE MONITORING

Given that the discharge from the Plant Site SCP is not to a water-course but rather to the RIBs, a specific trigger is not being considered to cease discharge from the SCP. Instead, turbidity will be used as an indicator to consider the implementation of potential contingency measures, such as the addition of flocculant. Some instances when the addition of flocculants can be added are during high flow events.

In the event that there is discharge from the SCP emergency spillway to the RIBs, BW Gold will notify the Director of Environmental Management Act Authorization – North Region within 24 hours at EnvAuthorizationsReporting@gov.bc.ca, in accordance with Section 3.1 of Permit 110602.

6.4 REPORTING

6.4.1 EARLY WORKS ACTIVITIES REPORTING

Reporting will be done in accordance with the CEMP – Early Works Phase (ERM, 2021). The Environmental Monitor will prepare weekly monitoring reports that will include a summary of environmental monitoring (e.g., date and time of each sample, weather conditions) and related results (e.g., receiving water results compared to Maximum Allowable Increase levels for any works in and around water, instrument calibration records, etc.), and documentation of all non-compliance instances, including the level of exceedance, the duration of exceedance, the mitigation measures taken, verification of the reporting of the exceedance and any related communications with regulators regarding the exceedance event, and future measures to be taken to avoid or control further exceedances.

Following completion of the early works construction activities, the Environmental Monitor will prepare a completion report that includes the following information specific to this ESCP:

- Maintenance activities
- Inspection results
- Assessment of the effectiveness of the BMPs based on the sampling results
- A brief description of ongoing activities at the site related to maintenance and monitoring of site areas

6.4.2 PERMIT 110602 ANNUAL REPORT

An Annual Report from the previous year will be submitted to the director within 60 days of the end of the calendar year. The Annual Report will include a summary outlining all the non-compliance report(s) required by Section 4.3 of Permit 110602, including any use of the emergency spillway. If no non-compliances have occurred this will be indicated in the report. The Annual Report will be submitted by email to the Ministry's Routine Environmental Reporting Submission Mailbox at EnvAuthorizationsReporting@gov.bc.ca or as otherwise instructed by the director.

6.4.3 PERMIT 110602 NON-COMPLIANCE NOTIFICATION AND REPORTING

BW Gold will immediately notify the director or designate by email at EnvironmentalCompliance@gov.bc.ca or as otherwise instructed by the director, of any non-compliance with the requirements of Permit 110602. BW Gold will immediately take remedial action to remedy any effects of such non-compliance. Written confirmation of all non-compliance events, including available test results, will be provided to the Director

within 24 hours of the original notification by email at EnvironmentalCompliance@gov.bc.ca, or as otherwise instructed.

A Non-Compliance Report will be submitted to the Director within 30 days of any non-compliance.

The non-compliance report will include:

- a) An explanation of the most probable cause(s) of the noncompliance.
- b) A description of remedial action planned and/or taken by the permittee to prevent similar noncompliance(s) in the future.

6.4.4 PERMIT M-246 COMPLIANCE STATUS REPORT

If suspension of construction occurs due to environmental concerns, BW Gold will immediately notify the Chief Inspector, as stipulated in Section C.2 (b) of Permit M-246.

BW Gold will track the compliance status of all permit conditions and inspection orders in a form acceptable to the Chief Inspector and maintain an up-to-date tracking table on site. The tracking table will be available at the mine site at all times and to a Mines Inspector upon request.

An annual Compliance Status report will be submitted to the Chief Inspector by March 31st of each year. The Annual report will include a summary of outstanding non-compliance issues and an action plan, for achieving compliance.

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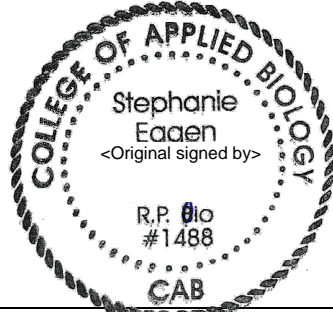
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8.0 CERTIFICATION

This report was prepared and reviewed by the undersigned.



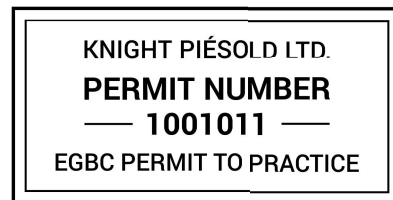
Prepared:

Stephanie Eagen, R.P. Bio.
Senior Environmental Scientist

<Original signed by>

Reviewed:

Jim Fogarty, P.Eng.
Senior Engineer



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Approval that this document adheres to the Knight Piésold Quality System:

APPENDIX A

Blackwater Gold Project – Plant Site Area and Sediment Control Pond – Site Characterization Summary

(Pages A-1 to A-26)

February 14, 2022

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Dear Alastair,

RE: Blackwater Gold Project – Plant Site Area and Sediment Control Pond – Site Characterization Summary

1.0 INTRODUCTION

BW Gold Ltd. (BW Gold), a wholly owned subsidiary of Artemis Gold Inc. (Artemis), is developing the Blackwater Gold Project (the Project), which is located approximately 112 km southwest of Vanderhoof in central British Columbia (BC), as shown on Figure 1. The Project is a large gold-silver deposit, which is proposed to be developed as a conventional truck-shovel open pit mine with a gold processing plant. The ore will be processed in a plant by a combined gravity circuit and whole ore leaching to recover gold and silver into a gold-silver doré product.

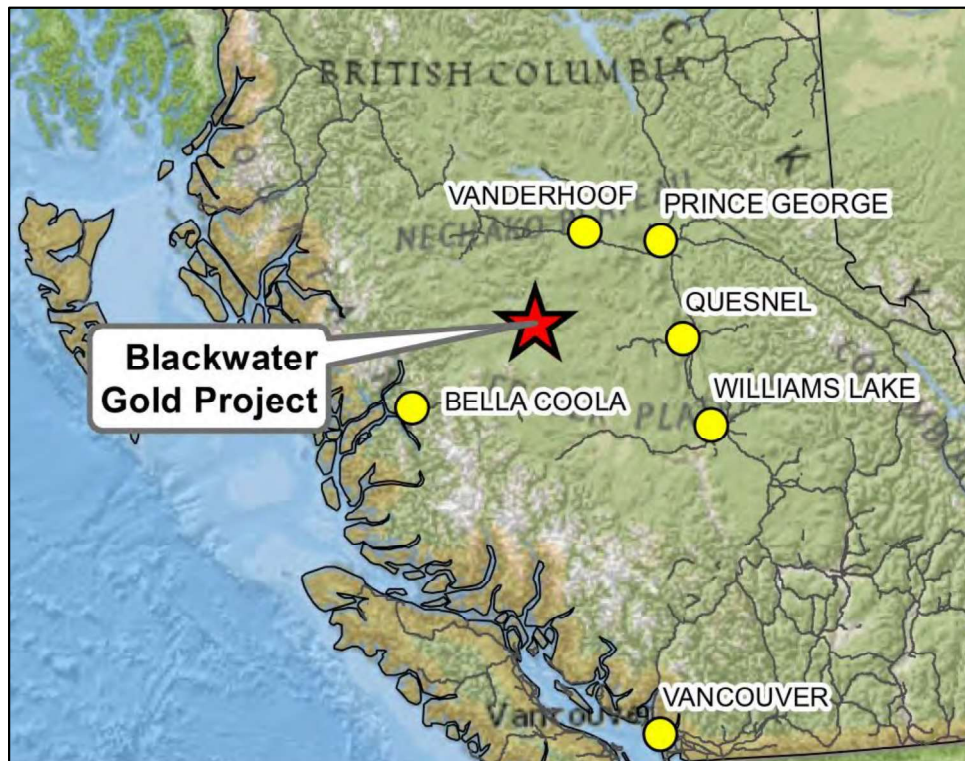


Figure 1 Project Location Map

The Blackwater area was actively explored by Richfield Ventures Corp. (Richfield) beginning in 2009. The Blackwater property was obtained by New Gold Inc. (New Gold) through the acquisition of Richfield in June 2011. Knight Piésold Ltd. (KP) was retained by New Gold beginning in early 2011 to provide technical support for the Project and has been involved continuously since early 2011 in various engineering and environmental aspects. Artemis entered into an asset purchase agreement in June 2020 to acquire Blackwater from New Gold. BW Gold is the holding entity for the mineral claims and was the party to the purchase agreement with New Gold. Artemis prepared a feasibility study in 2021 based on a revised approach to developing the Project. KP contributed to the design of the TSF and associated water management facilities for the 2021 Feasibility Study (the 2021 FS).

KP prepared the design of the plant site sediment control pond (SCP) and associated collection channels in the vicinity of the plant site area (KP, 2021a) and outlined additional concepts for several rapid infiltration basins (RIBs) (KP, 2021b) supporting an Early Works (EW) permit application. The *Mines Act* (MA) and *Environmental Management Act* (EMA) Permits were issued on June 22 and 24, 2021, respectively, authorizing the EW construction activities, including earthworks at the process plant location and the associated erosion and sediment control works designed by KP.

BW Gold submitted a joint *Mines Act* and *Environmental Management Act* Permits Application (the Joint Application) on November 26, 2021, seeking authorization for construction of the Project. KP prepared a report on the Plant Site Foundation Assessment (KP, 2021c), which was submitted with the Joint Application providing the characterization of the foundation conditions in the area and foundation design recommendations for the proposed process plant and associated infrastructure. The plant site area foundation characterization was informed by a geotechnical investigation conducted in the plant site area in February 2021. The factual data from this geotechnical investigation program was included in the 2020-2021 Geotechnical Site Investigation Data Report (KP, 2021d) and incorporated in the Dam Site Characterization Report (KP, 2021e), both of which were included in the Joint Application. The Dam Site Characterization Report compiles available geotechnical, geological, hydrogeological information for the mine site and provides a comprehensive assessment of the site conditions.

A supplemental test pitting program was completed in November 2021, including excavation of additional test pits in the plant site area and infiltration testing in two test pits to assess infiltration characteristics in the vicinity of the plant site SCP and RIBs. The factual data from the test pitting program is summarized in the Q4 2021 Test Pit Summary Letter (KP, 2022a). The location of the drillholes and test pits conducted in the plant site area are shown on Figure A.1 in Appendix A.

This letter report compiles all geological, geotechnical, and hydrogeological information collected from the site investigation programs and provides an updated characterization of the subsurface conditions at the plant site area, SCP, and RIBs.

2.0 SITE CONDITIONS

2.1 PHYSIOGRAPHIC SETTING

The Project site is situated on the Nechako Plateau, which is characterised by gently undulating northwest trending highlands dissected by small to medium sized valleys, drainages, and other low-lying areas. It features broad valleys with gentle slopes that have been shaped during glaciation. The elevation of the Blackwater property ranges from just over 1,000 m in low-lying areas northeast of the proposed mine site to 1,800 m at the summit of Mt. Davidson on the southwest side of the property. The Blackwater deposit is located on the northern flanks of Mt. Davidson.

The surficial deposits at the Project site are from the Fraser Glaciation, the last period of ice sheet glaciation in BC. The Cordilleran ice sheet covered the Blackwater mine area at the peak of the last (Fraser) glaciation approximately 19,000 years ago. At the peak of glaciation, the localized ice flow direction in the Project area was toward the northeast, as evidenced by drumlins, eskers, and other streamlined glacial landforms. Geomorphological evidence of glaciation suggests that at the height of the Fraser Glaciation, the ice elevation exceeded 1,750 masl, higher than most of the tallest peaks in the region.

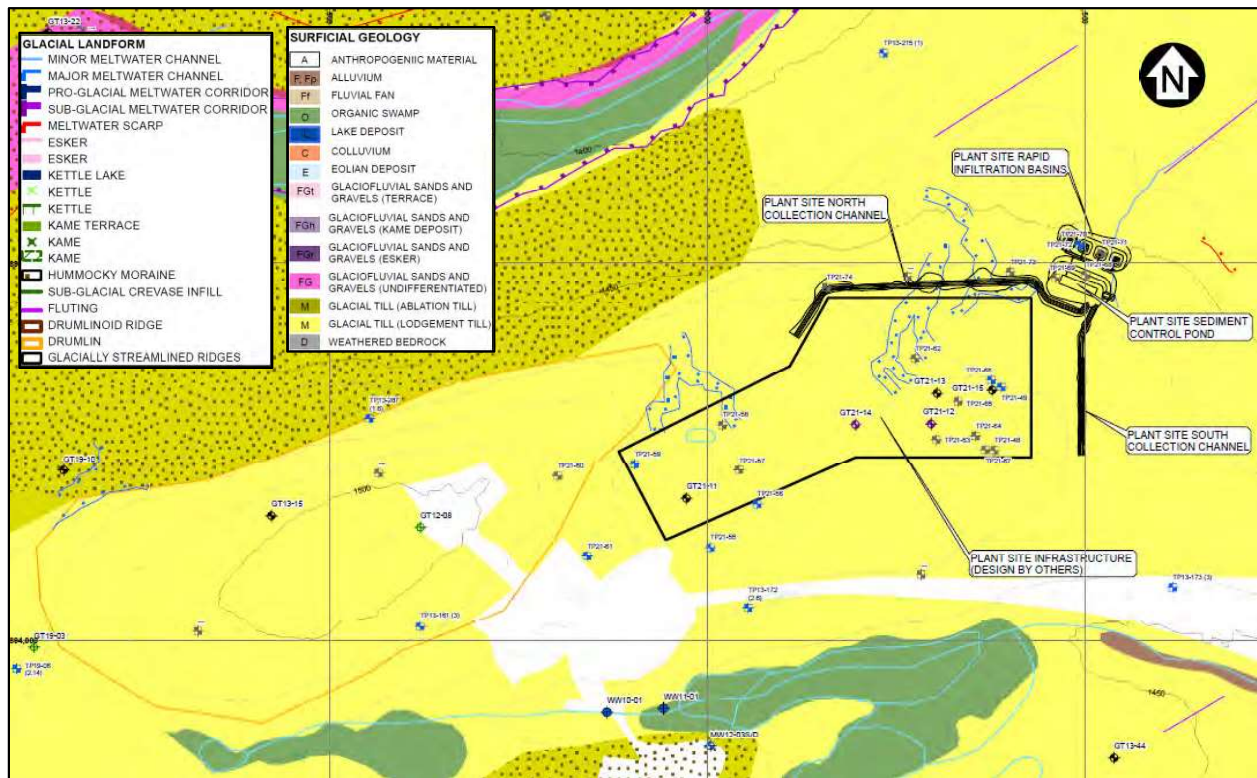
2.2 REGIONAL GEOMORPHOLOGY

Deglaciation commenced approximately 16,000 years ago and progressed by frontal retreat to the west or southwest towards the Coast Mountains and progressively lowering of the ice sheet surface by downwasting. The pattern of ice-marginal and subglacial meltwater channels indicates that areas of higher elevation in the vicinity of the mine site became ice-free before valley floors and other low-lying areas. Glacial ice appears to have stagnated in the Davidson Creek valley during late deglaciation producing ice stagnation landforms such as kettles and kames. The presence of eskers, kettles, and kames along this and other corridors shows that meltwater was largely confined in subglacial tunnels, rather than being proglacial. A large amount of glacial meltwater was channeled along Davidson Creek and other valleys in the area, producing eskers and meltwater channels.

Geomorphic evidence indicates that the meltwater corridors at the base of the stagnant ice mass evolved over the short period during which they were active. Downward-stepping terraces within some meltwater corridors show that active channel floors were progressively lowered by fluvial erosion as the ice melted. The lowest and youngest terraces may have formed in proglacial settings after the meltwater ceased to be confined by ice. Evidence also exists for shifts in meltwater discharge among the major meltwater corridors over this period. The oldest corridors lie somewhat higher than the Davidson Creek corridor and are truncated by it. The modern drainage system became established as soon as the area was fully deglaciated, probably around 13,000 years ago. Since then, there has been little geomorphic change in the study area (Clague, 2018).

2.3 LOCAL SURFICIAL GEOLOGY

The glacial landform mapping completed for the Project area indicates that the proposed plant site area is situated to the northeast of a drumlin landform. The primary surficial materials anticipated in the proposed plant site area comprise lodgement glacial till as evidenced by glacial fluting observed in the landform mapping. Minor meltwater channels, flowing towards the north, are present locally and differences in the surficial geology may be present in the vicinity of these channels. The surficial geology and landform map is shown on Figure A.2 in Appendix A.



Note(s):

- Information shown on Figure 2 is available from the attached source Figure A.2 included in Appendix A.

Figure 2 Plant Site Area – Surficial Geology and Landform Map

2.4 REGIONAL SEISMICITY

The Project site is situated within a region of BC where the level of recorded historical seismic activity has been low. However, higher seismicity is associated with the Queen Charlotte - Fairweather fault system located offshore of the west coast of BC and the Alaskan panhandle. The level of seismicity in the interior of BC and the Rocky Mountains region drops off rapidly with distance from the west coast and to the north. The seismicity of southwestern BC associated with the Cascadia and Explorer subduction zones has the potential for large magnitude 8 to 9+ earthquakes, but too distant to make a significant contribution to the seismic hazard at the Project site. A detailed seismic hazard assessment for the Project site is presented in a separate KP report (KP, 2021f).

2.5 LOCAL BEDROCK GEOLOGY

Bedrock exposure is rare at the Project site and is typically restricted to higher elevation areas. Andesites of the Eocene Ootsa Lake Group are found at the eastern half of the proposed waste and management facilities including the proposed plant site area. Mudstones, sandstones, and conglomerates of the Jurassic Bowser Lake Group; and fragmentals and felsic tuff of the Late Cretaceous Kasalka Group are found at central and western parts of the Project site.

The structural geology of the Project area was interpreted by SRK Consulting (Canada) Inc. (SRK) in 2013 (SRK, 2013) based on a series of airborne magnetic, electromagnetic, and radiometric data sets. A

northeast striking fault is inferred to be present at the southern part of the plant site area based on the regional structural geology maps which incorporated SRK’s interpretation (New Gold, 2014).

3.0 SUBSURFACE CONDITIONS

3.1 STRATIGRAPHY

The stratigraphy of the surficial materials and bedrock at the Project from surface downward is as follows:

- Holocene Deposits (Topsoil)
- Fraser Glaciation Deposits including
 - Glacial Till (includes Ablation Till, Lodgement Till, Undifferentiated Till)
 - Glaciofluvial
 - Glaciolacustrine
- Reworked Regolith
- Bedrock
 - Completely Weathered Bedrock
 - Highly Weathered Bedrock
 - Intact Bedrock

The surficial materials and bedrock at the proposed plant site area is described in Section 3.2 below. Cumulative detailed description of these materials found from the entire Project area can be found in the Dam Site Characterization Report (KP, 2021e).

3.2 MATERIAL AND FOUNDATION CONDITIONS

3.2.1 GENERAL

The geotechnical properties of the surficial material and bedrock at the plant site area were assessed using the information collected from the drillhole, test pits, and laboratory testing completed in 2021. Information from 23 test pits, 5 geotechnical drillholes, and 2 condemnation drillholes, completed at the vicinity of the plant site area, have been used characterize the material and foundation conditions at the plant site area. The associated drillhole and test pits divided into the infrastructure and the erosion and sediment control areas are summarized in Table 1 and shown on Figure A.1.

Table 1 Plant Site Drillhole and Test Pit Summary

Plant Site Areas	Drillhole Sites	Test Pit Sites
Main Infrastructure - Crusher, Ore Stockpile, Tanks, and Buildings	GT21-11 to GT21-15, CDH127	TP21-48, TP21-49, TP21-55 to TP21-61
Surface Water Management Structures - Collection Channels, Sediment Control Pond (SCP), and Rapid Infiltration Basins (RIBs)	CDH124	TP12-129, TP21-68 to TP21-74

The unit interval thicknesses are summarized in Table 2. The available laboratory index testing results and compaction results are summarized in Tables 3 and 4 and presented in Figures 2 to 4. In-situ downhole seismic testing results are summarized in Table 5. Descriptions of the surficial materials and bedrock units are provided in the sections 3.2.2 to 3.2.7.

Table 2 Plant Site – Unit Interval Thickness and Elevation Summary

Unit	Interval Thickness (mbgs)	Top Elevation (masl)
Topsoil	0.2 - 0.5	1,487.0 – 1,450.0
Glacial Deposits	0.5 – 46.1	1,486.7 – 1,449.7
Reworked Regolith	2.4 – >4.6	1,455.3 – <1,424.0
Bedrock (Highly and Intact)	-	1,452.4 – 1,425.6

Table 3 Plant Site – Laboratory Index Testing Summary

Unit	Particle Size Distribution (% Retained)				Moisture Content (%)	Atterberg Limits	Specific Gravity
	Total Test Count	Gravel	Sand	Fines		Plasticity Index, PI (%)	
Ablation Till	4	32	44	21	8	NP	2.6
Lodgement and Undifferentiated Till	20	29	36	35	9	7	
Glaciofluvial	1	23	66	11	9	-	-
Glaciolacustrine	1	0	69	31	21	NP	2.6
Reworked Regolith	4	24	37	39	10	-	-

Note(s):

1. Average values shown.

Table 4 Plant Site – Laboratory Compaction Testing Summary

Unit	Standard Proctor		
	Total Test Count	Corrected Maximum Dry Density (kg/m ³)	Corrected Optimum Moisture Content (%)
Ablation Till	7	2110-2270 (2180)	6-10 (7)
Lodgement and Undifferentiated Till			
Glaciofluvial	-	-	-
Glaciolacustrine	-	-	-
Reworked Regolith	-	-	-

Note(s):

1. Minimum and maximum values shown. Average value shown in brackets.

Table 5 Plant Site - Downhole Seismic Testing Summary

Unit	Downhole Seismic Testing	
	Data Points Count	Shear Wave Velocity, Vs (m/s)
Ablation Till	2	463-531 (500)
Lodgement and Undifferentiated Till	59	406-1044 (800)
Glaciofluvial	-	-
Glaciolacustrine	-	-
Reworked Regolith	1	1038

Note(s):

1. Minimum and maximum values shown. Average value shown in brackets.

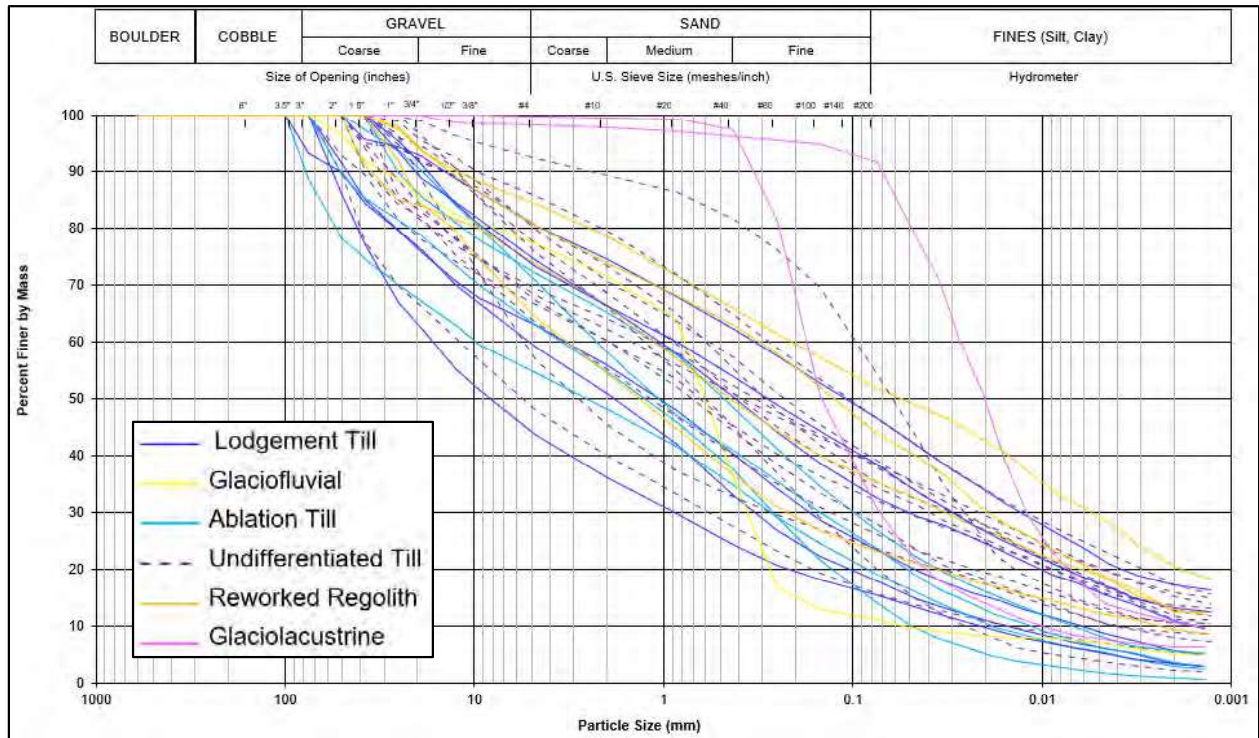


Figure 3 Plant Site Samples – Particle Size Distribution

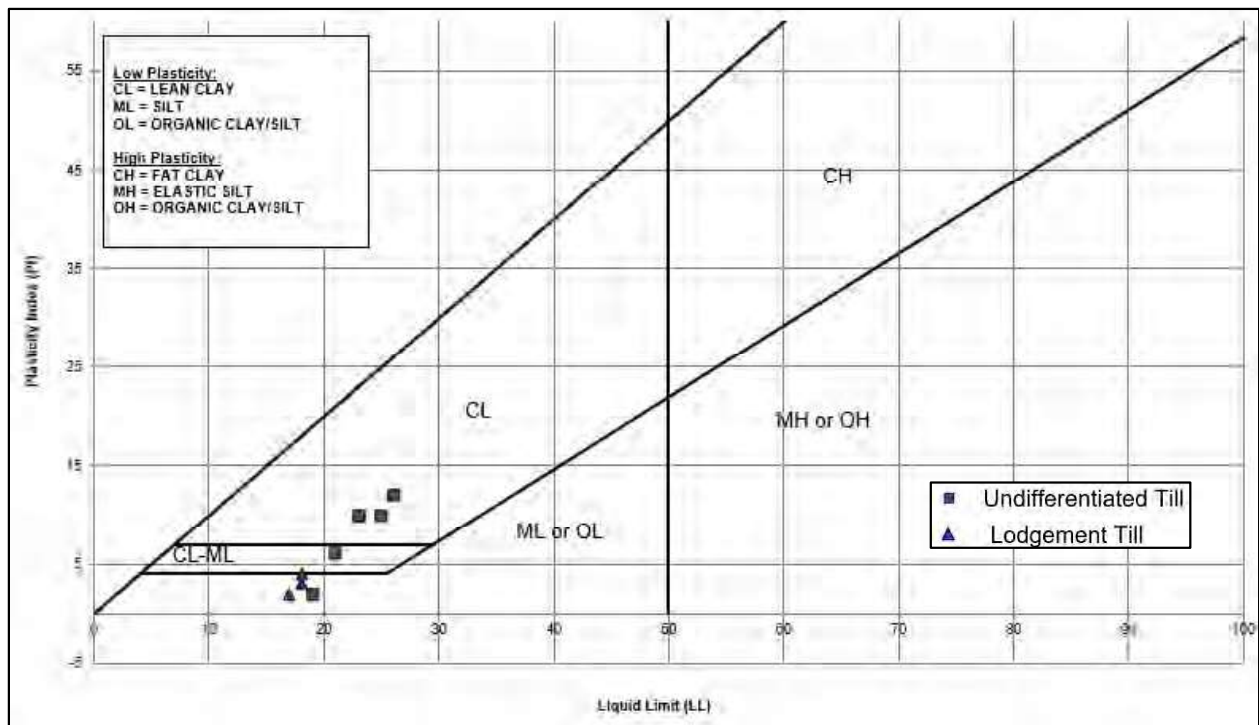


Figure 4 Plant Site Samples – Plasticity Chart

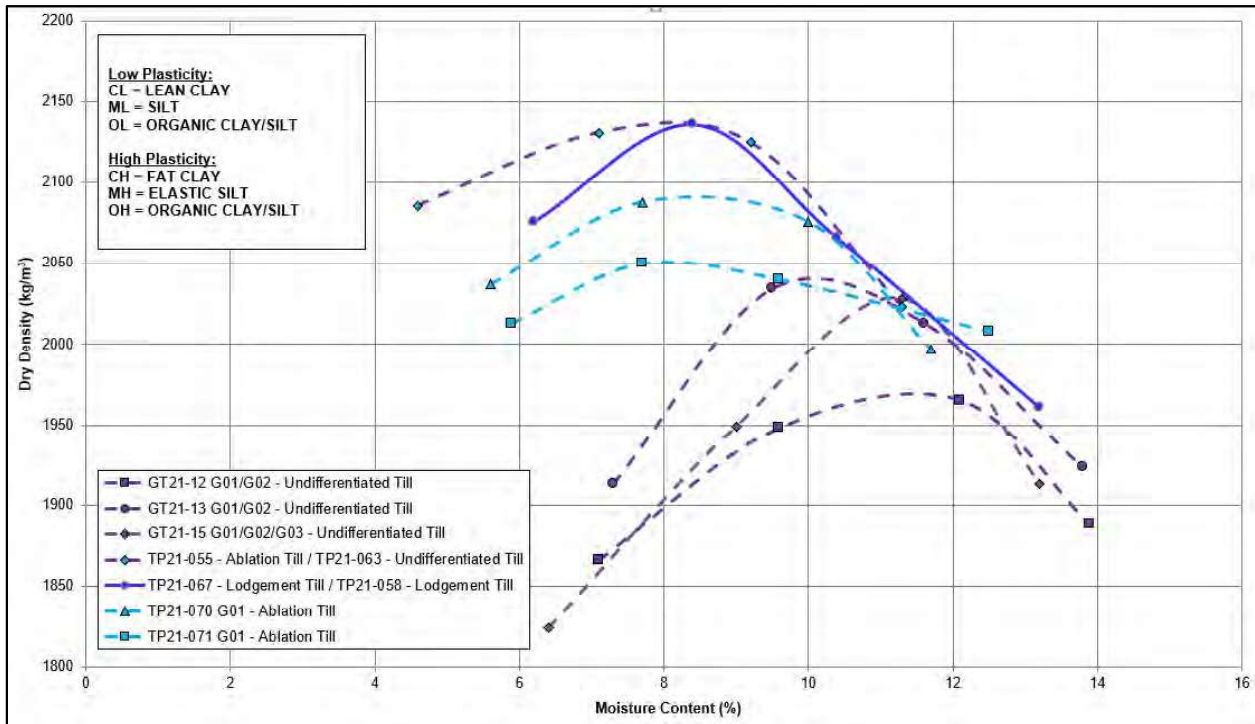


Figure 5 Plant Site Samples – Compaction Data

3.2.2 TOPSOIL

A topsoil layer varying in thickness from 0.2 to 0.5 m is present over the entire proposed plant site area, and generally observed to be orangey brown to light grey organic layer with fine to medium sand and trace silt and gravel with root inclusion. Wetland organic material was observed at test pit TP21-59 consisting of black, spongy, moist to saturated, silty peat material.

3.2.3 GLACIAL DEPOSITS

Glacial sequences were identified with thicknesses ranging from 0.5 m to the west and increasing in depth to up to 46 m to the east of the proposed plant site area. The glacial sequences are predominantly composed of glacial till with minor interlayers of glaciolacustrine units and shallow glaciofluvial deposits.

- **Glacial Till** – Glacial till is the dominant overburden material encountered across the site, immediately below the topsoil layer, and includes ablation till, lodgement till, and undifferentiated till. The glacial till materials.
 - Ablation till is present at surface with thickness ranging from 0.5 to 5.5 m. Ablation till is present at the northern and western part of the plant site area. These deposits were observed to be well graded, non-plastic, greyish brown to orangey brown, massive, moist, compact, gravelly sand to sandy gravel material with trace silt and cobbles. Particle size distribution data shows grain size composition averages of 32% gravel, 44% sand, and 21% fines. The ablation till was tested with an average moisture content of 8% and is non-plastic.

- Lodgement and undifferentiated till occur below at depth throughout the site with interval thickness ranging from 18.1 to 45.8 m and increasing depth towards the eastern part of the plant site area with a maximum depth of 46.1 mbgs. These deposits were observed to be gap graded to well graded, non-plastic to medium plasticity, dark brown to greyish brown, massive, moist, stiff to very still gravelly sandy silt material to compact to dense gravelly silty sand material. Particle size distribution data shows grain size composition averages of 29% gravel, 36% sand, and 35% fines. An average moisture content of 9% and plasticity index of 7% was determined for the tested samples of lodgement and undifferentiated till materials.
- Standard proctor testing of the glacial till materials resulted in an average corrected maximum dry density of 2,180 kg/m³ and an average optimum moisture content of 7%. Specific gravity testing resulted in an average of 2.6.
- Downhole seismic testing completed in the glacial till materials yielded a range in shear wave velocity from 406 to 1044 m/s. The shear wave velocity in the ablation till material has an average of approximately 500 m/s while the lodgement and undifferentiated tills have an average of approximately 800 m/s.
- **Glaciofluvial Deposits** - Glaciofluvial (undifferentiated) deposits were encountered close to surface at two test pits (TP21-49 and TP21-72) located at the northeastern part of the plant site area. These deposits correspond to the minor meltwater channels with flow direction towards the north. These glaciofluvial deposits were observed to be well graded, non-plastic, massive, light to greyish brown, compact, moist to wet, sand and gravel to gravelly sand material. Particle size distribution data shows grain size composition averages of 23% gravel, 66% sand, and 11% fines. Laboratory testing of the glaciofluvial deposit samples indicate an average moisture content of 9%.
- **Glaciolacustrine Units** - A localized 1-m thick layer in between glacial till layers was encountered in drillhole GT21-15 only located at the eastern part of the plant site area, at a depth of approximately 16 mbgs and at a top elevation of 1,454 masl. This glaciolacustrine unit was observed to be uniformly graded, non-plastic, indistinctly laminated, brown, moist, sand with some silt material. A surficial 0.5-m thick possible glaciolacustrine layer overlying ablation till was encountered in test pit TP21-59 at the western part of the plant site area at a top elevation of 1,478 masl. This unit was observed to be uniformly graded, indistinctly stratified, low to medium plasticity, greyish brown, soft to firm, moist to wet, sandy silt material. Particle size distribution data shows grain size composition averages of 0% gravel, 69% sand, and 31% fines. The glaciolacustrine unit was tested with an average moisture content of 21% and is non-plastic. One specific gravity test in the glaciolacustrine unit resulted in a value of 2.6.

3.2.4 REWORKED REGOLITH

The Fraser glacial sequence rests on a reworked weathered bedrock horizon termed as “reworked regolith”. The reworking is due to gravitational and perhaps glacial overriding on top of the weathered bedrock. This unit was encountered in four of the five drillholes within the plant site area with thickness ranging from 2.4 to greater than 4.6 m. The reworked regolith was observed to be gap graded, low to medium plasticity, massive, moist, mottled dark brown to reddish grey with iron oxide staining. Particle size distribution data shows grain size composition averages of 24% gravel, 37% sand, and 39% fines. Laboratory testing indicates an average moisture content of 10% for the reworked regolith material. One downhole seismic data point was collected in the reworked regolith resulting in a shear wave velocity of 1,038 m/s.

3.2.5 BEDROCK

The bedrock at the site is categorized into completely weathered, highly weathered, and intact bedrock depending on weathering and strength characteristics. Completely weathered bedrock is absent in topographically high areas such as the plant site area where it was not encountered. Highly weathered bedrock was intercepted in drillhole GT21-12 at a depth of 46.9 mbgs and an elevation of 1,426 masl located at the southeastern part of the plant site area. The bedrock surface deepens to the east where condemnation drillhole CDH127 intercepted bedrock at a depth of 65.5 mbgs and an elevation of 1,406 masl. A condemnation drillhole CDH124 located at the plant site SCP intercepted bedrock at a depth of 81.1 mbgs and an elevation of 1,371 masl.

Bedrock is higher to the west of the plant site area as intercepted in drillholes GT12-11 and GT12-14 at 26 mbgs (1,450 masl) and 22.6 mbgs (1,452 masl), respectively. Bedrock was encountered close to surface in two test pits further west with a depth of 1 mbgs (1,486 masl) in TP21-60 and a depth of 1 mbgs (1,483 masl) in TP21-61. The bedrock lithology is predominantly andesite which can generally be described as a strong rock with 'FAIR' RMR₈₉ Rating (KP, 2021e).

3.3 GROUNDWATER CONDITIONS

Groundwater elevations were measured in open holes during and immediately after the February 2021 drilling program. The open hole groundwater levels varied from 6 m to 38 mbgs. Artesian conditions were not observed. VVPs were installed after the completion of drillholes GT21-12 and GT21-14 and the measured static groundwater levels in October 2021 were 30 mbgs (1,443 masl) and 25 mbgs (1,450 masl), respectively.

Groundwater seepage was observed at depths from 0.5 to 3 mbgs in test pit TP21-59 located at the western part of the plant site area where it is near a wetland. Groundwater seepage was also observed at depths from 1 to 2 mbgs in the highly weathered bedrock in test pit TP21-61. Minor groundwater seepage was observed at depths ranging from 1.25 to 2.5 mbgs in five other test pits (TP21-49, TP21-55, TP21-56, TP21-66, and TP21-72) throughout the plant site area. The seepage was generally observed in ablation till and undifferentiated till overlying a lodgement/undifferentiated till unit.

Infiltration testing was completed in the ablation till material in test pits TP21-70 and TP21-71 at the northern plant site RIB area. The results of the test pit infiltration tests show an average infiltration rate of 0.004 m/hr for TP21-70 and 0.04 m/hr for TP21-71, which corresponds to an estimated annual hydraulic loading of 35 m/year for TP21-70 and 336 m/year for TP21-71. The materials encountered in the two test pits were similar, and the variability in results may be due to differences in material underlying the test pits. A meltwater channel is located in close proximity to TP21-71 and may influence the infiltration capacity on the eastern side of the proposed plant site SCP and RIBs.

The RIB design contemplates an average annual hydraulic loading rate of approximately 88 m/year (KP, 2021b), which was based on the results of previous investigations at the site. The infiltration tests completed in 2021 indicate that the average hydraulic loading rate is reasonably consistent with local site conditions, but that local variability could be expected to influence operational performance of the RIBs. No changes to RIB land area requirements are recommended based on the results of the investigations; however, it is recommended that the SCP outlet works incorporate sufficient flow isolation and control components to manage hydraulic loading to the individual RIBs consistent with their observed performance. Larger scale infiltration testing should be incorporated in the initial performance monitoring of the

constructed RIBs, and the results should be considered in the operations, maintenance, and surveillance plans for the Plant Site SCP and RIBs.

4.0 SUMMARY AND CONCLUSIONS

This updated site characterization for the proposed plant site area and associated erosion and sediment control works at Blackwater was prepared based on the results of the 2020-2021 geotechnical investigation program and the more recent Q4 2021 test pitting program. The characterization of the plant site area remains consistent with the previous assessment (KP, 2021c) and confirms the previously inferred characteristics of the foundation materials present at the proposed Plant Site SCP and RIBs.

The proposed facilities will be founded on glacial deposits comprising mainly till, localized surficial glaciofluvial deposits at the northeastern part, and localized minor discontinuous glaciolacustrine sediments. The bedrock at the proposed plant site area is characterized as a strong, slightly to highly weathered andesite where it is closer to surface to the west and as deep as 66 mbgs to the southeast and 81 mbgs to the northeast at the plant site SCP area. Groundwater levels are expected to be deep in the area with measured depths ranging from 25 to 30 mbgs at two sites; however, there the potential for shallower layers with perched water above this depth as indicated by the minor groundwater seepage observations in several of the test pits.

Please do not hesitate to contact the undersigned with any questions regarding this letter report.

Yours truly,
Knight Piésold Ltd.

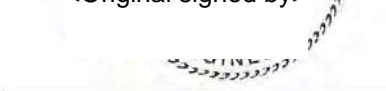

 <Original signed by>


 <Original signed by>

Prepared:


 Joseph Cristobal, P. Eng.
 Senior Engineer

Reviewed:


 Daniel Fontaine, P. Eng.
 Specialist Engineer | Associate

Approval that this document adheres to the Knight Piésold Quality System:

DOF

Attachments:

Appendix A Reference Plan Maps
 Appendix B Site Characterization Assurance Statements

References:

Clague, J. (2018). Deglacial Geology of the Blackwater Mine Study Area.
 Eagle Mapping Ltd. (2012). Blackwater LiDAR Data Report prepared for Knight Piésold, March, 2012. Vancouver.

Knight Piésold Ltd. (2021a). Surface Water Management and Sediment Control Design Report for the Plant Site Early Works. February 5, 2021. Vancouver, British Columbia. Ref No: VA21-00232. Vancouver.

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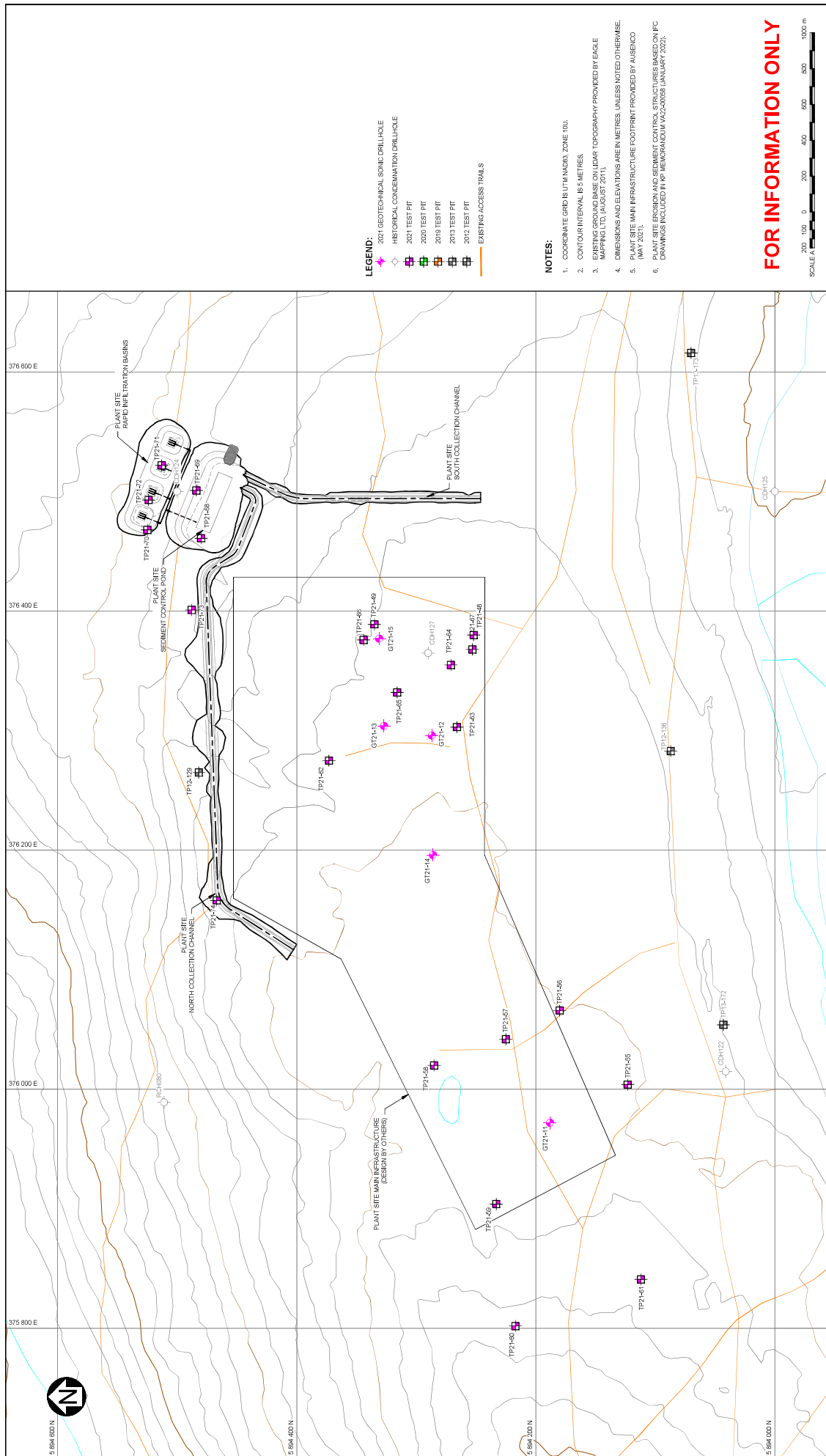
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/jbc

APPENDIX A

Reference Plan Maps

(Figures A.1 to A.2)



- LEGEND:**
- ◆ 2021 GEOTECHNICAL SONIC DRILLHOLE
 - ◇ HISTORICAL CONDENSATION DRILLHOLE
 - 2021 TEST PIT
 - 2020 TEST PIT
 - 2019 TEST PIT
 - 2013 TEST PIT
 - 2012 TEST PIT
 - EXISTING ACCESS TRAILS

- NOTES:**
1. COORDINATE GRID IS UTM MGRS, ZONE 10U.
 2. CONTOUR INTERVAL IS 5 METRES.
 3. EXISTING GROUND BASE ON LUMAR TOPOGRAPHY PROVIDED BY EAGLE MAPPING LTD. (AUGUST 2011).
 4. DIMENSIONS AND ELEVATIONS ARE IN METRES, UNLESS NOTED OTHERWISE.
 5. PLANT SITE MAIN INFRASTRUCTURE FOOTPRINT PROVIDED BY AUSTRACO (MAY 2021).
 6. PLANT SITE EROSION AND SEDIMENT CONTROL STRUCTURES BASED ON IFC DRAWINGS INCLUDED IN KP MEMORANDUM W22-00185 (JANUARY 2021).

FOR INFORMATION ONLY



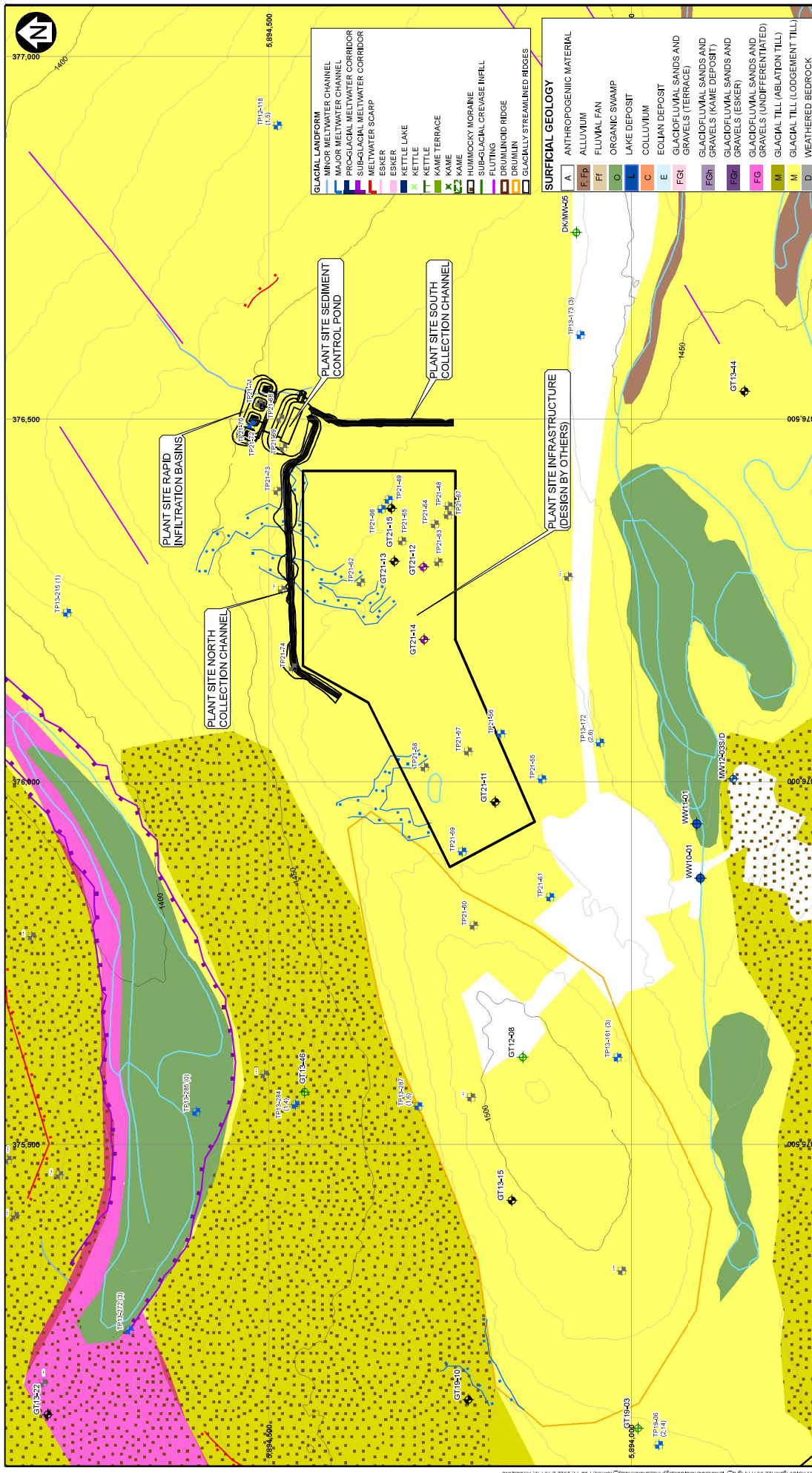
PLAN SCALE A

BW GOLD LTD.

**PLANT SITE GENERAL ARRANGEMENT
DRILLHOLE AND TEST PIT PLAN**

	DRAWING NO. VAD-0517/36	REF. NO. W22-00111
	FIGURE A.1	

REV	DATE	ISSUED WITH LETTER	ISSUED BY	CHKD BY	DESIGNED BY	DATE	CHKD BY	DATE
0	14/05/22	ISSUED WITH LETTER	ISSUED BY	CHKD BY	DESIGNED BY	DATE	CHKD BY	DATE



Legend

SYMBOL	DESCRIPTION
+	TEST PIT (NO SEEPAGE OBSERVED)
+	TEST PIT (SEEPAGE OBSERVED)
+	STOORPILE
+	OPEN PIT
+	SURGICAL GEOLOGY STUDY AREA
+	CONTOUR 50 m
+	CONTOUR 10 m
+	RIVER/STREAM
+	DRILLHOLE WITH VIBRATING WIRE PIEZOMETER
+	DRILLHOLE WITH NO INSTALLATION
+	DRILLHOLE WITH STANDPIPE PIEZOMETER
+	DRILLHOLE WITH WIRE PIEZOMETER NESTED STANDPIPE PIEZOMETER
+	MONITORING WELL
+	WELL

Groundwater Monitoring Sites

REV	DATE	ISSUED WITH LETTER	BY	CHK	APP	REVISION
0	14 FEB 22					

Notes:

1. SURFICIAL GEOLOGY TAKEN FROM DRAWING 0002 (W/18-0017).
2. COORDINATE GRID IS IN METRES, COORDINATE SYSTEM: NAD 83 UTM ZONE 18N.
3. THIS FIGURE IS PRODUCED AT A NOMINAL SCALE OF 1:600 FOR 1147 TABULAR PAPER. ACTUAL SCALE MAY VARY ACCORDING TO CHANGES IN PLOTTER SETTINGS OR PRINTED PAPER SIZE.
4. INFORMATION SHOWN IS BASED ON TERRAIN MAPPING AS SUMMARIZED IN KP REFERENCE NO. W/18/0117.
5. PROPOSED LINE SITE GENERAL ARRANGEMENT FROM TSP LINE OF MINE DESIGN REPORT DATED AUGUST 2021, TS = TOPSOIL STOCKPILE.
6. PLANT SITE MAIN INFRASTRUCTURE FOOTPRINT PROVIDED BY AUSTRACO (MAY 2021).
7. PLANT SITE EROSION AND SEDIMENT CONTROL STRUCTURES BASED ON IFC DRAWINGS INCLUDE IN KP REFERENCE NO. W/22-00111.

BW GOLD LTD.

BLACKWATER GOLD PROJECT

SURGICAL GEOLOGY AND LANDFORM MAP

PLANT SITE

DRAWING NO. W/22-00111
REV. 0

FIGURE A.2

KNIGHT PIRSOLO
CONSULTANTS

APPENDIX B

Site Characterization Assurance Statements

Appendix B1	Design Engineer Assurance Statement (CP)
Appendix B2	Supporting Registered Professional's Assurance Statement (DDF)
Appendix B3	Supporting Registered Professional's Assurance Statement (JBC)

APPENDIX B1

Design Engineer Assurance Statement (CP)

(Pages B1-1 to B1-3)

APPENDIX B1 – DESIGN ENGINEER’S SITE CHARACTERIZATION ASSURANCE STATEMENT FOR PLANT SITE AREA AND SCP

Note: This statement is based on the template provided in the *Site Characterization for Dam Foundations in BC* guideline (APEGBC, 2016).

To: The Owner(s) Date: February 14, 2022

Name: BW Gold Ltd.
Address: 595 Burrard St #3083
Vancouver, British Columbia, Canada, V7X 1L3

For the dam:

UTM (Location):	<u>Approximately 376 500 E, 5 894 485 N (Coordinate grid is UTM (NAD83) Zone 10)</u>
Located at (Description):	<u>Blackwater Gold Project</u>
Name of dam or description:	<u>Plant Site Area – Sediment Control Pond and Infiltration Basins</u>
Provincial dam number:	<u>Not applicable (not yet constructed)</u>
Dam function:	<u>Surface Water Management</u>

(Herein referred to as “the Dam”)

Current project stage is:

(Check one)

- Feasibility design
 Detailed design
 Construction/operations

The undersigned hereby gives assurance that he is a qualified EGBC-registered professional and is a professional engineer and is the **Design Engineer** for the dam project identified above. The following reports must be read in conjunction with this Assurance Statement:

- I have reviewed and accepted the characterization letter report [Blackwater Gold Project – Plant Site Area and Sediment Control Pond – Site Characterization Summary, Ref. No. VA101-457/36, Cont. No.: VA22-00111, February 14, 2022] in accordance with the *EGBC Professional Practice Guidelines – Site Characterization for Dam Foundations in BC*.
- I have prepared, reviewed, signed, sealed, and dated the detailed design letter [Surface Water Management and Sediment Control Design Report for the Plant Site Early Works, Ref. No. VA101-457/33, Cont. No.: VA21-00232, February 5, 2021], the conceptual design letter [Rapid Infiltration

Concept for the Plant Site Sediment Collection Pond Discharge, Ref. No. VA101-457/33, Cont.: VA21-00711, April 20, 2021] and the [Plant Site Early Works Erosion and Sediment Control Engineering Work Plan, Ref. No. VA101-00457/36, Cont. No.: VA22-00058] to assist with an application for *Mines Act* and *Environmental Management Act* permits associated with the Early Works construction activities at the project site.

In preparing the site characterization letter report, I have completed the following activities:

(Check the applicable items)

Completed by the Design Engineer	Activity
✓	Collected and reviewed available and relevant background information, documentation, and data
<input type="checkbox"/>	Visited the site and reviewed the conditions in the field that may be relevant for site characterization
<input type="checkbox"/>	Developed and executed a site characterization program that provides information to support the design of the dam, subject to the qualifications noted
✓	Reviewed previous site characterization studies and data and updated the dam site characterization assessment report to include all data and, where appropriate, revised interpretations of data
✓	Assessed potential areas of risk identified during site characterization programs to date and, as far as is practical, addressed the risks
✓	Evaluated the level of complexity of the site and documented how it was assessed and supported by the site characterization program(s)
✓	Reviewed and accepted all assurance statements submitted by the supporting registered professionals (SRPs)
<input type="checkbox"/>	Prepared a data record report
<input type="checkbox"/>	Prepared the dam site characterization report, which interprets the site conditions

In preparing the site characterization letter report, I have completed the following activities or reviewed and accepted such activities completed by a supporting registered professional (SRP):

(Check the applicable items)

Completed by the Design Engineer	Completed by the SRP, and reviewed and accepted by the Design Engineer	Activity
<input type="checkbox"/>	✓	1. Assessed the surficial and bedrock geological models to confirm that they adequately support the understanding of the spatial variability of the geotechnical properties of the foundation materials
<input type="checkbox"/>	✓	2. Carried out sufficient in situ and laboratory testing to quantify the geotechnical properties of the foundation materials
<input type="checkbox"/>	✓	3. Assessed the strength properties of the foundation materials with consideration of stress state and response to loadings
<input type="checkbox"/>	✓	4. Assessed the hydrogeological properties of the foundation materials with consideration of potential hydraulic gradients, artesian pressures, and seepage flow paths
<input type="checkbox"/>	✓	5. Assessed the seismotectonic conditions to provide a basis for the seismic hazard analysis of the dam
✓	✓	6. Evaluated the level of complexity of the site and documented how it was assessed and supported by the site characterization program(s)

<input checked="" type="checkbox"/>	<input type="checkbox"/>	7. Reviewed and accepted all assurance statements submitted by the supporting registered professionals (SRPs)
<input type="checkbox"/>	<input checked="" type="checkbox"/>	8. Prepared a data record report
<input type="checkbox"/>	<input checked="" type="checkbox"/>	9. Prepared the dam site characterization report, which interprets the site conditions

I hereby give my assurance that based on the site characterization letter, at this point in time:

(Check one)

- The site characterization letter report is reasonably comprehensive and supports the design of the facility.

Comments:

- This is the first site characterization assurance statement prepared for this facility.
- It is recommended that larger scale infiltration testing should be incorporated in the initial performance monitoring of the constructed infiltration basins, and the results should be considered in the operations, maintenance, and surveillance plans for the Plant Site Sediment Control Pond and Rapid Infiltration Basins.

- The dam site characterization report is not sufficiently comprehensive to support the design of the Dam, in that the dam site characterization report identifies areas of potential concern that require additional investigation as set out in section(s) _____ of the attached dam site characterization report

Name: Carlos Penate, M.Eng., P.Eng.

<Original signed by>

Signature: _____

Date: February 14, 2022

Address: 1400-750 West Pender Street

Vancouver, British Columbia, Canada, V6C 2T8

Telephone: +1 (604) 685-0543

Email: cpenate@knightpiesold.com


<Original signed by>


2022-02-14

(If the EGBC professional is a member of a firm, complete the following:)

I am a member of the firm Knight Piésold Ltd. and I sign this letter on behalf of the firm.

APPENDIX B2

Supporting Registered Professional's Assurance Statement (DDF)

(Pages B2-1 to B2-2)

APPENDIX B2 - SUPPORTING REGISTERED PROFESSIONAL'S ASSURANCE STATEMENT OF PROFESSIONAL SERVICES

To: The Design Engineer Date: February 14, 2022

Name: Carlos Penate, P.Eng.

Address: 1400-750 West Pender Street
Vancouver, British Columbia, Canada, V6C 2T8

For the dams:

UTM (Location):	<u>Approx. 376 500 E, 5 894 485 N</u> <u>(Coordinate grid is UTM (NAD83) Zone 10)</u>
Located at (Description):	<u>Blackwater Gold Project</u> <u>Plant Site Area – Sediment Control Pond and Infiltration</u>
Name of dam or description:	<u>Basins</u>
Dam function:	<u>Surface Water Management</u>
Owned by:	<u>BW Gold Ltd.</u>

Current project stage is:

(Check one)

- Feasibility design
- Detailed design
- Construction/operations

This is to advise that the undersigned is a supporting registered professional (SRP) retained by Knight Piésold Ltd. to carry out supporting professional services for the dam.

I undertook supporting professional services in the following:

(Check applicable sections)

- Bedrock/structural geology
- Surficial geology
- Geotechnical investigations
- Hydrogeology
- Seismotectonic investigations
- Other [preparation of site characterization letter report]

The undersigned hereby gives assurance that the supporting professional services indicated above and the documents prepared by this supporting registered professional for the project, including preparing the characterization letter report [Blackwater Gold Project – Plant Site Area and Sediment Control Pond – Site Characterization Summary, Ref. No. VA101-457/36, Cont. No.: VA22-00111, February 14, 2022], have been carried out in a manner that meets the intent of the applicable EGBC guidelines and good professional practice.

These professional services are described, and the results of them reported on in the documents prepared by me, or under my direct supervision, which bear my professional seal.

(With respect to field reviews, initial the following statements, as applicable. Leave blank those that are not applicable.)

- Field review(s) are not applicable
- Field review(s) are applicable:
- I have performed field review(s) for the services identified above.
 - Field review(s) have been performed by _____.

I confirm that I have communicated and liaised as required with the appropriate EGBC professionals for the purposes of my services.

I hereby give my assurance that I am an EGBC-registered professional.

Name: Daniel Fontaine, P.Eng.
<Original signed by>

Signature: _____ Date: February 14, 2022
Address: 1400-750 West Pender Street
Vancouver, British Columbia, Canada, V6C 2T8
Telephone: +1 (604) 685-0543
Email: dfontaine@knightpiesold.com



(If the EGBC professional is a member of a firm, complete the following:)

I am a member of the firm Knight Piesold Ltd. and I sign this letter on behalf of the firm.

APPENDIX B3

Supporting Registered Professional's Assurance Statement (JBC)

(Pages B3-1 to B3-2)

APPENDIX B3 - SUPPORTING REGISTERED PROFESSIONAL'S ASSURANCE STATEMENT OF PROFESSIONAL SERVICES

To: The Design Engineer Date: February 14, 2022

Name: Carlos Penate, P.Eng.

Address: 1400-750 West Pender Street
Vancouver, British Columbia, Canada, V6C 2T8

For the dams:

UTM (Location):	<u>Approx. 376 500 E, 5 894 485 N</u> <u>(Coordinate grid is UTM (NAD83) Zone 10)</u>
Located at (Description):	<u>Blackwater Gold Project</u> <u>Plant Site Area – Sediment Control Pond and Infiltration</u>
Name of dam or description:	<u>Basins</u>
Dam function:	<u>Surface Water Management</u>
Owned by:	<u>BW Gold Ltd.</u>

Current project stage is:

(Check one)

- Feasibility design
- Detailed design
- Construction/operations

This is to advise that the undersigned is a supporting registered professional (SRP) retained by Knight Piésold Ltd. to carry out supporting professional services for the dam.

I undertook supporting professional services in the following:

(Check applicable sections)

- Bedrock/structural geology
- Surficial geology
- Geotechnical investigations
- Hydrogeology
- Seismotectonic investigations
- Other [preparation of site characterization letter report]

The undersigned hereby gives assurance that the supporting professional services indicated above and the documents prepared by this supporting registered professional for the project, including preparing the characterization letter report [Blackwater Gold Project – Plant Site Area and Sediment Control Pond – Site Characterization Summary, Ref. No. VA101-457/36, Cont. No.: VA22-00111, February 14, 2022], have been carried out in a manner that meets the intent of the applicable EGBC guidelines and good professional practice.

These professional services are described, and the results of them reported on in the documents prepared by me, or under my direct supervision, which bear my professional seal.


(With respect to field reviews, initial the following statements, as applicable. Leave blank those that are not applicable.)

- Field review(s) are not applicable
- Field review(s) are applicable:
 - I have performed field review(s) for the services identified above.
 - Field review(s) have been performed by _____.

I confirm that I have communicated and liaised as required with the appropriate EGBC professionals for the purposes of my services.

I hereby give my assurance that I am an EGBC-registered professional.

Name: Joseph Cristobal, P.Eng.
<Original signed by> _____

Signature: 
Address: 1400-750 West Pender Street
Vancouver, British Columbia, Canada, V6C 2T8
Telephone: +1 (604) 685-0543
Email: jcristobal@knightpiesold.com

Date: February 14, 2022



(If the EGBC professional is a member of a firm, complete the following:)

I am a member of the firm Knight Piésold Ltd. and I sign this letter on behalf of the firm.



APPENDIX B

Plant Site Early Works Erosion and Sediment Control Engineering Work Ian

(Pages B-1 to B-32)

MEMORANDUM

Date:	January 26, 2022	File No.:	VA101-00457/36-A.01
		Cont. No.:	VA22-00058
To:	Alex Kourline		
Copy To:	Alastair Tiver, Alex Shepard, Shane Budd		
From:	Cyrus Niamir		
Re:	Plant Site Early Works Erosion and Sediment Control Engineering Work Plan		

1.0 GENERAL

This Engineering Work Plan (EWP) and the Issued for Construction (IFC) Drawings have been prepared to support tendering and construction activities for the Plant Site Early Works Erosion and Sediment Control.

The surface contact runoff from the Plant Site disturbance area will be collected by the Plant Site North and South Collection Channels. These channels will be located near the perimeter of the Plant Site and will convey surface contact runoff into the Plant Site Sediment Control Pond (SCP) located at the northeast corner of the Plant Site. The SCP is designed to provide temporary storage of surface contact runoff prior to discharge to the Rapid Infiltration Basins (RIBs). The RIBs are located downstream of the SCP and allow the outflow from the SCP to infiltrate into the surficial overburden layer.

2.0 IFC DRAWINGS

This EWP should be reviewed with reference to the IFC Drawings (the Drawings) listed in Table 2.1, which are included in Appendix A. An extension to the permit boundary has been applied for by BW Gold Ltd. (BW Gold). The previous boundary has been removed from the IFC drawings for clarity.

Table 2.1 IFC Drawings

Drawing Number	Drawing Revision	Drawing Title
G0006	Rev 1	Technical Notes
G0040	Rev 1	Construction Material Gradations
C3810	Rev 2	Erosion and Sediment Control Plan - Plant Site - General Arrangement - Phase 1 (Early Works)
C3811	Rev 2	Erosion and Sediment Control Plan - Plant Site - North Collection Channel - Plan and Profile
C3812	Rev 2	Erosion and Sediment Control Plan - Plant Site - North Collection Channel - Cross Sections
C3813	Rev 2	Erosion and Sediment Control Plan - Plant Site - South Collection Channel - Plan and Profile
C3814	Rev 2	Erosion and Sediment Control Plan - Plant Site - South Collection Channel - Cross Sections
C3815	Rev 2	Erosion and Sediment Control Plan - Plant Site - Sediment Control Pond - Plan and Sections
C3816	Rev 2	Erosion and Sediment Control Plan - Plant Site - Additional Sections and Details
C3820	Rev 0	Erosion and Sediment Control Plan - Plant Site - Sediment Control Pond Piping - Plan and Section
C3821	Rev 0	Erosion and Sediment Control Plan - Plant Site - Sediment Control Pond Piping Detail - Plan

3.0 BILL OF QUANTITIES

A bill of quantities for the Plant Site SCP, collection channels, and RIBs are attached in Table 1.

4.0 OPERATION AND MAINTENANCE

It is expected that after each storm event, some collected sediment will remain in the SCP and RIBs. This sediment shall be excavated or dredged to maintain functionality consistent with the design intent of the systems. The sediment removed from the SCP and RIBs will be used as fill material for the grading of the plant site, if appropriate or otherwise disposed within designated waste areas identified by BW Gold. Visual inspections of the sediment levels in the pond and the integrity of the collection channels, berms, discharge pipes and RIBs will be required after each significant rainfall event to identify if maintenance is required.

5.0 TECHNICAL SPECIFICATIONS

5.1 GENERAL

The Drawings are to be read in conjunction with the information provided in this EWP. The Drawings will take precedence in the case of a discrepancy. The Owner or its Constructor shall notify the Engineer upon any discovery of discrepancies between the Drawings, Technical Specifications, and the constructed work.

5.2 COMMUNICATION AND RESPONSIBILITIES

The parties with responsibilities for the construction of the work are as follows:

- Owner – refers to the BW Gold senior management group and technical services department.
- Constructor – refers to the entity responsible for constructing the work, including performance of Quality Control (QC) testing to confirm the work is in compliance with the Drawings and Technical Specifications. This could include the mine operations team of BW Gold and all contractors of BW Gold.
- Engineer – refers to the Design Engineer employed by Knight Piésold Ltd. (KP) or an employee or subconsultant nominated by KP working under the responsible charge of the Design Engineer. KP is responsible for preparation of the designs described herein and Quality Assurance (QA) of the work.

Typical project communications and quality documentation will include the following:

- Request for Information (RFI) – RFIs shall be used to request design clarification, substitution, or changes. RFIs are written by the Owner or Constructor and submitted to the Engineer. The Engineer will prepare a response to the RFI.
- Submittals - Submissions of relevant design information shall be prepared by the Owner and Constructor to verify that procured materials and equipment, QC plans and test results, and construction methods meet the design intent. These submittals may also include work plans (i.e. procedures and methods), as-built survey information, supplied material specifications (catalogues or QC test results), etc. Where appropriate, the Engineer will prepare a response to the submittal that will include either approval or required amendments.
- Non-Conformance Report (NCR) – The Engineer or Constructor can submit an NCR if a final product, material or construction method deviates from the IFC Drawings, Technical Specifications, or other approval. The NCR shall identify the non-conformance, provide an explanation and if possible, suggest remedial actions. No work is to continue until the non-conformance has been resolved.

- Subgrade Inspection Record (SIR) – An SIR will be prepared following inspection of the subgrade of any work where subgrade approval is required. The SIR will document the conditions of the subgrade and will provide approval for the commencement of fill placement or required remedial actions.

5.3 CONSTRUCTION DEWATERING

The Constructor shall build, maintain, and operate all ditches, sumps, and other temporary diversion and protection works needed to divert surface water through or around the construction site and away from the construction work while construction is in progress. Storm runoff from disturbed areas shall discharge to the appropriate collection control facilities for retention of surface water runoff as described in Section 7.0. Construction dewatering activities shall be performed as follows:

- Provide and maintain, at all times during construction, proper equipment and facilities to promptly and adequately remove and dispose of all water entering excavations. Maintain foundation conditions until backfilling operations have been completed to such an extent that the placed material will not be damaged by allowing water levels to return to natural elevations.
- Conduct dewatering, at all times, in such a manner to preserve the natural undisturbed capacity of the subgrade soils at the bottom of excavations. Evaluate the impact of the anticipated subsurface soil/water conditions on the proposed method of excavation and removal of water.
- Operate the dewatering system until the excavation is adequately backfilled. Provide for continuous system operation when necessary. Arrange for standby pumps and appropriate backup power if electrical power is the primary energy source for a dewatering system.
- Monitor operations to verify that the system(s) lower the groundwater levels at a rate required to maintain a dry excavation resulting in a stable subgrade for inspection and backfill.
- Collect water entering the excavation from precipitation or surface runoff in shallow ditches around the perimeter of the excavation. Collect and pump from the excavation to maintain a dry bottom with no standing water.
- Dispose of water in an approved area so that backflow or site discharge does not occur.

5.4 CLEARING, GRUBBING, REMOVAL OF TOPSOIL AND UNSUITABLE MATERIALS

The Constructor shall clear and grub all ground surfaces to the limits shown on the IFC Drawings. In order to minimize erosion and contamination of the surface runoff, clearing and grubbing shall be performed only as and when required to enable each portion of the work to be carried out.

The work area will shall be logged and cleared of timber prior to commencing construction. Clearing in the work area shall not be commenced until the project boundaries are surveyed in the field and confirmed. Grubbing of the work area shall consist of the complete removal of all vegetation and organic matter and grubbing to remove all roots and stumps. All roots over 50 mm in diameter, protruding from the ground surface, shall be grubbed to a depth of 300 mm below the ground surface. Pieces of wood less than 75 mm in diameter and 1,000 mm in length may be scattered within the clearing limits and will be incorporated with the topsoil during topsoil stripping operations.

After an area has been cleared and grubbed and the debris removed, the Constructor shall remove the topsoil and/or unsuitable materials and either windrow or stockpile this material in designated areas identified by the Owner. The Constructor will be required to remove and stockpile all the available topsoil from disturbed areas shown on the Drawings for later use in reclaiming the site. Topsoil is described as a dark brown organic layer that ranges in thickness from approximately 150 mm to over 2,000 mm in some parts of the project area. Unsuitable material will generally be comprised of saturated soils or fill materials

which when compacted, do not achieve the required density. The material is to be stockpiled in a neat workmanlike manner in the designated areas such that it will be stable and protected from erosion.

After removal of topsoil and/or unsuitable material in a work area and before any additional work is undertaken:

- The Engineer shall inspect the area to determine whether removal of topsoil material has been completed satisfactorily.
- An as-built survey will be performed by the Constructor in order to verify topsoil quantities removed and stockpiled.

5.5 EXCAVATION AND FOUNDATION PREPARATION

Excavation

The Constructor shall develop excavation methods, techniques and procedures with due consideration regarding the nature of the materials to be excavated and shall take such precautions as are necessary to preserve, in an undisturbed condition, all materials outside the lines and grades shown on the Drawings. The Constructor shall be permitted to carry out excavation and shaping of the foundations by whatever method it considers most suitable, providing it is consistent with producing an acceptable result consistent with the design intent as determined by the Engineer. The Owner and Constructor shall be solely and completely responsible for the safety, stability, maintenance, support and protection of all excavations. The Constructor shall supply, install and provide all temporary supports, bulkheads, canopies, sheeting and bracing, divert surface water, remove water from the excavations, and shall provide and maintain such drainage and pumping facilities as are necessary to stabilize and protect the excavations. Except as otherwise instructed by the Engineer, such temporary support and facilities shall be removed by the Owner or Constructor on completion of the work.

The Constructor shall not excavate beyond the lines and grades shown on the Drawings without the prior approval of the Engineer. Material from the excavations, which meets, or can be processed to meet, the specifications of the construction materials, shall be either stockpiled for later use, or used directly for construction of the work. Excavated materials not suitable for use in construction shall be disposed of in designated disposal areas identified by the Owner.

Subgrade Preparation for Fill Placement

Foundation preparation of any surface that is to receive fill and from which topsoil, unsuitable material or temporary cover has already been removed shall consist of trimming and levelling to a consistent surface suitable for fill material. Proof rolling, with a minimum of 4 passes of a smooth drum or sheepsfoot drum vibratory roller, may be required by the Engineer to produce a well compacted, smooth or roughened surface depending on the design intent of the structure and conditions observed during the subgrade inspection. Roller specifications are further discussed in Section 5.8. Placing of fill materials on excavated surfaces shall not commence until the preparation of the surfaces has been approved in writing by the Engineer.

Subgrade Preparation for Geosynthetics and Pipework

Subgrade surfaces prepared for placement of overlying geosynthetics or pipework shall be trimmed and dressed to form a surface that is firm, dry, smooth and free of projections of sharp rock fragments that could puncture or damage the overlying materials. The surfaces shall be rolled with a smooth drum vibratory roller to bed gravel particles into the soil matrix.

Particles not bedded during the rolling process shall be removed by raking, brooming, and/or hand-picking rocks from the surface. Any holes, depressions or rough areas created during this process shall be filled with suitable fill material free of sharp rock fragments meeting the design specifications. The surface must then be rolled again.

Placing of geosynthetics or pipeworks on excavated surfaces shall not commence until the preparation of the surfaces has been approved in writing by the Engineer.

Subgrade Inspection

The Constructor shall notify the Engineer when the excavation and subgrade preparation is complete to the design lines and grades and ready for inspection. The Engineer will inspect the area and provide approval for continued construction or specify the required remedial actions to complete prior to placement of fill, geosynthetics, and/or pipeworks.

Inspection requirements for subgrade surface preparation include:

- An as-built survey will be collected by the Constructor and submitted to the Engineer to verify that the design lines and grades were achieved.
- The Engineer shall inspect the area to determine whether subgrade preparation was completed satisfactorily.
- The Engineer will prepare a SIR documenting the subgrade conditions observed during the inspection.

5.6 EARTHWORKS AND EARTHFILL PROPERTIES

Earthfill material gradations, placement and compaction specifications are shown on Drawing G0040. QC testing requirements are included in Section 5.11. General requirements for earthworks construction are as follows:

- Correct and complete clearing and grubbing
- Correct and complete removal and stockpiling of topsoil
- Achievement of design lines and grades
- Drainage and diversion of surface runoff and groundwater
- Stability of excavations and stockpiles
- Foundation approvals before covering with fill materials
- Identification of suitable materials in local excavations, borrow areas and stockpiles
- Procurement of suitable materials from outside sources
- Planning and haul patterns for transportation of materials
- Placement of the specified fill materials
- Compaction of specified fill materials
- Testing of specified fill materials

Fill materials shall be durable and shall not, except as otherwise specified, contain more than a small proportion of thin, flat, or elongated particles. They shall also be free of topsoil, organics, and other deleterious material. Except as otherwise specified, the particles shall be hard and resistant to breakdown during handling. Fill materials that will be required for construction of the work are as follows:

- Zone S - Constructed from low permeability glacial till. The material will consist of well graded silty sand with some gravel and will generally require no processing except for the removal of oversized particles.

- Zone F - Constructed with clean, fine to coarse sand. This material will be processed non-reactive fluvial materials from approved sources.
- Zone C - Constructed with random fill comprising non-reactive waste rock and overburden.
- Riprap Bedding - Processed quarry rock supplied by rock excavation or from approved outside sources. Riprap bedding will be placed under riprap in select locations.
- Riprap - Processed quarry rock supplied by the rock excavation or from approved outside sources. Riprap will be placed in ditches and ponds where erosion protection is required, and rock foundations are not encountered during excavation. Riprap shall be placed and not dropped to avoid damaging geotextile.

5.7 FILL PLACEMENT

The Constructor shall develop procedures for placing fill as shown on the Drawings and provided in these Technical Specifications. No fill materials shall be placed in embankments, berms or trenches until foundation preparation in the fill area has been completed and approved in writing by the Engineer. The Constructor shall construct the work only with materials meeting the specified requirements or approved equivalents. The fill material shall be free from lenses, pockets and layers of materials that are substantially different in gradation from the surrounding material in the same zone.

Fill material shall be excavated, transported, placed, and spread in such a manner that segregation is avoided. The equipment used for placing fill shall be such that it does not cause segregation of the material. Fill shall be placed and spread in such a manner that no gaps are left between adjacent placed loads of materials. The work shall be constructed by placing, spreading, and, where required, compacting the specified fill material in continuous lifts of the specified thickness. The fill shall be levelled prior to compaction using a dozer or grader to obtain a smooth surface free from depressions. The surface of each lift shall be sloped only at such grades as are necessary to maintain adequate surface drainage at all times.

Any material placed which does not meet the specified requirements shall be removed or remixed, blended, disked, or otherwise reworked by the Constructor to produce a material that meets the specified material requirements. If a non-conforming material has been placed upon by additional fill materials, it is the responsibility of the Constructor to excavate and replace the non-conforming and affected conforming materials, unless otherwise approved by the Engineer.

The Owner or its Contractor shall exercise particular care in fill placement for trench backfill or working near pipes, valves, instrumentation, or structures to avoid damage to the work. Fill shall not be placed against concrete until a minimum of 7 days have elapsed after concrete placement.

In fills that require moisture conditioning, the Constructor shall condition the material to the moisture content designated by the Engineer. The Constructor shall adopt all measures necessary to achieve moisture content within one percent of the specified moisture content, distributed uniformly throughout the layer of material being placed, prior to compaction. Wherever necessary, after a layer of fill has been placed, the moisture content of the fill material shall be modified to maintain the fill material within the range specified. If after placing, spreading and levelling any fill material becomes too wet for proper compaction as determined by the Engineer, it shall be either removed or the moisture content reduced to a value acceptable to the Engineer by scarification or other approved methods. Suitable disc harrows or other approved equipment shall be available for use if required. Equipment used by the Constructor to apply water to fill material shall be designed to apply water uniformly and at sufficient rates to achieve the designated moisture content. Water tank trucks shall be equipped with positive shut-off valves so that there

is no leakage from the nozzles when the equipment is not operating. In the event that leaks do occur, they shall be repaired immediately. Moisture conditioning shall be carried out in a manner that will avoid flow of water between different material types.

Fill Placement During Freezing Conditions

The Constructor will be permitted to place fill materials in freezing conditions only if the materials can be placed and compacted to the specified densities that would normally be achieved if freezing conditions did not prevail. Criteria for placing fill materials during freezing conditions are summarized below.

- (i) All ice and snow and loose frozen fill materials shall be removed from compacted fill surfaces or prepared foundations prior to placing any new fill materials.
- (ii) Fill materials can be placed on previously placed and compacted frozen fill or approved frozen foundations provided that the surfaces are cleaned as per (i) above.
- (iii) Where the previous compacted surface of any layer is too smooth to bond properly with the succeeding layer it shall be scarified or otherwise roughened to provide a bonding surface before the next layer is placed.
- (iv) Only non-frozen fill can be used as fill. Frozen soils shall be removed from the borrow areas prior to excavation of non-frozen fill materials. Fill materials must meet the specified moisture content criteria before excavation in the borrow areas and before placement in the work area.
- (v) The fill materials shall be immediately spread, compacted, and tested after placement to achieve the specified density before the material freezes.
- (vi) Fill placement and compaction should occur rapidly and in relatively small areas. The exposed surfaces shall be kept to a minimum so as to minimize the potential for fill materials to become frozen before they are compacted to the specified densities.
- (vii) Any fill materials that become frozen prior to adequate compaction shall be removed to spoil.
- (viii) Fill materials shall not be placed when there is any accumulation of snow or ice on surfaces to be covered by the succeeding layers of fill.

5.8 COMPACTION

All fill material, after placing, spreading, and levelling to the appropriate lift thickness, shall be compacted in accordance with the requirements presented herein, and to the requirements specified on the Drawings. Compaction of each lift of fill shall proceed in a systematic, orderly, and continuous manner such as to ensure that no part of the lift is left uncompacted. The compaction shall be carried out by routing the compaction equipment parallel to the axis of the embankment or berm. When such routing is impractical, the compaction equipment may be routed in any direction provided that all of each lift receives the compaction specified. These measures may be taken at the lower elevations of the fill, in areas adjacent to concrete, and in trenches. The rolling pattern at all zone boundaries or construction joints shall be such that the full number of roller passes required in one of the adjacent zones or on one side of the construction joint extends completely across the boundary or joint. Should the surface of the fill become rutted or uneven subsequent to compaction it shall be re-graded and re-compacted by the Constructor, before the next layer of fill is placed. All large particles that interfere with compaction shall be removed from the zone in which they were placed, either prior to or during compaction.

If the Constructor wishes to use alternative equipment, it shall submit to the Engineer for approval complete details of such equipment and the methods proposed for its use. Unless otherwise approved by the Engineer, all fill material shall be compacted using the following specified equipment:

- (i) Smooth Drum and Sheepsfoot Drum Vibratory Rollers:
- Smooth drum and sheepsfoot drum vibratory rollers shall be equipped with a suitable cleaning device to prevent the accumulation of material on the drum during rolling. Each roller shall have a total static weight of not less than 10 tonnes at the drum when the roller is standing on level ground. The drum shall be not less than 1.5 metres in diameter and not more than 2.2 metres in width. The vibration frequency of the roller drum during operations shall be between 1,100 and 1,500 vibrations per minute and the centrifugal force developed by the roller at 1,250 vibrations per minute shall not be less than 18 tonnes.
 - The power of the motor driving the vibrator shall be sufficient to maintain the specified frequency and centrifugal force under the most adverse conditions that may be encountered during compaction of the fill. Propulsion equipment for the roller shall be adequate to propel the roller at speeds up to 6 km/hr.
 - A minimum overlap of 300 mm shall be maintained between the surfaces traversed by adjacent passes of the roller drum. The roller shall be propelled at 3 km/hr during compaction.
- (ii) Hand Guided Vibratory Compactors:
- The Constructor shall use hand guided vibratory compactors to compact fill in trenches, around structures and in other confined areas which are not accessible to larger equipment. Such compaction shall be capable of compacting the material to an equivalent density as that achieved by the larger vibratory roller.

The Constructor shall take every precaution when operating compaction equipment to avoid damage to adjacent structures, and to avoid disturbing the foundation. Any such damage or disturbance shall be repaired or remedied by the Constructor at their own expense.

5.9 GEOTEXTILE PROPERTIES

Geotextile shall be packaged and shipped in standard roll lengths and widths. It shall be kept dry and wrapped such that it is protected from the elements during shipping and storage. Geotextile will comprise non-woven needle punched synthetic fibre fabric supplied in rolls and composed of polypropylene with inhibitors added to base plastic to resist deterioration by ultraviolet light and heat. The minimum required geotextile properties are presented in Table 5.1 below:

Table 5.1 Geotextile Properties

Property	Minimum Value Required	Standard
Grab Strength	1,400 N	ASTM D4632
Puncture Strength	3,510 N	ASTM D6241
Elongation at Break	50 %	ASTM D4632
Tear Strength	500 N	ASTM D4533
Permeability	0.8 s ⁻¹	ASTM D4491
Apparent Opening Size	150 microns	ASTM D4751

The surfaces underlying the geotextile shall be approved by the Engineer and shall be smooth and free of ruts or protrusions which could damage the geotextile. The geotextile shall be laid flat and smooth so that it is in direct contact with the subgrade. The geotextile shall be free of tensile stresses, folds and wrinkles so that the overlying materials will not excessively stretch or tear the fabric. On slopes steeper than 10H:1V, the geotextile shall be laid with the machine direction of the fabric parallel to the slope direction. Anchoring

of the terminal ends of the geotextile shall be accomplished using key-in trenches or aprons at the crest and toe of slope.

Successive sheets shall be overlapped in such a manner that the upstream sheet is placed over the downstream sheet and/or the upslope over the downslope. The overlying material placement shall begin at the toe and proceed up the slope. Riprap shall be placed carefully and not be dropped from a height exceeding one meter.

5.10 PIPEWORK AND APPURTENANCES

All materials furnished by the Constructor shall be new, suitable and the best of their respective kind and shall be subject to approval by the Engineer. They shall comply with the latest applicable standards for:

- American Society for Testing and Materials (ASTM)
- American Water Works Association (AWWA)
- American Society of Mechanical Engineers (ASME)

Any contradictions between standards shall be submitted to the Engineer for review.

Pipe, fittings, valves, and other appurtenances shall be loaded and unloaded by lifting with hoists in such a manner as to avoid damage or hazard. Under no circumstances shall the pipe or pipe fittings be dropped to the ground or into trenches. Pipe shall not be skidded or rolled against pipe already on the ground. The interior of all pipes, fittings and valves shall be kept free from dirt and foreign material at all times.

Pipe shall be made of High-Density Polyethylene (HDPE), which shall be in accordance with ASTM D3350, ASTM F714, ASTM F2206 and ASTM F2619. All piping is to be installed to the minimum pipeline pressure rating. Installation of HDPE pipework shall be in accordance with AWWA M55 requirements and the manufacturer's specifications.

Joining of HDPE pipe shall be butt fusion as per ASTM F2620. Butt fusion joined pipes shall not be misaligned by more than ± 3 mm. Gaskets are to be used for all flanged joints and the gaskets shall be centered accurately in the joint. Bolts, studs, and nuts to be installed and tightened as per manufacturer's instructions for any flanged joints.

Where perforations are specified, they shall be circular and arranged in symmetrical rows parallel to the axis of the pipe. Perforation hole diameters to be at minimum 10 mm and at maximum 15 mm.

Pipework shall be laid to the maximum extent, in long lengths as to minimize the number of joints required. The Constructor shall develop methods to avoid damage to piping during installation or backfilling. The pipe foundation shall be inspected prior to laying of the pipe and the pipe will not be placed on timber or rock outcrops that can cause stress concentrations. Placement of the HDPE pipe shall be sequenced to protect all pipework from damage due to vehicle and equipment traffic. Barricades and flagging shall be installed so that towers are visible to vehicle and equipment traffic.

The Constructor shall construct the pipework to the lines and grades as shown on the Drawings, maintaining a negative grade on the pipeline to prevent pooling and/or air pockets. Survey control shall be maintained on all aspects of the work and all locations shall be verified prior to commencement of construction.

5.11 QUALITY CONTROL

The Constructor shall be responsible for QC of the work and perform the following tasks:

- Samples of fill materials are to be collected and tested to confirm the earthfill properties of the fill materials as described in Section 5.6.
- Visual inspection and verification of lift thicknesses as described in Section 5.7.
- Field density tests on the compacted fill and any other tests considered necessary to ascertain that the fill being placed or already placed meets the specified requirements.

The results of the tests carried out by QC personnel will be final and conclusive in determining compliance with the Technical Specifications and the Drawings. Notwithstanding any QC testing, the Constructor shall be responsible for performing such tests as are necessary to control the quality of the materials prior to delivery to, and after incorporation in the fill.

The Constructor shall render such assistance as is necessary to enable such sampling and testing to be carried out expeditiously. Samples for QC testing will be excavated and collected by the Constructor. Sample pits excavated for quality purposes shall be backfilled and compacted by the Contractor using fill material similar to that excavated and compacted, at no extra charge. The Constructor shall allow sufficient time for QC and QA personnel (described in Section 6.3) to conduct the required test work in order to determine the acceptability of each lift. Performing the tests or the time taken to interpret their results shall not constitute grounds for a claim by the Constructor for additional compensation or an extension of time.

Tests carried out by QC and QA personnel will be performed in accordance with the principles and methods prescribed by the American Society for Testing and Materials (ASTM) and other such recognized authorities with such methods being modified, if necessary, to take into account local conditions and materials containing large particle sizes.

QC testing for the purposes defined above will be as follows:

- Control tests on samples of fill materials taken from the borrow areas and stockpiles prior to placement and compaction.
- Record tests on fill materials after placement and compaction.

All fill materials as well as fill beneath and around structures or pipework, must meet the specified gradations and placing requirements. The minimum control testing frequencies for earthworks materials are provided in Table 5.2. The minimum record testing frequencies for earthworks materials are provided in Table 5.3.

Table 5.2 Minimum Control Testing Frequency

Material	Control Tests (1 per / X m ³)		
	C1	C2	C3
Zone C	500	500	-
Zone F	25	25	-
Zone S	250	250	250
Riprap Bedding	50	50	-
Riprap	Visual Inspection		

Note(s):

1. C1 – Particle Size Distribution (ASTM D422).
2. C2 – Optimum Moisture Content (ASTM D2216).
3. C3 – Standard Proctor (ASTM D698).

Table 5.3 Minimum Record Testing Frequency

Material	Record Tests (1 per / X m ³)				
	R1	R2	R3	R4	R5
Zone C	500	500	-	-	-
Zone F	25	25	-	-	-
Zone S	250	250	250	250	250
Riprap Bedding	50	-	-	-	-
Riprap	Visual Inspection				

Note(s):

1. R1 – Particle Size Distribution (ASTM D422).
2. R2 – Optimum Moisture Content (ASTM D2216).
3. R3 – Standard Proctor (ASTM D698).
4. R4 – Field Density by Nuclear Methods (ASTM D2922).
5. R5 – Field Moisture Content (ASTM D2216).

As part of the inspection requirements, the Engineer shall be responsible for performing QA and properly documenting any issues or concerns noted during inspections. The role of QA is detailed in Section 6.

5.12 SUBMITTALS

Submittals to the Engineer include but are not limited to the following:

- RFIs
- Work Plans (Procedures and Methods)
- Supplier Material Specifications (Catalogues or QC tests)
- QC Test Results and Reports
- As-Built Surveys

6.0 QUALITY ASSURANCE

6.1 REVIEW OF QC TESTING

All of the test results derived from QC testing are to be reviewed by QA personnel as they become available. QA personnel will carry out spot checks to verify the accuracy of the data and will carry out an independent analysis of test results as necessary for QA purposes. This review will be used to summarize the following:

- Conformance of the materials and workmanship with the Technical Specifications and the Drawings.
- Identification of any non-compliant test results and trends with respect to compliance over time.
- At the completion of work, the Contactor will provide a QC summary of all results as part of any approval request.

During QA inspections, any quality issues detected shall be communicated to QC personnel on site so that appropriate corrective actions can immediately be taken before the work results in a non-conformance. If the QC testing identifies samples that do not comply with the requirements of the Technical Specifications and the Drawings and if subsequent re-testing confirms this, then appropriate corrective measures shall be taken. This may include removal of the non-compliant materials, developing modifications to the construction procedures and/or reviewing the design objectives for the particular material. Any requested

modifications to the Technical Specifications and/or the Drawings shall be submitted as a RFI to the Engineer for review and approval.

6.2 MATERIAL SUBSTITUTIONS

All "equal/equivalent" materials shall be approved by the Engineer in advance of their use. QA personnel will review each request with regards to the requirements of the Technical Specifications, the Drawings and the design objectives for the material, and the request will be forwarded to the Engineer for approval.

As soon as reasonably possible, the Engineer will inform the Owner or Constructor in writing of the acceptance or rejection of the proposed "equal/equivalent" material. In the case of rejection, the reasons will be clearly stated.

6.3 INDEPENDENT TESTING

From time to time, the Engineer may request that additional independent testing be carried out on selected items of the work to verify that the intent of the designs is being met. QA personnel will arrange for such testing to be carried out and coordinate with the Owner and Constructor for access to appropriate aspects of the work.

7.0 SEDIMENT AND EROSION CONTROL STRATEGIES

7.1 GENERAL

Construction of the work is expected to adhere to the Surface Erosion Prevention and Sediment Control Plan (KP, 2021) which was developed based on the recommendations by the Ministry of Energy, Mines and Low Carbon Innovation (EMLI formally EMPR, 2020). The relevant best management practices (BMPs) associated with the plant site early work activities have been extracted from this plan and are presented below as reference.

Erosion control BMPs reduce erosion by stabilizing exposed soil or by reducing surface runoff flow velocities. There are generally two types of erosion control BMPs:

- Source control BMPs for protection of exposed surfaces
- Conveyance BMPs for control of runoff

Descriptions of BMPs to be used at the site are provided below. Typical BMP figures are attached in Appendix B.

7.2 BEST MANAGEMENT PRACTICES

Construction Water Management

Diversion ditches are constructed upgradient of disturbed areas to intercept clean surface water runoff and convey it around areas to be disturbed to avoid excessive sheet flow. All diversion ditches should discharge through a stabilized outlet designed to handle the expected runoff velocities and volumes from the ditch without scouring. Each diversion ditch type should provide a minimum freeboard of 0.5 m between the top of flow and the ditch crest.

Collection ditches intercept contact water runoff from disturbed areas and divert it to stabilized areas where it can be effectively managed. Collection ditches are used within construction areas to collect runoff and convey it to appropriate sediment control measures. Where fine grained soils are exposed, appropriate

erosion protection materials shall be installed based on the estimated magnitude of flow and the flow velocity. General locations and conditions may include:

- Below disturbed slopes to divert sediment-laden water to control facilities.
- At or near the perimeter of the construction area to prevent sediment-laden runoff from leaving the site.
- Below disturbed areas before stabilization to prevent erosion if stabilization measures cannot be implemented immediately.

Rock Check Dams

Rock check dams are small dams constructed across ditches, and waterways to avoid erosion by reducing flow velocity. Rock check dams accomplish this by interrupting the flow of water to form small ponds, thereby flattening the surface of the water, and reducing the velocity of flow. The obstructions induce infiltration and reduce erosion potential. Check dams are also used to distribute flows across a swale to avoid preferential paths and guide flows towards vegetation.

Rock check dams require regular maintenance and shall be inspected regularly, and before and after every large storm event. It is important that rubble, litter, and leaves are removed from the upstream side of the dam. This is typically done when the sediment has reached a height of one-half of the original height of the dam.

Sediment Basins

A sediment basin is a temporary structure that is used to detain runoff from small drainage areas so that sediment can settle out. The basin is typically maintained until the site is permanently protected against erosion by vegetation and/or structures. Sediment basins are generally located in areas where access can be maintained for sediment removal and proper disposal. Sediment basins are typically constructed at the end of collection ditches to detain sediment-laden runoff long enough to allow the majority of the sediment to settle out to comply with water quality objectives. A sediment basin can be created by excavating a basin, utilizing an existing depression, or constructing a dam on a slight slope downward from the work area. Sediment-laden runoff from the disturbed site is conveyed to the basin via ditches or diversion structures. The efficacy of sediment basins is largely dictated by the extent to which they are properly sized and constructed as designed; whether the banks are stabilized immediately following construction; and the extent to which they are regularly cleaned out / maintained.

Stream Diversion Structures

A temporary diversion structure consists of sandbags stacked in a pyramid formation with a polyethylene sheet placed diagonally in between. Temporary diversion structures are useful for diverting streams and/or concentrated overland flows to an appropriate sediment basin or other BMP where it can be effectively managed.

Vegetation Management and Re-vegetation

Natural vegetation is one of the best and most cost-effective methods of reducing the potential for erosion and sedimentation. Vegetation keeps soil secure and ground cover reduces raindrop velocities. In order to preserve vegetation, a “no-entry” vegetation buffer shall be maintained to prevent excess clearing, particularly around water bodies, prior to clearing vegetation from surrounding areas. If preserving natural vegetation is not a viable option, cleared areas that will not include infrastructure shall be re-vegetated as soon as practical after construction activities have ended.

Mulching

Mulching is the application of a uniform protective layer of straw, wood fiber, wood chips, or other acceptable material on or incorporated into the soil surface of a seeded area to allow for the immediate protection of the seed bed. The purpose of mulching is to protect the soil surface from the forces of raindrop impact and overland flow, foster the growth of vegetation, increase infiltration, reduce evaporation, insulate the soil, and suppress weed growth. Mulching also helps to hold fertilizer, seed, and topsoil in place in the presence of wind, rain, and runoff, and reduces the need for watering. Mulching may be utilized in areas that have been seeded either for temporary or permanent cover.

There are two basic types of mulches: organic mulches and chemical mulches. Organic mulches likely to be used include straw, hay, wood fiber, wood chips, and bark chips. This type of mulch is usually spread by hand or by machine (mulch blower) after seed, water, and fertilizer have been applied. Chemical mulches, also known as soil binders or tackifiers, are composed of a variety of synthetic materials. Chemical mulches are usually mixed with organic mulches as a tacking agent to aid in the stabilization process, and are not used as mulch alone, except in cases where temporary dust and erosion control is required. The choice of materials for mulching shall be based on soil conditions, season, type of vegetation, and the size of the area.

Rolled Erosion Control Products

Rolled Erosion Control Products (RECPs) are geosynthetic or organic materials composed of two layers of coarse mesh that contain a central layer of permeable fibres in between. These products take the form of flexible sheet materials that are often composed of organic materials that decompose over time. When intended for long-term use, RECPs are made from UV-stable synthetics such as polypropylene.

RECPs are used to cover un-vegetated cut or fill slopes in order to provide erosion control when seeding or mulching alone is unsuccessful. RECP sheets shall be anchored with special stakes or rocks and shall be in direct, tight contact with the soil surface in order to perform effectively.

Slope Roughening

Cut and fill slopes are roughened with tracked machinery or by other means, to reduce runoff velocity, increase infiltration, reduce erosion, and to aid in the establishment of vegetative cover with seed. Roughening is typically carried out by a tracked machine moving up and down the slope, creating undulations on the soil surface. This procedure is simple, inexpensive, and provides immediate short-term erosion control for bare soil, where vegetative cover is not yet established. Compared to hard, compacted smooth surfaces a rough soil surface provides more favorable moisture conditions, which will aid in seed germination. Slope roughening works best on flat to moderately sloped areas.

Filter Bags

Filter bags are generally constructed from a sturdy non-woven geotextile capable of capturing particles larger than 150 microns. Filter bags are installed at the discharge end of pumped diversion pipelines, via fabric flange fittings, to remove fine grained materials before discharging to the environment, as needed. Filter bags are generally temporary sediment control measures. Filter bags are installed on flat, stable, non-erodible foundations, or in well vegetated areas. The pumping rate is specified by the manufacturer. Discharge from filter bags is routed to avoid erosion.

A smaller variety of filter bags, referred to as filter socks, can be installed on the discharge ends of gravity flow pipes, such as slope drains, to filter silt particles before discharging to the environment. Filter bags

shall be inspected daily for defects, rips, tears, sediment accumulation, and erosion of the surrounding area. When sediment fills one-half of the volume of the filter bag, the filter bag shall be removed from service and replaced. Spare bags shall be kept nearby to minimize time required to recommence pumping activities. Once the used bag is fully drained, the bag and its contents can be disposed of as solid waste.

Waterbars

Waterbars are ridges or ridges and channels constructed diagonally across a sloping road or right-of-way to limit the accumulation of erosive volumes of water at pre-designed intervals. Waterbars reduce sheet flow and surface erosion of areas of exposed soil and/or roads by diverting runoff toward a stable vegetated area or diversion ditch. Spacing of waterbars shall be field-fit based on slope grade, general erodibility of the surface, and anticipated flows. Waterbars should not direct runoff into a ditch that channels water toward a watercourse unless the ditch is adequately designed with check dams and armoring where appropriate.

Silt Fencing

Silt fencing is a perimeter control type BMP used to intercept sheet flow runoff and used in conjunction with other BMPs. Typical silt fencing comprises a geotextile fabric anchored to posts driven into the ground. Silt fencing promotes sediment control by filtering water that passes through the fabric and increases short term retention time, allowing suspended sediments to settle.

Silt fences shall be placed parallel to slope contours to maximize ponding efficiency when required. Barrier locations are informally chosen based on site features and conditions (e.g., soil types, terrain features, sensitive areas, etc.), design plans, existing and anticipated drainage courses, and other available erosion and sediment controls. Typical barrier sites are catch points beyond the toe of fill or on side slopes above waterways or drainage channels. Silt fences shall not be used for wide low-flow, low-velocity drainage ways, for concentrated flows, in continuous flow streams, for flow diversion, or as check dams. Silt fencing shall be installed in backfilled trenches for proper anchoring.

All silt fences shall be inspected and maintained, as required, following major rainfall events. Proper installation and frequent maintenance are required for effective sediment control.

Straw Bales

A straw bale barrier consists of straw bales placed end to end along a level contour in a channel and then staked to hold them in place. The straw bale barrier detains and filters stormwater runoff, creating a small pond behind the barrier where sedimentation occurs. Straw bales, along with silt fences, significantly reduce sediment accumulation in sediment control ponds and basins.

7.3 MONITORING

The success of the erosion and sediment control mitigation is dependent on monitoring of implemented BMPs. The contractor and environmental monitoring technicians should inspect all erosion control measures periodically and after each significant runoff-producing rainfall event. BMPs shall be visually inspected for the following:

- Excess sediment build-up
- Structural/physical integrity
- Visible wear and tear

Sediment removal and proper disposal shall be performed as required.

Yours truly,
Knight Piésold Ltd.



<Original signed by>

Prepared: 2022-01-26
Cyrus Niamir, P.Eng.
Senior Engineer

Reviewed: _____
Carlos Penate, M.Eng., P.Eng.
Senior Engineer

Approval that this document adheres to the Knight Piésold Quality System:

DDF

Attachments:

Table 1 Rev 0	Updated Material Take-offs
Appendix A	Plant Site Early Works Sediment Pond IFC Drawings
Appendix B	Sediment and Erosion Control BMP Figures

References:

Knight Piésold Ltd. (KP, 2021). Early Works Erosion and Sediment Control Plan. February 4, 2021. Vancouver, British Columbia. Ref No: VA101-457/33-11 Rev 1.

/cbn

TABLE 1

BW GOLD LTD.
BLACKWATER GOLD PROJECT

PLANT SITE EARLY WORKS EROSION AND SEDIMENT CONTROL
UPDATED MATERIAL TAKE-OFFS

Print Jan/26/22 9:57:40

Item		No.	Length (m)	Diameter (mm)	Area (m ²)	Volume (m ³)	Notes	
Plant Site North Collection Channel (PSNCC) and Plant Side South Collection Channel (PSSCC)	Fill (Zone C)	-	-	-	-	4,410		
	Cut	-	-	-	-	2,460		
	Riprap	-	-	-	-	1,410	D ₅₀ = 200mm	
	Geotextile	-	-	-	5,080	-		
Sediment Control Pond (SCP)	Fill (Zone C)	-	-	-	-	3,730		
	Cut	-	-	-	-	5,230		
	Liner	0.6 m Thick Fill (Zone S)	-	-	-	-	1,870	
		0.5 m Thick Fill (Zone C)	-	-	-	-	1,560	
		Geotextile	-	-	-	3,110	-	
	Inlet	Riprap	-	-	-	-	210	D ₅₀ = 565mm
			-	-	-	-	50	D ₅₀ = 150mm
	Outlet	Geotextile	-	-	-	170	-	
		Riprap	-	-	-	-	140	D ₅₀ = 565mm
	Geotextile	-	-	-	290	-		
Rapid Infiltration Basins (RIBs)	Pipe, DR17 HDPE, Plain End Connected ^{1,2}	1	140	200	-	-		
	Pipe, DR17 HDPE, Perforated, Plain End Connected ^{1,2}	1	60	200	-	-		
	Tee, DR17 HDPE, Fabricated, Plain End Connected ^{1,2}	5	-	200	-	-		
	90° Elbow, DR17 HDPE, Fabricated 3-Segment, Plain End Connected	8	-	200	-	-		
	22.5° Elbow, DR17 HDPE, Fabricated 2-Segment, Plain End Connected	8	-	200	-	-		
	Cross, DR17 HDPE, Fabricated, Plain End Connected	4	-	200	-	-		
	Gate Valve, Class 150, Raised Face, Flange Connected, Handwheel Operated	1	-	200	-	-		
	Flange Adapter, DR 17 HDPE, c/w Ductile Iron Back-up Ring and Gasket	12	-	200	-	-		
	Blind Flange, HDPE	2	-	200	-	-		
	Fill (Zone C)	-	-	-	-	-	4,490	
	Cut	-	-	-	-	-	360	
	Sand (Zone F)	-	-	-	-	-	45	

\\KPL\VA-Prj\1101\00457135\A\Correspondence\VA22-00058 - Plant Site Early Works Erosion and Sediment Control EWP\Table 1 - Plant Site Early Works Erosion and Sediment Control - Updated Material Take-offs.xlsx\Civil

NOTES:

1. NOMINAL DIAMETER 200 mm HDPE DR17, UNLESS NOTED OTHERWISE.
2. QUANTITIES SHALL BE VERIFIED IN THE FIELD.

0	26JAN22	ISSUED WITH MEMO VA22-00058	CAP	CBN
REV	DATE	DESCRIPTION	PREP'D	RW'D

APPENDIX A

Plant Site Early Works Sediment Pond IFC Drawings

C3810 R2

C3811 R2

C3812 R2

C3813 R2

C3814 R2

C3815 R2

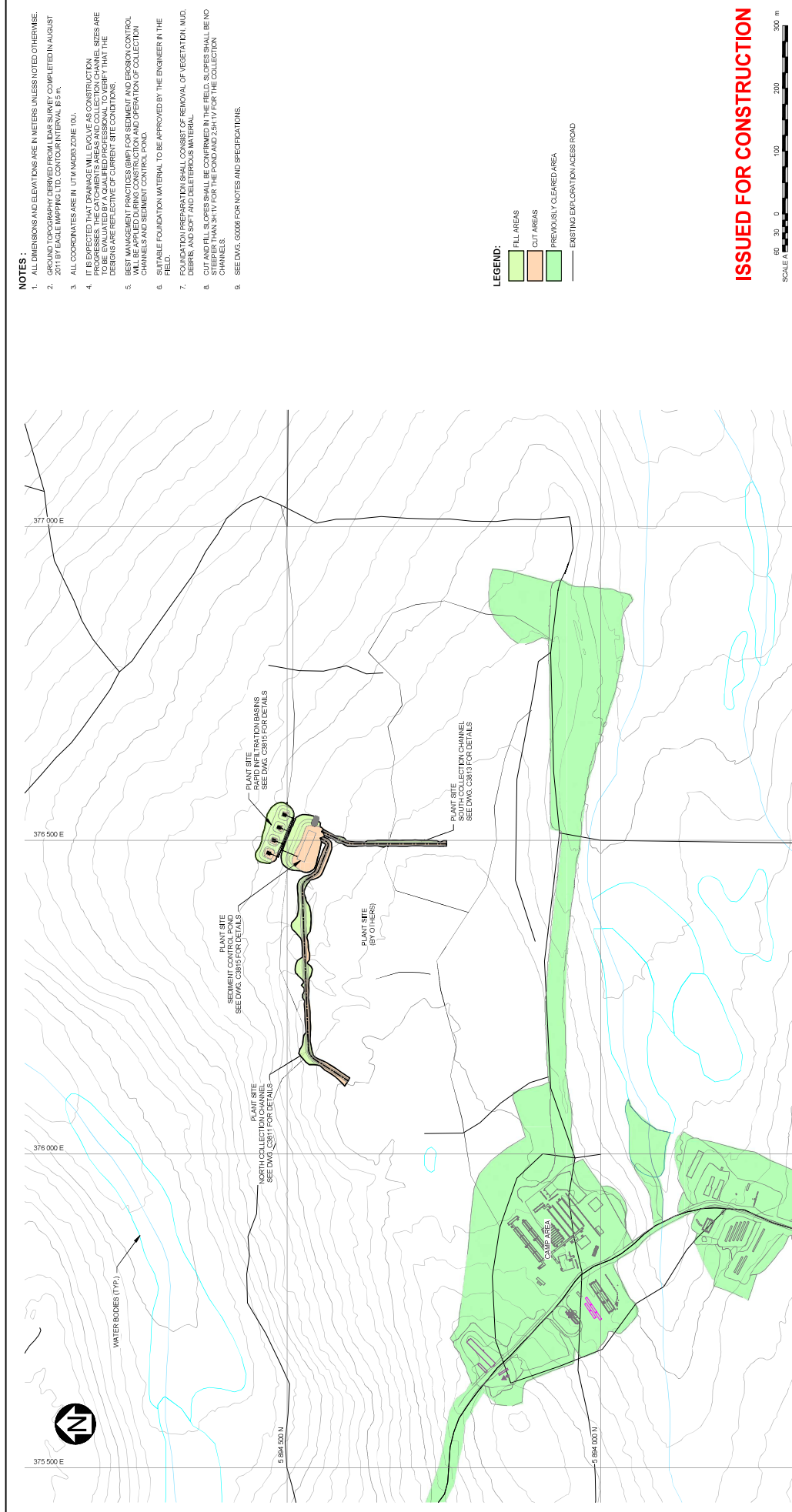
C3816 R2

C3820 R0

C3821 R0

G0006 R1

G0040 R1



NOTES:

1. ALL DIMENSIONS AND ELEVATIONS ARE IN METERS (UNLESS NOTED OTHERWISE).
2. THIS PLAN AND EROSION AND SEDIMENT CONTROL DETAILS WERE COMPLETED IN AUGUST 2021 BY EAGLE DRAINAGE LTD. CONTROL INTERVAL: 0.5 M.
3. ALL COORDINATES ARE IN UTM MGRS ZONE 10U.
4. IT IS EXPECTED THAT DRAINAGE WILL EVOLVE AS CONSTRUCTION PROGRESSES. THE DESIGNER HAS PROVIDED SUFFICIENT DESIGN TO BE EVALUATED BY A QUALIFIED PROFESSIONAL TO VERIFY THAT THE DESIGNS ARE REFLECTIVE OF CURRENT SITE CONDITIONS.
5. BEST MANAGEMENT PRACTICES (BMP) FOR SEDIMENT AND EROSION CONTROL, INCLUDING THE DESIGN, CONSTRUCTION AND OPERATION OF COLLECTION CHANNELS AND SEDIMENT CONTROL POND.
6. SUITABLE FOUNDATION MATERIAL TO BE APPROVED BY THE ENGINEER IN THE FIELD.
7. FOUNDATION PREPARATION SHALL CONSIST OF REMOVAL OF VEGETATION, MUD, DEBRIS AND SOFT AND DELETERIOUS MATERIAL.
8. CUT AND FILL SLOPES SHALL BE COMBINED IN THE FIELD. SLOPES SHALL BE NO STEEPER THAN 3H:1V FOR THE POND AND 2H:1V FOR THE COLLECTION CHANNELS.
9. SEE DWG. G3009 FOR NOTES AND SPECIFICATIONS.

ISSUED FOR CONSTRUCTION

SCALE: 1:500

Knights Pitsold CONSULTING

BW GOLD LTD.

BLACKWATER GOLD PROJECT

EROSION AND SEDIMENT CONTROL PLAN

PLANT SITE

GENERAL ARRANGEMENT

PHASE 1 (EARLY WORKS)

PROJECT NO.: VA101-457/33 DRAWING NO.: C3810 REVISION: 2

(Original signed by)

DATE: 2022-01-26

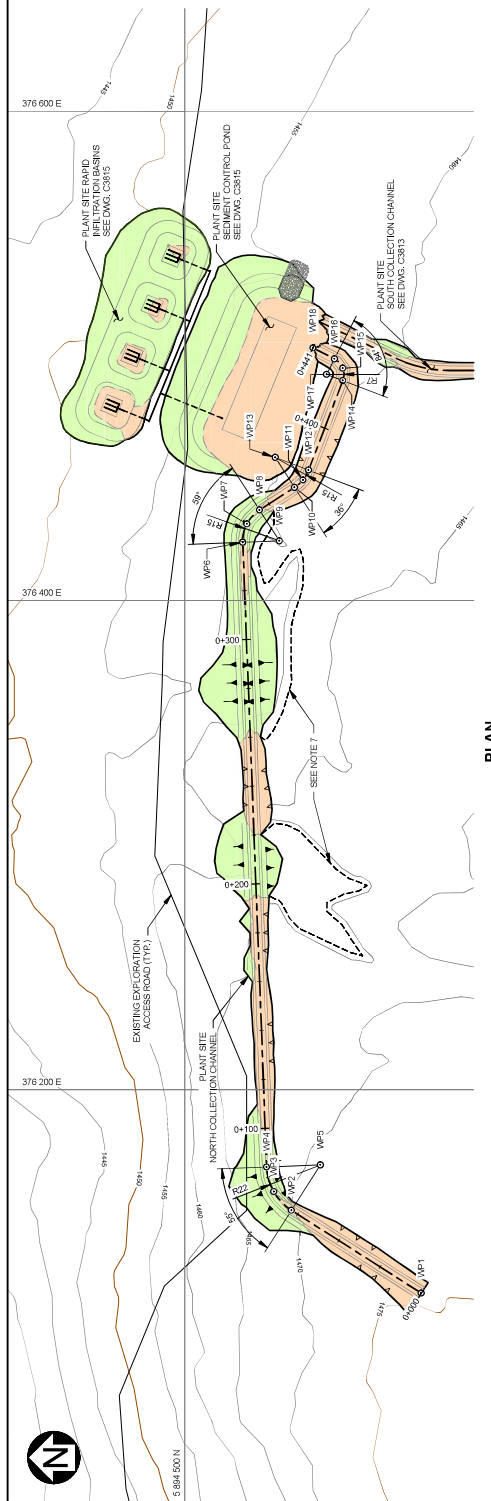
REV	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED
2	26/JAN/22	ISSUED FOR CONSTRUCTION	CAP	ELG	ELG	ELG
1	18/DEC/21	REVISED ARRANGEMENT ISSUED FOR CLIENT REVIEW	CAP	ELG	ELG	ELG
0	03/FEB/21	ISSUED FOR PERMITTING	CAP	ELG	ELG	ELG

DESCRIPTION	DATE	REVISIONS
EROSION AND SEDIMENT CONTROL PLAN - PHASE 1 (EARLY WORKS)		

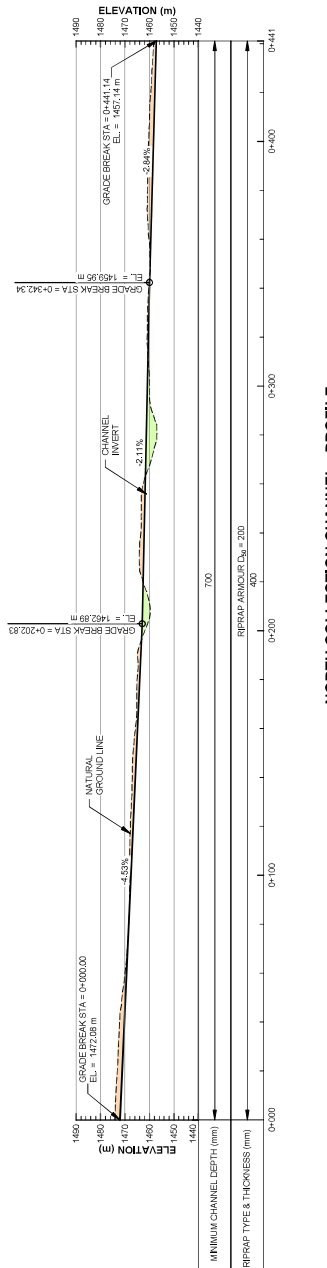
REF. NO.	DESCRIPTION	DATE	REVISIONS
C3816	ESCP - PLANT SITE - ADDITIONAL SECTIONS AND DETAILS		
C3815	ESCP - PLANT SITE - SEDIMENT CONTROL POND - PLAN AND PROFILE		
C3814	ESCP - PLANT SITE - SOUTH COLLECTION CHANNEL - PLAN AND PROFILE		
C3811	ESCP - PLANT SITE - NORTH COLLECTION CHANNEL - PLAN AND PROFILE		
G3009	CONSTRUCTION MATERIAL GRADATIONS		
G3008	TECHNICAL NOTES		

NOTES:

1. ALL DIMENSIONS AND ELEVATIONS ARE IN METERS UNLESS NOTED OTHERWISE.
2. GROUND TOPOGRAPHY DERIVED FROM LEAS SURVEY COMPLETED IN AUGUST 2017 BY SINGLE SURVEYORS LTD. CONTIGUOUS INTERVAL 10 m.
3. ALL COORDINATES ARE IN UTM (WGS 84) ZONE 10U.
4. FOR CROSS SECTIONS SEE DWG. C3812.
5. TYPICAL SECTIONS SHOWN ON DWG. C3818.
6. SEE DWG. G0006 FOR NOTES AND SPECIFICATIONS.
7. EARTHWORKS TO BE COMPLETED PRIOR TO PLANT SITE BULK EARTHWORKS FILL PLACEMENT.



POINT NO.	NORTHING	EASTING	INVERT ELEVATION (m)
WP1	5,884,402.79	376,116.86	1,472.88
WP2	5,884,406.98	376,150.71	1,469.33
WP3	5,884,406.52	376,158.34	1,468.75
WP4	5,884,406.02	376,169.45	1,468.27
WP5	5,884,444.00	376,169.30	N/A
WP6	5,884,472.76	376,423.84	1,460.20
WP7	5,884,474.03	376,437.34	1,459.80
WP8	5,884,468.92	376,437.02	1,459.58
WP9	5,884,460.79	376,424.41	N/A
WP10	5,884,454.58	376,446.26	1,459.10
WP11	5,884,451.15	376,446.24	1,458.86
WP12	5,884,446.89	376,453.33	1,458.83
WP13	5,884,462.48	376,458.53	N/A
WP14	5,884,434.89	376,469.06	1,457.72
WP15	5,884,434.89	376,469.06	1,457.72
WP16	5,884,436.30	376,468.83	1,457.42
WP17	5,884,441.53	376,492.50	N/A
WP18	5,884,447.11	376,503.33	1,457.14



NORTH COLLECTION CHANNEL - PROFILE
SCALE A

ISSUED FOR CONSTRUCTION



Knights PileSolid CONSULTING

BW GOLD LTD.

BLACKWATER GOLD PROJECT

EROSION AND SEDIMENT CONTROL PLAN

NORTH COLLECTION CHANNEL

PLAN AND PROFILE

Original signed by

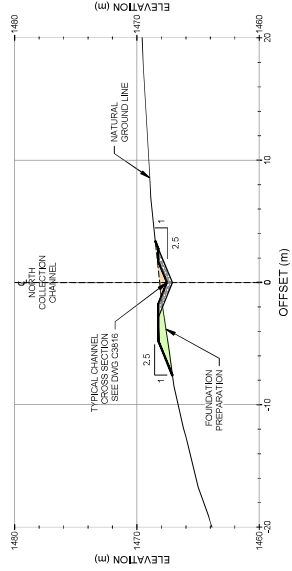
REVISIONS

REV	DATE	DESCRIPTION	APPROVED	REVIEWED
2	26/JAN/22	ISSUED FOR CONSTRUCTION	ELC	ELC
1	18/DEC/21	REVISED ARRANGEMENT ISSUED FOR CLIENT REVIEW	CAP	ELC
0	04/FEB/21	ISSUED FOR PERMITTING	CAP	DDF

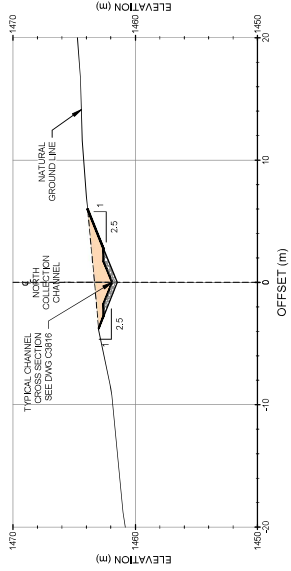
REF. NO.	DESCRIPTION	DATE	APPROVED	REVIEWED
C3816	ESCP - PLANT SITE - ADDITIONAL SECTIONS AND DETAILS			
C3815	ESCP - PLANT SITE - SEDIMENT CONTROL BARRIERS SECTIONS			
C3813	ESCP - PLANT SITE - SOUTH COLLECTION CHANNEL - PLAN AND PROFILE			
C3812	ESCP - PLANT SITE - NORTH COLLECTION CHANNEL - CROSS SECTIONS			
C3810	ESCP - PLANT SITE - GENERAL ARRANGEMENT - PHASE 1 (EARLY WORKS)			
G0040	CONSTRUCTION MATERIAL GRADATIONS - PHASE 1 (EARLY WORKS)			
G0006	TECHNICAL NOTES			

NOTES :

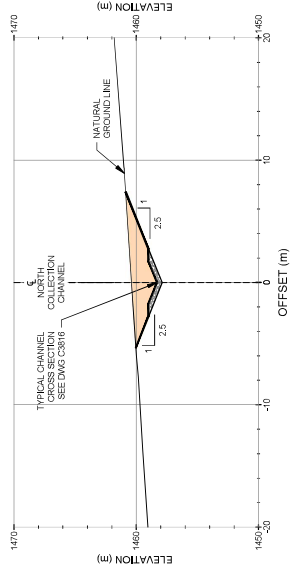
1. ALL DIMENSIONS AND ELEVATIONS ARE IN METERS UNLESS NOTED OTHERWISE.
2. GROUND TOPOGRAPHY DERIVED FROM LIDAR SURVEY COMPLETED IN AUGUST 2011 BY ENGLE MAPPING LTD. CONTOUR INTERVAL IS 0.1m.
3. ALL COORDINATES ARE IN UTM (NAD83 ZONE 10U).
4. SEE DWG. 0006 FOR NOTES AND SPECIFICATIONS.
5. PLACE FILL TO PROMOTE POSITIVE DRAINAGE PRIOR TO PLANT SITE BULK EARTHWORKS FILL PLACEMENT.



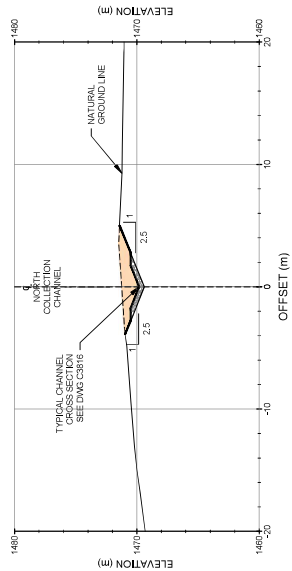
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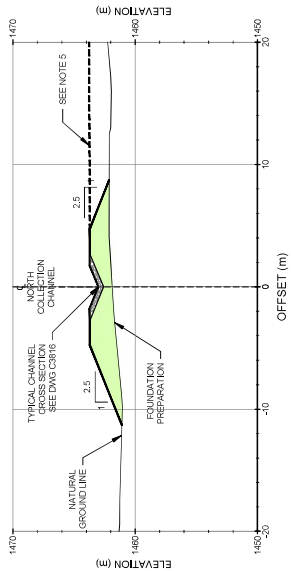
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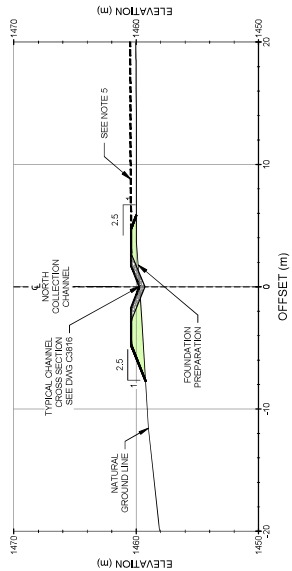
CROSS SECTION - STA. 0+400
SCALE A



CROSS SECTION - STA. 0+050
SCALE A



CROSS SECTION - STA. 0+200
SCALE A



CROSS SECTION - STA. 0+350
SCALE A



ISSUED FOR CONSTRUCTION



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BLACKWATER GOLD PROJECT

Original signed by: _____

EROSION AND SEDIMENT CONTROL PLAN
PLANT SITE
NORTH COLLECTION CHANNEL
CROSS SECTIONS

REV. NO.	DATE	DESCRIPTION	APPROVED
0	04 FEB 21	ISSUED FOR PERMITS	ELC
1	18 DEC 21	REVISED ARRANGEMENT ISSUED FOR CLIENT REVIEW	ELC
2	26 JAN 22	ISSUED FOR CONSTRUCTION	ELC

REV	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED
0	04 FEB 21	ISSUED FOR PERMITS	ELC	ELC	ELC	ELC
1	18 DEC 21	REVISED ARRANGEMENT ISSUED FOR CLIENT REVIEW	ELC	ELC	ELC	ELC
2	26 JAN 22	ISSUED FOR CONSTRUCTION	ELC	ELC	ELC	ELC

REV. NO.	DESCRIPTION	DATE	APPROVED
C3816	ESCP - PLANT SITE - ADDITIONAL SECTIONS AND DETAILS		
C3817	ESCP - PLANT SITE - NORTH COLLECTION CHANNEL - PLAN AND PROFILE		
C3818	ESCP - PLANT SITE - GENERAL ARRANGEMENT - PHASE 1 (EARLY WORKS)		
G0040	CONSTRUCTION MATERIAL GRADATIONS		
G0046	TECHNICAL NOTES		

REVISIONS

REVISIONS

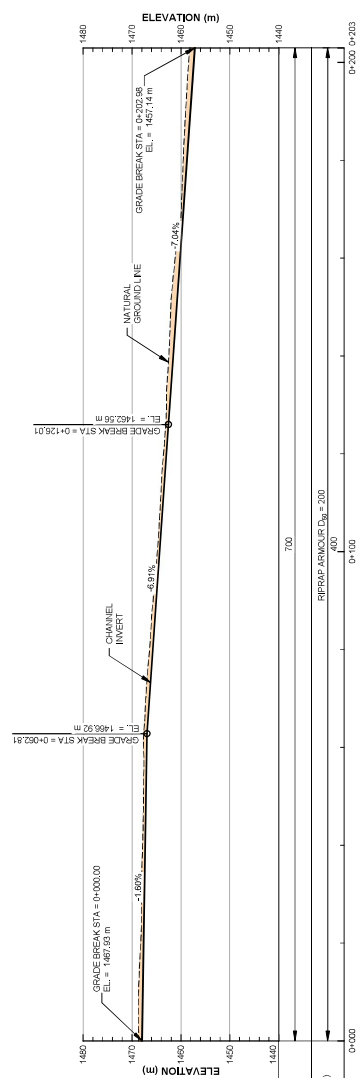
REVISIONS

2022-01-26

PROJECT NO.	VA101-457/33
DRAWING NO.	C3812
REVISION	2

- NOTES:**
1. ALL DIMENSIONS AND ELEVATIONS ARE IN METERS UNLESS NOTED OTHERWISE.
 2. GROUND TOPOGRAPHY DERIVED FROM LIDAR SURVEY COMPLETED IN AUGUST 2017 BY BRUCE WIPPAUS/UTL CONSULTING INC.
 3. ALL COORDINATES ARE IN UTM MGRS ZONE 10U.
 4. FOR CROSS SECTIONS SEE DWG. C3814.
 5. TYPICAL SECTIONS SHOWN ON DWG. C3816.
 6. SEE DWG. 00006 FOR NOTES AND SPECIFICATIONS.

SOUTH COLLECTION CHANNEL WORK POINTS			
POINT NO.	NORTHING	EASTING	INVERT ELEVATION (m)
WP1	5,894,266.00	376,494.08	1,465.83
WP2	5,894,391.32	376,494.08	1,462.26
WP3	5,894,402.33	376,495.31	1,461.56
WP4	5,894,412.79	376,498.93	1,460.10
WP5	5,894,391.32	376,544.08	N/A
WP6	5,894,444.62	376,514.16	1,459.26



ISSUED FOR CONSTRUCTION



KNIGHT PIPESOLD CONSULTING
 BW GOLD LTD.
BLACKWATER GOLD PROJECT
EROSION AND SEDIMENT CONTROL PLAN
PLANT SITE
SOUTH COLLECTION CHANNEL
PLAN AND PROFILE

Original signed by [Signature]

DATE: 2022-01-26

SOUTH COLLECTION CHANNEL - PROFILE

REV.	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED
2	26/JAN/22	ISSUED FOR CONSTRUCTION				
1	18/DEC/21	REVISED ARRANGEMENT ISSUED FOR CLIENT REVIEW				
0	04/FEB/21	ISSUED FOR PERMITTING				

REVISIONS

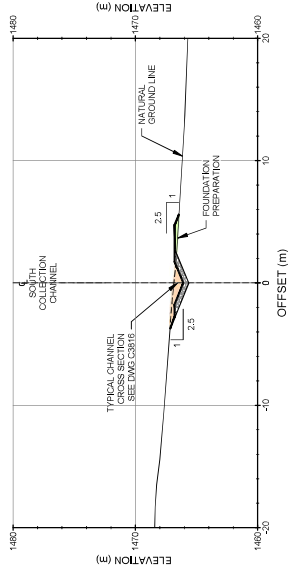
REV.	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED
2	26/JAN/22	ISSUED FOR CONSTRUCTION				
1	18/DEC/21	REVISED ARRANGEMENT ISSUED FOR CLIENT REVIEW				
0	04/FEB/21	ISSUED FOR PERMITTING				

REFERENCE DRAWINGS

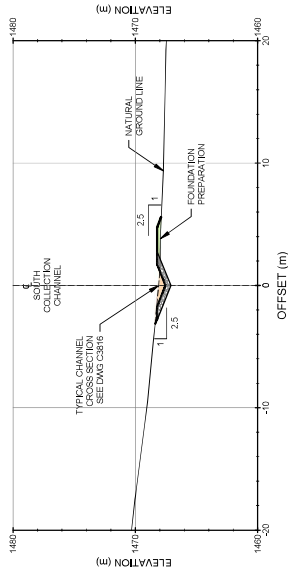
DWG. NO.	DESCRIPTION
C3816	ESCP - PLANT SITE - ADDITIONAL SECTIONS AND DETAILS
C3815	ESCP - PLANT SITE - SEDIMENT CONTROL BOUNDARY AND SECTIONS
C3814	ESCP - PLANT SITE - SOUTH COLLECTION CHANNEL - CROSS SECTIONS
C3811	ESCP - PLANT SITE - NORTH COLLECTION CHANNEL - PLAN AND PROFILE
C3810	ESCP - PLANT SITE - GENERAL ARRANGEMENT - PHASE 1 (EARLY WORKS)
G0040	CONSTRUCTION MATERIAL GRADATIONS
G0006	TECHNICAL NOTES

NOTES :

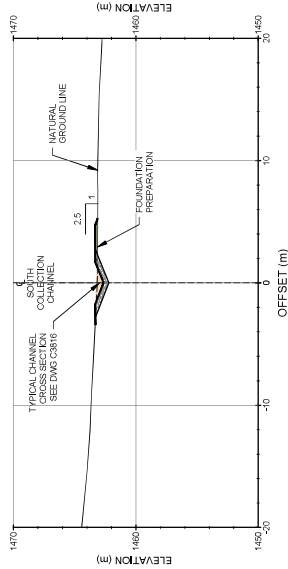
1. ALL DIMENSIONS AND ELEVATIONS ARE IN METERS UNLESS NOTED OTHERWISE.
2. GROUND TOPOGRAPHY DERIVED FROM LIDAR SURVEY COMPLETED IN AUGUST 2011 BY ENGLE MAPPING LTD. CONTOUR INTERVAL IS 1m.
3. ALL COORDINATES ARE IN UTM (MDS3 ZONE 19U).
4. SEE DWG. 00006 FOR NOTES AND SPECIFICATIONS.



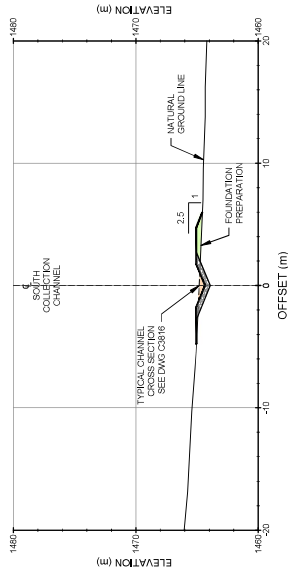
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SCALE A



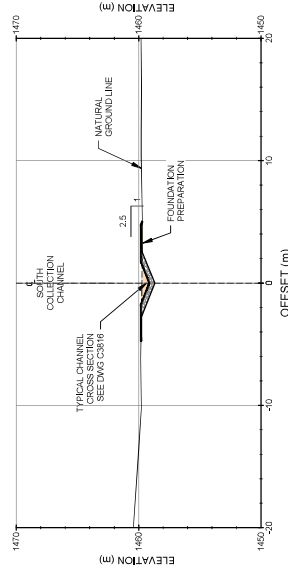
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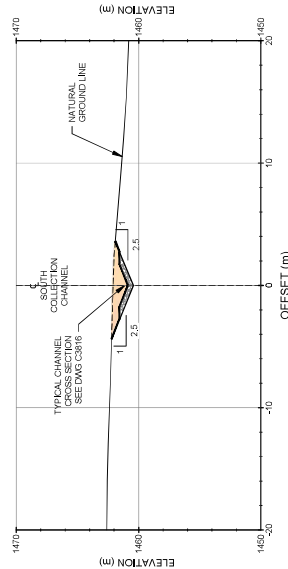
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SCALE A



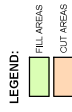
CROSS SECTION - STA. 0+100
SCALE A



CROSS SECTION - STA. 0+175
SCALE A



CROSS SECTION - STA. 0+150
SCALE A



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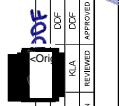
EROSION AND SEDIMENT CONTROL PLAN
PLANT SITE
SOUTH COLLECTION CHANNEL
CROSS SECTIONS

REV. NO. DRAWING NO. PROJECT NO. SHEET NO.

01/2022 01/2022 01/2022 01/2022

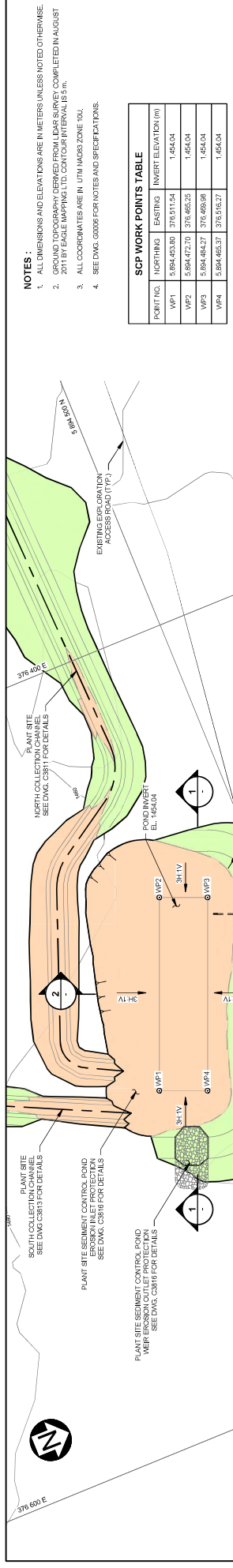
VA101-457/33 C3814 2

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REV	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED
2	26/JAN/22	ISSUED FOR CONSTRUCTION	CAP	ELC	ELC	DOF
1	18/DEC/21	REVISED ARRANGEMENT ISSUED FOR CLIENT REVIEW	CAP	ELC	ELC	DOF
0	08/FEB/21	ISSUED FOR PERMITS	CAP	ELC	ELC	DOF

REF. NO.	DESCRIPTION	DATE	REVISIONS
C3816	ES&P - PLANT SITE - ADDITIONAL SECTIONS AND DETAILS		
C3810	ES&P - PLANT SITE - SOUTH COLLECTION CHANNEL - PLAN AND PROFILE		
C3810	ES&P - PLANT SITE - GENERAL ARRANGEMENT - PHASE 1 (EARLY WORKS)		
G0040	CONSTRUCTION MATERIAL GRADATIONS		
G0006	TECHNICAL NOTES		



NOTES :

- ALL DIMENSIONS AND ELEVATIONS ARE IN METERS UNLESS NOTED OTHERWISE.
- GROUND TOPOGRAPHY DERIVED FROM LIDAR SURVEY COMPLETED IN AUGUST 2011 BY EAGLE MAPPING LTD. CONTOUR INTERVALS 5m.
- ALL COORDINATES ARE IN UTM MADS ZONE 10J.
- SEE DWG. 0009 FOR NOTES AND SPECIFICATIONS.

SCP WORK POINTS TABLE

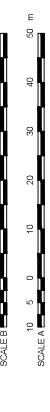
POINT NO.	NORTHING	EASTING	INVERT ELEVATION (m)
WPS1	5,884,468.88	376,542.75	1,450.50
WPS2	5,884,472.70	376,462.25	1,454.04
WPS3	5,884,484.27	376,485.38	1,454.04
WPS4	5,884,465.37	376,516.27	1,454.04

INFILTRATION BASIN WORK POINTS TABLE

POINT NO.	NORTHING	EASTING	INVERT ELEVATION (m)
WPS5	5,884,468.88	376,542.75	1,450.50
WPS6	5,884,502.52	376,536.26	1,450.50
WPS7	5,884,500.00	376,538.91	1,450.50
WPS8	5,884,506.35	376,545.39	1,450.50
WPS9	5,884,508.19	376,522.37	1,450.50
WPS10	5,884,510.83	376,515.89	1,450.50
WPS11	5,884,517.31	376,518.54	1,450.50
WPS12	5,884,514.67	376,525.02	1,450.50
WPS13	5,884,516.50	376,507.01	1,450.50
WPS14	5,884,519.15	376,465.52	1,450.50
WPS15	5,884,525.63	376,468.17	1,450.50
WPS16	5,884,522.88	376,504.65	1,450.50
WPS17	5,884,524.82	376,481.64	1,450.50
WPS18	5,884,527.46	376,475.16	1,450.50
WPS19	5,884,533.94	376,477.80	1,450.50
WPS20	5,884,531.30	376,484.28	1,450.50



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BLACKWATER GOLD PROJECT

EROSION AND SEDIMENT CONTROL PLAN

PLANT SITE

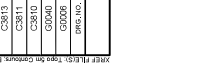
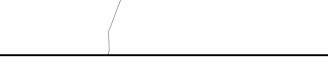
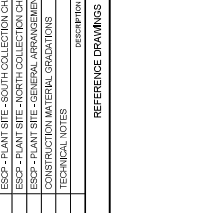
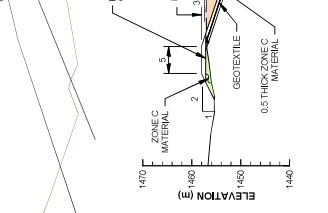
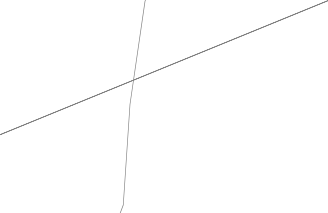
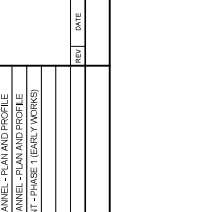
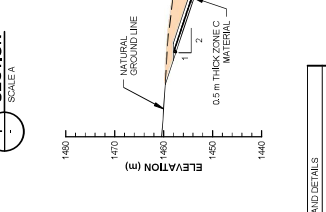
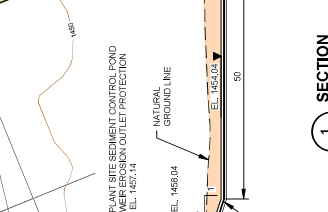
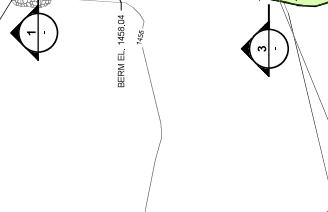
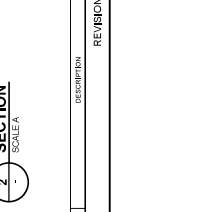
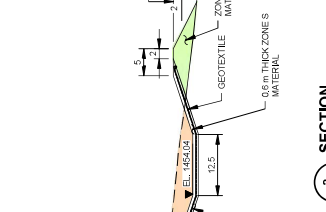
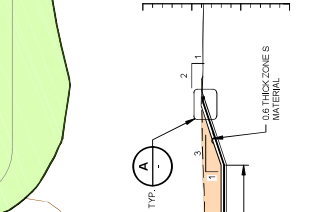
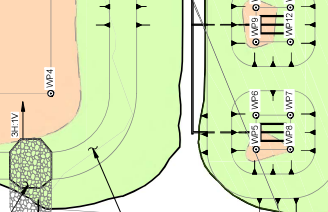
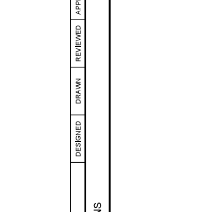
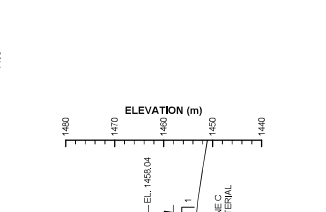
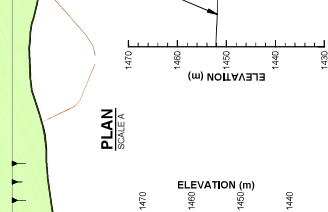
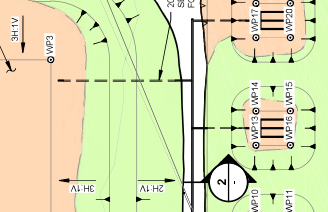
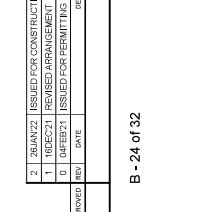
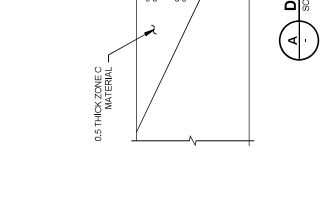
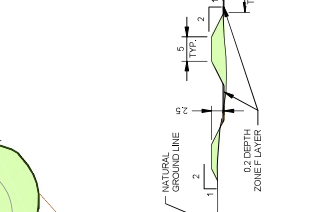
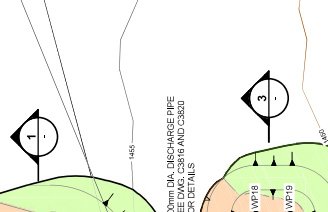
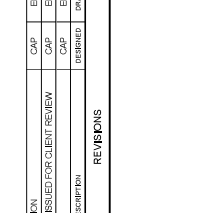
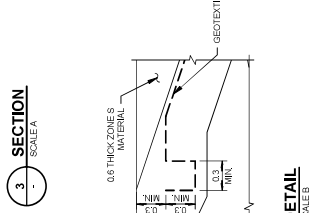
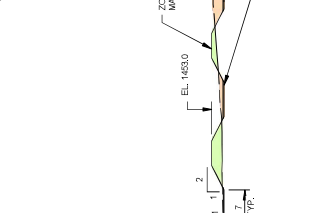
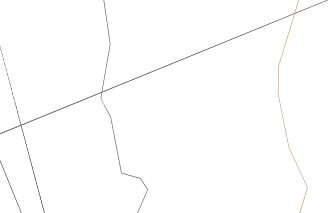
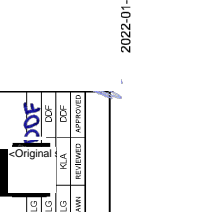
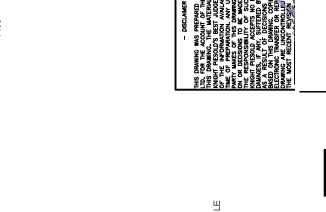
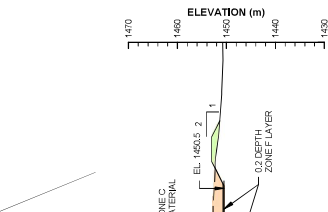
SEDIMENT CONTROL POND

PLAN AND SECTIONS

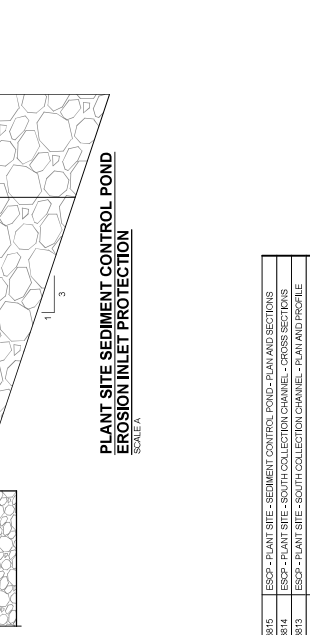
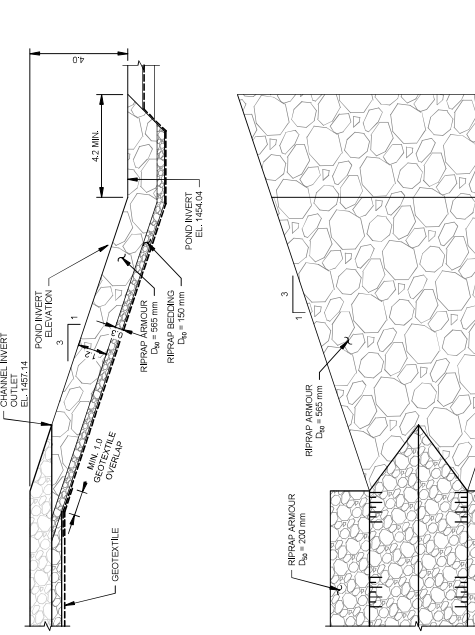
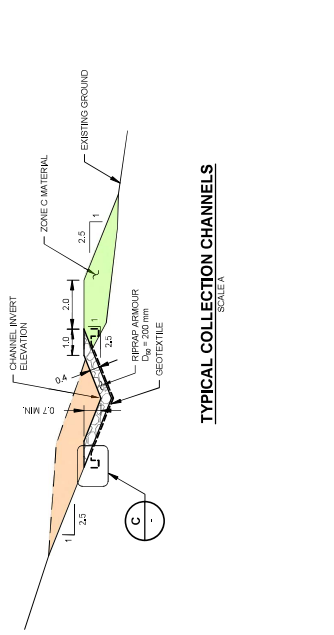
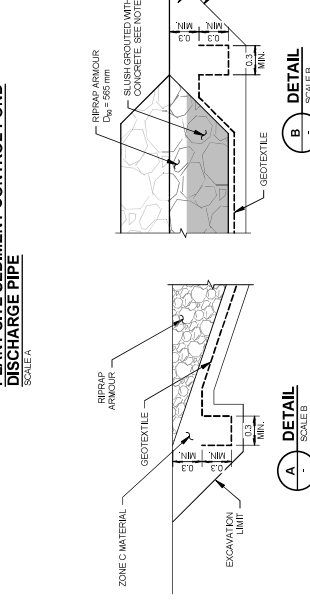
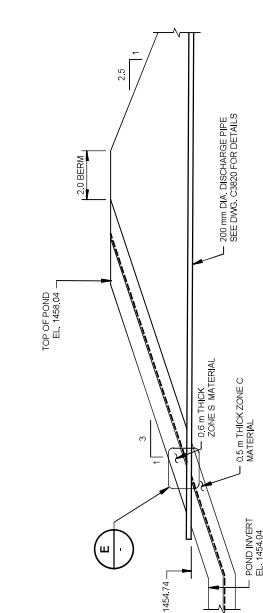
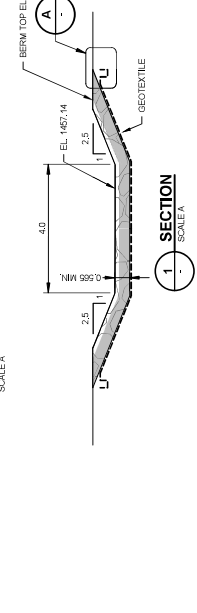
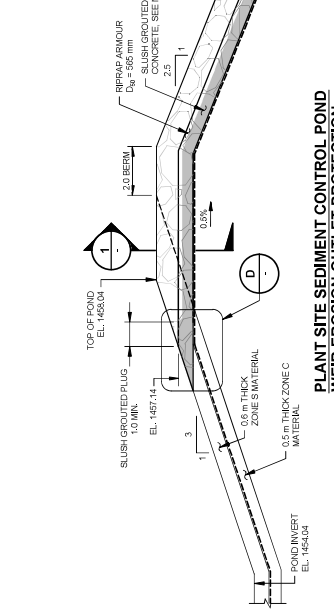
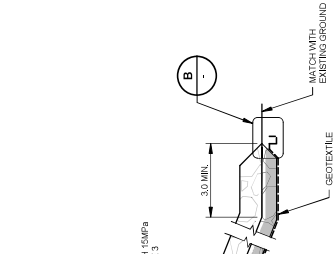
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2022-01-26	REVISION ARRANGEMENT ISSUED FOR CLIENT REVIEW	[Signature]
2022-01-26	REVISION ARRANGEMENT ISSUED FOR PERMITTING	[Signature]

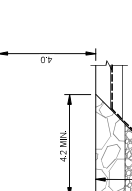
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1	18/08/21	REVISION ARRANGEMENT ISSUED FOR CLIENT REVIEW	ELC	DLF
2	26/01/22	ISSUED FOR CONSTRUCTION	ELC	DLF



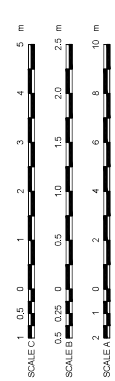
- NOTES:**
1. ALL DIMENSIONS AND ELEVATIONS ARE IN METERS (UNLESS NOTED OTHERWISE).
 2. PROPOSED EROSION CONTROL STRUCTURES SHALL BE CONSTRUCTED TO A FINISH SURFACE OF RIPPAP THICKNESS USING 15MPa CONCRETE. A FINAL ROUGH SURFACE SHALL REMAIN TO AID ENERGY DISSIPATION.
 3. SEE DWG. G000R FOR NOTES AND SPECIFICATIONS.



- LEGEND:**
- ALL AREAS
 - CUT AREAS



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BLACKWATER GOLD PROJECT

EROSION AND SEDIMENT CONTROL PLAN

ADDITIONAL SECTIONS AND DETAILS

PROJECT NO: VA101-457/33 DRAWING NO: C3816 REVISION: 2

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REV	DATE	DESCRIPTION	DESIGNED	DRAWN	APPROVED
0	02/02/21	ISSUED FOR PERMITTING			
1	18/02/21	REVISED ARRANGEMENT ISSUED FOR CLIENT REVIEW			
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REVISIONS

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REFERENCE DRAWINGS

DWG. NO.	DESCRIPTION
C0315	ESCP - PLANT SITE - SEDIMENT CONTROL POND - PLAN AND SECTIONS
C0316	ESCP - PLANT SITE - SOUTH COLLECTION CHANNEL - PLAN AND PROFILE
C0317	ESCP - PLANT SITE - NORTH COLLECTION CHANNEL - PLAN AND PROFILE
C0318	ESCP - PLANT SITE - NORTH COLLECTION CHANNEL - CROSS SECTIONS
C0319	ESCP - PLANT SITE - GENERAL ARRANGEMENT - PHASE 1 (EARLY WORKS)
C0320	CONSTRUCTION MATERIAL GRADATIONS
G0040	TECHNICAL NOTES

REVISIONS

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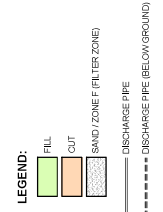
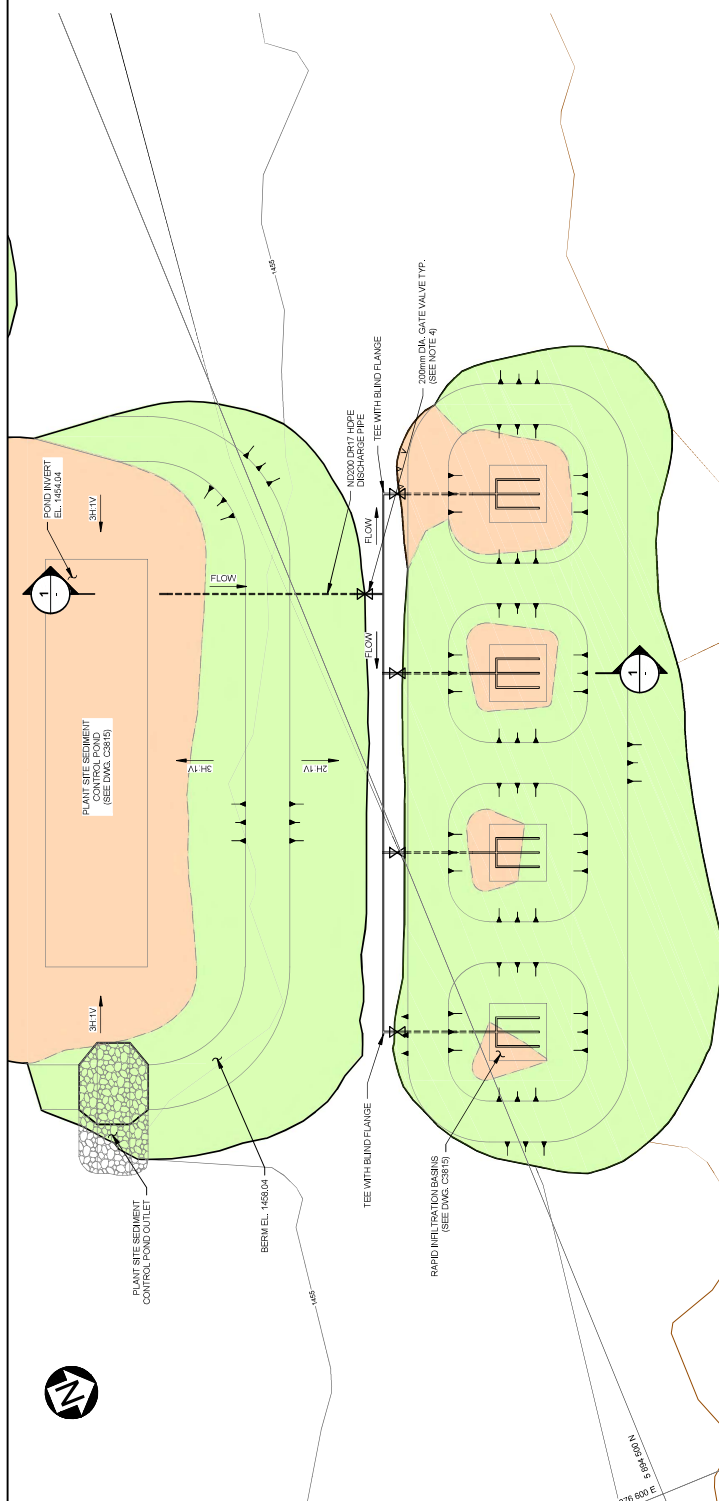
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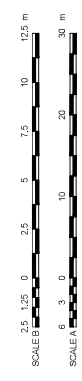
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- NOTES :**
- SEE DRAWINGS 0006 FOR NOTES AND SPECIFICATIONS.
 - CONTRACTOR TO SUBMIT HOPE BONDING PROCEDURE FOR REVIEW AND APPROVAL.
 - REGRADE AS NECESSARY TO ALLOW FOR COMPLETE GRAVITY DRAINAGE TOWARDS RAPID INFILTRATION BASINS AND PREVENT POOLING IN PIPE.
 - ALL FLANGES AND VALVES TO BE SUPPORTED IN A MANNER AS TO PROVIDE ADEQUATE CLEARANCE FOR INSTALLATION AND MAINTENANCE.

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EROSION AND SEDIMENT CONTROL PLAN
PLANT SITE
SEDIMENT CONTROL POND PIPING
PLAN AND SECTION

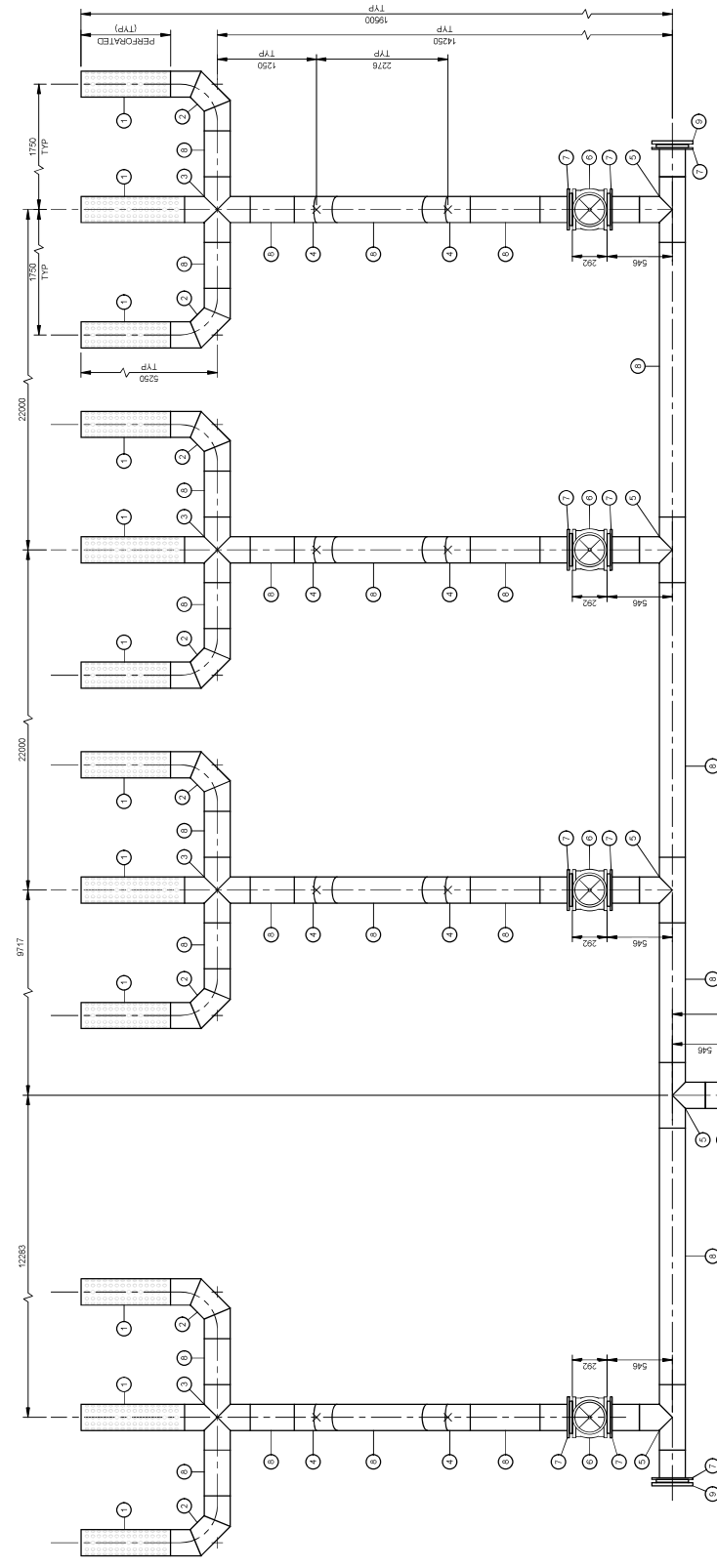
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DRAWING NO.	C3820
REVISION	0

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REF. NO.	DESCRIPTION
C3821	ESCP - PLANT SITE - SEDIMENT CONTROL POND PIPING DETAIL - PLAN
C3818	ESCP - PLANT SITE - ADDITIONAL SECTIONS AND DETAILS
C3815	ESCP - PLANT SITE - SEDIMENT CONTROL POND - PLAN AND SECTIONS
G0040	CONSTRUCTION MATERIAL GRADATIONS
G0006	TECHNICAL NOTES



ITEM NO.	DIAMETER (mm)	QTY.	DESCRIPTION
1	200	58 m	PIPE DRY HOPE PERFORATED PLAIN END CONNECTED
2	200	8	90 DEGREE ELBOW DRY HOPE FABRICATED 2-SEGMENT PLAIN END CONNECTED
3	200	4	CROSS DRY HOPE FABRICATED PLAIN END CONNECTED
4	200	8	22.5 DEGREE ELBOW DRY HOPE FABRICATED 2-SEGMENT PLAIN END CONNECTED
5	200	5	TEE DRY HOPE FABRICATED PLAIN END CONNECTED
6	200	5	GATE VALVE CLASS 150 RANSEDFACE FLANGE CONNECTED HANDWHEEL OPERATED
7	200	12	FLANGE ADAPTER DRY HOPE C/DUCTILE IRON BACKUP RING AND GASKET
8	200	138 m	PIPE DRY HOPE PLAIN END CONNECTED
9	200	2	FLANGE BLIND HOPE

- NOTES:**
1. SEE DRAWINGS 500M FOR NOTES AND SPECIFICATIONS.
 2. ALL VALVES AND FLANGES ARE CLASS 150 UNLESS SPECIFIED OTHERWISE.
 3. MATERIAL PRESSURE RATING IS THE MINIMUM REQUIRED.
 4. ALL HOPE MATERIALS ARE TO BE PE4710 AS PER ASTM D3350-08 UNLESS NOTED OTHERWISE.
 5. HOPE FLANGE ASSEMBLY INCLUDES FLANGE ADAPTER & BACKUP RING.

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PLANT SITE
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PLAN

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REV. NO. VA101-457/33 DRAWING NO. C3821 REVISION 0

Original signed by: [Signature]

DESIGNING: [Signature]

PROJ. NO. [Signature]

PLAN SEDIMENT POND DISCHARGE PIPING
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REV.	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED	ISSUED FOR CONSTRUCTION	DATE	REV.	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED
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REFERENCE DRAWINGS

REF. NO.	DESCRIPTION
C3820	ESOP - PLANT SITE - SEDIMENT CONTROL POND PIPING - PLAN AND SECTION
G040	CONSTRUCTION MATERIAL GRADATIONS
G006	TECHNICAL NOTES

REVISIONS

REV.	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED
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GENERAL:

- COORDINATE GRID IS UTM MAG 63 ZONE 00L.
- GRID AND TOPOGRAPHY BASED ON INFORMATION PROVIDED BY EAGLE CONSULTING ENGINEERS AND GROUND DATA.
- ALL DIMENSIONS IN METRES AND ELEVATIONS ARE IN METRES, UNLESS NOTED OTHERWISE.
- DRAWINGS WILL BE READ IN CONJUNCTION WITH THE PROJECT TECHNICAL SPECIFICATIONS. THE DRAWINGS WILL TAKE PRECEDENCE IN THE CASE OF A DISCREPANCY.
- THE ENGINEER SHALL BE NOTIFIED UPON ANY DISCOVERY OF DISCREPANCIES BETWEEN THE ISSUED DRAWING SET AND/OR CONSTRUCTED WORKS.
- MAIN SURVEY CONTROL ON ALL ASPECTS OF THE WORKS. VERIFY ALL DIMENSIONS AND LEVELS AGAINST THE SURVEY CONTROL. NOTIFY THE ENGINEER IMMEDIATELY OF ANY DISCREPANCY.
- COMPARE THE LOCATION OF ALL ROAD AND PIPE CROSSINGS.
- ALL MATERIALS USED WILL BE THE BEST SUITED FOR THE APPLICATION BASED ON SUPPLIER'S PERFORMANCE.

DESIGN CHANGE MANAGEMENT:

- MATERIALS OR PRODUCTS USED SHALL BE AS SPECIFIED ON THE DESIGN DRAWINGS OR EQUIVALENT AS APPROVED BY THE ENGINEER.

INSTRUMENTATION:

- ALL WATER LEVEL, PORE PRESSURE, SURFACE AND SUBSURFACE INSTRUMENTATION SHALL BE SURVEILLED AND MONITORED AUTOMATICALLY CAPABILITY TO AUTOMATICALLY COLLECT AND TRANSMIT DATA.
- FLOW MONITORING INSTRUMENTATION SHALL BE SURVEILLED AUTOMATICALLY OR MANUALLY DEPENDING ON THE LOCATION AND MONITORING SET UP AS DETERMINED BY THE ENGINEER. FLOW MONITORING INSTRUMENTATION SHALL BE COMPRISED OF THE FOLLOWING:
 - V NOTCH WEIRS AT THE END OF PERMANENT INLET AND OUTLET PIPES OR FLOW METERS ON PERMANENT PUMPS.
 - DATA LOGGERS WITH CELLULAR TRANSMITTING CAPABILITIES ARE TO BE INSTALLED AT THE TOP OF MAIN DAM CAT AT EACH INSTRUMENTATION SECTION.
 - DAM CREST SURFACE DISPLACEMENT TO BE AUTOMATICALLY MONITORED BY TOTAL STATION AND SURVEY PRISMS.
- SURVEY PRISMS INSTALLED AT 100 METER INTERVALS ON MAIN DAM CREST.
- AUTOMATIC TOTAL STATIONS TO SCAN SURVEY PRISMS AT A MINIMUM ONCE DAILY.
- AUTOMATIC MONITORING TO COMMENCE AT SUBSTANTIAL COMPLETION.

FOUNDATIONS:

- THE FOUNDATION LEVELS GIVEN ON THE DRAWINGS ARE ANTICIPATED LEVELS. THE EXACT LEVELS SHALL BE DETERMINED BY THE ENGINEER BASED ON ACTUAL SITE CONDITIONS.
- EXCAVATIONS WITH SIGNIFICANT WATER SEEPAGE MAY REQUIRE REDUCED EXCAVATION SLOPES THAN WHAT IS SHOWN ON THE EXCAVATION DRAWINGS UNLESS NOTED OTHERWISE. CONTRACTOR TO ALLOW FOR SUCH DEWATERING SYSTEMS.
- BLINDING CONCRETE / LEAN MIX CONCRETE MURALS MAY BE REQUIRED IN THE BOTTOM OF SOME FOUNDATION EXCAVATIONS. MINIMUM THICKNESS OF BLINDING CONCRETE SHALL BE 50 mm WITH A MAXIMUM NOMINAL THICKNESS OF 100 mm. ALL EXCAVATIONS SHALL BE PROTECTED WITH 600 mm AT DEEP INFILL AREAS SUCH AS ROCK EXCAVATION OVERBREAK.
- BLINDING CONCRETE SHALL HAVE A COMPRESSIVE STRENGTH OF AT LEAST 15 MPa AT 28 DAYS.
- FOR BLINDING LAYER CONCRETE THICKER THAN NOMINAL 200 mm USE CONVENTIONAL TYPE C25 CONCRETE UP TO DESIGN GRADE AND ELEVATION. ALL OTHER AREAS SHALL BE CONCRETE DESIGN FOR THE STRUCTURAL MEMBER SHOULD BE USED.
- PRIOR TO PLACING BUILDING CONCRETE, REMOVE AND REPLACE ALL AREAS OF LOOSE OR SOFT MATERIAL OR COMPACT SUB GRADE SOILS AS SPECIFIED.
- FREEDING OF BUILDING LAYER CONCRETE AND/OR EXPOSED FOUNDATION MATERIAL SHALL NOT BE ALLOWED AND WILL BE REJECTED BY THE ENGINEER. ACCEPTED BY THE ENGINEER PRIOR TO PLACING BUILDING CONCRETE AND APPROVAL BY ENGINEER. REMOVAL OF EXCESSIVE CONCRETE AND APPROVAL BY ENGINEER.
- ALL EXCAVATIONS SHALL BE KEPT FREE OF STANDING WATER AT ALL TIMES.

TEMPORARY STRUCTURES

- THE CONTRACTOR SHALL DESIGN AND DETAIL ALL TEMPORARY STRUCTURES USED FOR THE CONSTRUCTION OF THE PERMANENT WORKS.
- MAINTAIN ALL STRUCTURES IN A STABLE CONDITION DURING CONSTRUCTION STRESSED DUE TO THE CONSTRUCTION ACTIVITIES.
- PERMANENT WORKS SHALL NOT BE ALLOWED TO BE UNDERCUT OR UNDERMINED BY ANY CONSTRUCTION ACTIVITIES.

PIPEWORKS AND APPURTENANCES:

- GENERAL
 - PIPELINE ALIGNMENTS TO BE CONFIRMED IN THE FIELD TO ENSURE PIPELINE INSTALLATION AND OPERATION DO NOT INTERFERE WITH OTHER INFRASTRUCTURE OPERATING ACTIVITIES.
 - COMPARE THE LOCATION OF ALL HIGH AND LOW POINTS ALONG THE PIPELINE ALIGNMENT. FOR THE INSTALLATION OF COMBINATION ARCHIVALUM RELEASE VALVES AND DRAIN POINTS, RESPECTIVELY.
 - GEOTECHNICAL REQUIREMENTS
 - PIPE FOUNDATION SHALL BE INSPECTED BY THE ENGINEER PRIOR TO LAYING OF THE PIPE. ANY SOFT SPOTS OR HARD SPOTS SUCH AS ROCK OR TOP NOT EXPECTED SHALL BE SURVEYED AND REPORTED TO ENGINEER FOR CHECKING AND APPROVAL. ALL FOUNDATION SPOTS SHALL BE PROTECTED WITH PIPE SUPPORTS OR ROCK CUT CROPS THAT CAUSE STRESS CONCENTRATIONS UNLESS NOTED OTHERWISE.
 - PIPELINE THICKNESS SHALL BE THE MINIMUM THICKNESS REQUIRED.
 - MINIMUM HOPE BEND RADIUS IS TO BE CONFIRMED BASED ON MANUFACTURERS SPECIFICATION.
 - AS PART OF THESE SPECIFICATIONS THE MANUFACTURER SHALL HAVE INSPECTED THE END PREPARATION, THICKNESS AND DIAMETERS AS PER SPECIFICATIONS. THIRD PARTY QUALITY ASSURANCE SHALL VERIFY THAT THE PIPE MEETS THE REQUIRED SPECIFICATIONS PRIOR TO BEING SHIPPED TO SITE.
 - PRESSURE RATINGS - ALL EQUIPMENT IS TO BE RATED TO THE INSTALLED MINIMUM PIPELINE PRESSURE RATING UNLESS OTHERWISE NOTED.
 - QUALITY ASSURANCE - THE MANUFACTURER SHALL ALWAYS HAVE IN EFFECT A QA PROGRAM WHICH CLEARLY ESTABLISHES THE AUTHORITY AND RESPONSIBILITY OF THOSE RESPONSIBLE FOR THE QA PROGRAM. PERSONS RESPONSIBLE FOR QA FUNCTIONS SHALL HAVE SUFFICIENT KNOWLEDGE AND WELL UNDERSTANDING OF RESPONSIBILITY AND AUTHORITY TO IDENTIFY PROBLEMS AND TO VERIFY THE EFFECTIVENESS OF THE SOLUTION.
- MANUFACTURING AND INSTALLATION
 - EQUIPMENT SUPPLIERS SHALL PROVIDE MATERIAL OF HIGH AND CONSISTENT QUALITY.
 - MATERIAL TESTING - WHERE APPLICABLE, MATERIALS TESTING SHALL BE RECORDED, AND TEST CERTIFICATES SUBMITTED TO THE OWNER OR ENGINEER IF REQUESTED.
 - SHIPPING - THE SUPPLIER SHALL ARRANGE FOR THE DELIVERY OF EQUIPMENT AND MATERIALS TO THE CONSTRUCTION SITE. THE CONTRACTOR SHALL HAVE RESPONSIBILITY FOR UNLOADING AND STORING THE SUPPLIED EQUIPMENT.
 - FINAL TESTING - THE INSTALLED EQUIPMENT SHALL BE TESTED AS REQUIRED BY THE OWNER BEFORE FINAL ACCEPTANCE. TESTING SHALL BE PERFORMED IN ACCORDANCE WITH THE SUPPLIER'S INSTALLATION PROCEDURES AND SHALL INCLUDE ALL RELEVANT COMPONENTS OF EQUIPMENT.
 - TESTS - UPON COMPLETION OF THE WORK, THE SYSTEMS SHALL BE TESTED BY THE SUPPLIER'S REPRESENTATIVE TO DEMONSTRATE THAT ALL EQUIPMENT IS FUNCTIONING SATISFACTORILY IN THE MANNER REQUIRED.
 - INSTALLATION AS PER SUPPLIER SPECIFICATION. INSTALLATION BY BOLTING TO FLANGE MATCHING AS (MEANS) B16.5 CLASS 150 OR THREAD CONNECTED TO PIPELINE OR VALVE AS OTHERWISE SPECIFIED ON DESIGN DRAWINGS.
 - WATER MAY INCLUDE MINOR QUANTITIES OF SUSPENDED SILTS OR SANDS AND SLIGHT OR NEUTRAL BUOYANCY DEBRIS. SUPPLIERS MAY INCLUDE LARGE QUANTITIES OF SUSPENDED SILTS OR SANDS, BED LOADS IN PIPE INVERT AND FLOATING OR NEUTRAL BUOYANCY DEBRIS.
- PIPE MATERIAL
 - HOPE PIPE MATERIALS SHALL BE IN ACCORDANCE WITH ASTM D3500, ASTM F714, ASTM F7206 AND ASTM F7019.
 - STEEL PIPE MATERIALS SHALL BE IN ACCORDANCE WITH ASTM A33 OR EQUIVALENT.
- LENGTH
 - PIPELINE LENGTHS ARE ENGINEERS ESTIMATES ONLY. ACTUAL LENGTH SHALL BE MEASURED ON SITE
- HOPE - PIPE AND FITTINGS
 - INSTALLATION OF HOPE PIPE SHALL MEET AWMA M52 REQUIREMENTS.
 - THE OUT OF ROUNDNESS OF PIPE ENDS SHALL BE CONSISTENT WITH THE DIAMETER AND WALL THICKNESS OF THE PIPE SUPPLIED AND THE TYPE OF JOINT. ANY OUT OF ROUNDNESS SHALL BE LIMITED TO A SMOOTH OVAL THAT MAY BE JACKED BACK IN A CIRCULAR SHAPE.
 - HOPE PIPE DIMENSION AND WORKMANSHIP FOR PIPE AND FITTINGS SHALL BE IN ACCORDANCE WITH ASTM F714.
 - JOINED HOPE PIPE FOR BUTT JOINT FUSION SHALL BE ACCURATELY ALIGNED AND RETAINED IN POSITION DURING THE WELDING OPERATION. THE JOINED PIPE SHALL NOT BE MISALIGNED BY MORE THAN +4.3 mm.

- THE PIPE AND SITE JOINING OF THE PIPE SHALL PROCEED IN A MANNER AIMED TO CONTROL THE TEMPERATURE OF THE PIPE.
- ALL HOPE JOINING SHALL BE BUTT FUSION AS PER ASTM F2620 UNLESS NOTED OTHERWISE.
- ALL HOPE FITTINGS TO BE OF THE SAME POLYETHYLENE RESIN AS THE JOINED PIPE.
- THE DIMENSION RATIO (DR) OF THE FITTING SHALL BE THE MINIMUM REQUIRED.
- PERFORATIONS TO BE CIRCULAR AND ARRANGED IN ROWS PARALLEL TO THE AXIS OF THE PIPE.
- PERFORATIONS ROWS TO BE ARRANGED IN TWO EQUAL GROUPS PLACED SYMMETRICALLY ON EITHER SIDE OF THE LOWER HALF OF THE PIPE.
- MINIMUM NUMBER OF ROWS OF PERFORATIONS TO BE 4 ROWS.
- PERFORATION HOLE DIAMETER TO BE AT MINIMUM 10 mm AND AT MAXIMUM 15 mm.
- PERFORATION ROWS TO BE ARRANGED IN EITHER STAGGERED OR STRAIGHT ROWS WITH A LONGITUDINAL HOLE SPACING OF 150 mm.

FLANGED JOINTS

- USE GASKETS FOR ALL FLANGED JOINTS UNLESS OTHERWISE SHOWN ON THE DRAWINGS OR REQUIRED BY THE ENGINEER. CENTRE GASKETS ACCURATELY IN THE JOINT.
- LUBRICATE BOLTS, STUDS AND NUTS WITH FLANGE BOLT LUBRICANT SO THAT THE NUTS CAN BE RUN UP BY HAND. TAKE CARE TO PREVENT EXCESSIVE INITIAL TIGHTENING OF BOLTS AND STUDS AND TO ENSURE THAT TENSION IS APPLIED UNIFORMLY.
- REMOVE EXCESSIVE PREVENTIVE COMPOUND APPLIED TO THE FACES OF FLANGES BEFORE SHIPMENT PRIOR TO INSTALLATION. DO NOT USE ACID OR TOOLS THAT MAY DAMAGE FINISHED SURFACES FOR CLEANING FLANGES.

- COATING AND LINING OF CARBON STEEL APPURTENANCES
 - ALL STEEL PIPE, FLANGES, ETC. TO BE FINISHED WITH POLYURETHANE LININGS AND COATINGS, 625 um (25 MILS) DRY FILM THICKNESS (DFT), IN ACCORDANCE WITH AWMA C222. WITH SSPC SP10 SURFACE PREPARATION FOR 75 um PROFILE

VALVES

- THE PRESSURE CLASS RATING OF ALL VALVES IS THE MINIMUM REQUIRED.
- GATE VALVE
 - GATE VALVES ARE TO BE PERMANENTLY INSTALLED AT PIPE JOINTS TO ALL RAPID DECELERATION BASINS (RBS). THE VALVES ARE TO BE FLANGE CONNECTED. THE VALVES MAY BE CLOSED TO ISOLATE INDIVIDUAL RBS.
 - MAXIMUM OPERATING PRESSURE: 120 psi
 - VALVE TYPE: GATE
 - ACTUATION: HAND/REEL OPERATED VISUAL POSITION INDICATOR
 - MATERIALS OF CONSTRUCTION
 - BODY: A214WCB
 - SEAT: A10
 - STEM: 13C8
 - WAKE MODEL (OR SIMILAR): BERG DAMS CAST CARBON STEEL GATE VALVE CLASS 150

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TECHNICAL NOTES

REVISION	NO.	DESCRIPTION
1	G0006	VA101-457/33

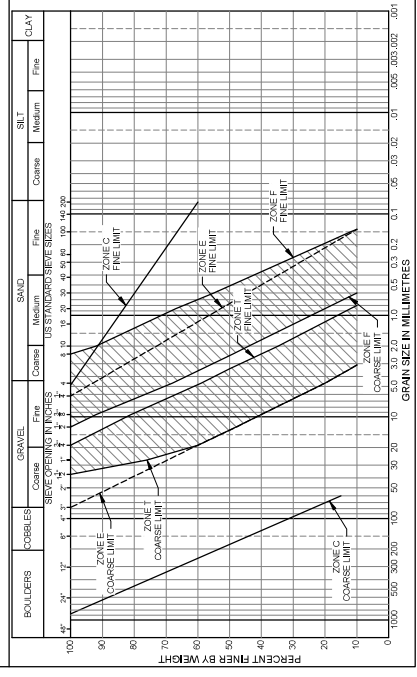
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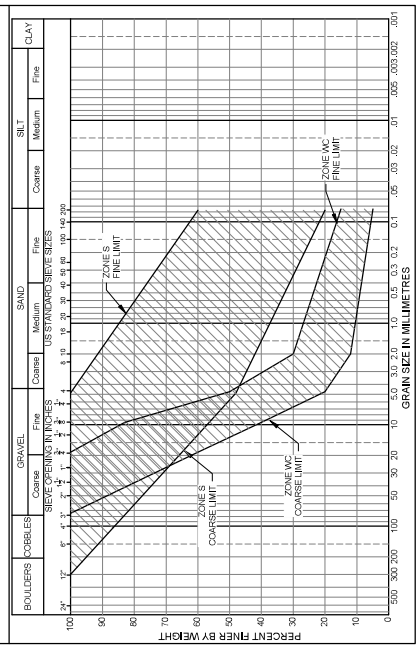
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0	29/07/21	ISSUED FOR PERMITTING	DNF

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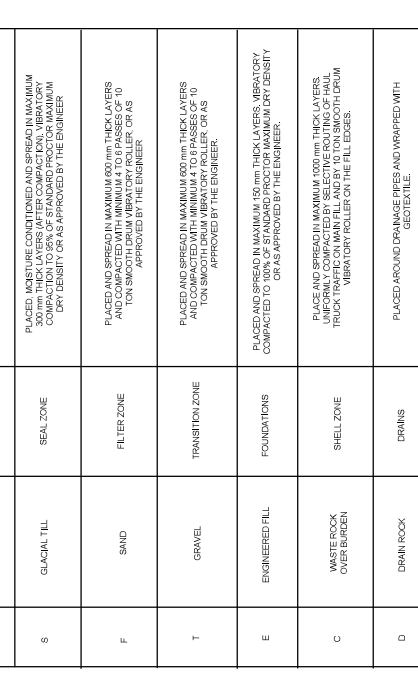
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ZONE - F.T.T.C



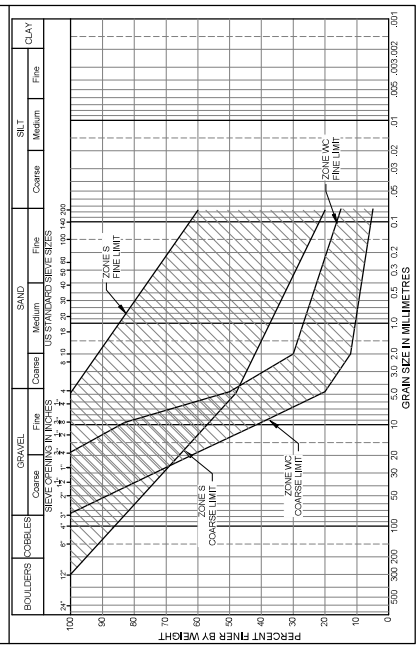
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ZONE - S.W.C



UNIFIED SOIL CLASSIFICATION SYSTEM
ZONE - D.R.B



UNIFIED SOIL CLASSIFICATION SYSTEM
ZONE - F.T.T.C



UNIFIED SOIL CLASSIFICATION SYSTEM
ZONE - F.T.T.C



NOTES:

- FOR GENERAL NOTES SEE DRAWING G008.
- RIPRAP TO BE HARD, DENSE AND DURABLE TO WITHSTAND LONG EXPOSURE TO WEATHERING.
- RIPRAP STONES SHALL BE ANGULAR IN SHAPE, NO STONE SHALL EXCEED A LENGTH TO BREADTH OR THICKNESS OF 3.
- SELECTED BC MINISTRY OF TRANSPORTATION RIPRAP CLASS AND DIMENSIONS SHOWN IN TABLE 1 AND TABLE 2.
- SEE PROJECT TECHNICAL SPECIFICATIONS FOR ADDITIONAL MATERIAL REQUIREMENTS.

GRADATION OF ROCK SIZES IN EACH CLASS OF RIPRAP

CLASS OF RIPRAP (kg)	D50 (mm)	ROCK GRADATION PERCENTAGE SMALLER THAN GIVEN ROCK MASS (kg)		
		15%	50%	85%
5	150	0.5	5	15
10	200	1	10	30
50	300	5	50	150
250	565	25	250	750
1000	900	100	1000	3000
2000	1130	200	2000	6000

APPROXIMATE AVERAGE DIMENSION OF EACH SPECIFIED ROCK CLASS MASS (mm) (SG = 2.64)

CLASS OF RIPRAP (kg)	D50 (mm)	APPROXIMATE AVERAGE DIMENSION (mm)		
		15%	50%	85%
5	150	70	150	215
10	200	90	200	285
50	300	155	300	475
250	565	260	565	815
1000	900	475	900	1285
2000	1130	525	1130	1630

MATERIAL PLACEMENT AND COMPACTION REQUIREMENTS

ZONE	MATERIAL TYPE	LOCATIONS	PLACING AND COMPACTION REQUIREMENTS
S	GLACIAL TILL	SEAL ZONE	PLACE AND SPREAD IN MAXIMUM 150mm THICK LAYERS AND COMPACTED WITH MINIMUM 4 TO 8 PASSES OF 10 TON SMOOTH DRUM VIBRATORY ROLLER OR AS APPROVED BY THE ENGINEER.
F	SAND	FILTER ZONE	PLACED AND SPREAD IN MAXIMUM 150mm THICK LAYERS AND COMPACTED WITH MINIMUM 4 TO 8 PASSES OF 10 TON SMOOTH DRUM VIBRATORY ROLLER OR AS APPROVED BY THE ENGINEER.
T	GRAVEL	TRANSITION ZONE	PLACED AND SPREAD IN MAXIMUM 150mm THICK LAYERS AND COMPACTED WITH MINIMUM 4 TO 8 PASSES OF 10 TON SMOOTH DRUM VIBRATORY ROLLER OR AS APPROVED BY THE ENGINEER.
E	ENGINEERED FILL	FOUNDATIONS	PLACED AND SPREAD IN MAXIMUM 150mm THICK LAYERS, VIBRATORY COMPACTED TO 95% OF STANDARD PROCTOR MAXIMUM DRY DENSITY OR AS APPROVED BY THE ENGINEER.
C	WASTE ROCK OVER BURDEN	SHELL ZONE	PLACE AND SPREAD IN MAXIMUM 150mm THICK LAYERS, UNIFORMLY COMPACTED BY SELECTIVE ROUTING OF HAUL TRUCK TRAFFIC ON MAIN FILL AND BY 10 TON SMOOTH DRUM VIBRATORY ROLLER ON THE FILL BODIES.
D	DRAIN ROCK	DRAINS	PLACED AROUND DRAINAGE PIPES AND WRAPPED WITH GEOTEXTILE.
R	RIPRAP	RIPRAP	PLACED WITH EXCAVATOR BUCKET IN INTERLOCKING PATTERN WITH MINIMAL COMPACTIVE TENTION.
RB	RIPRAP BEDDING	RIPRAP	PLACE AND SPREAD IN MAXIMUM 150mm THICK LAYERS, UNIFORMLY COMPACTED BY BUCKET TAPPING.
WC	WEARING COURSE	ROADS	PLACE AND SPREAD IN MAXIMUM 150mm THICK LAYERS, EACH LAYER SHALL BE COMPACTED BY A MINIMUM OF 4 PASSES OVER THE ENTIRE SURFACE WITH 10 TON SMOOTH DRUM VIBRATORY ROLLER.

REVISIONS

NO.	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED	REV	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED
1	26/04/22	ISSUED FOR CONSTRUCTION	CEN	SKC	DOE	DOE	DOE						
0	29/07/21	ISSUED FOR PERMITTING	CEN	SKC	DOE	DOE	DOE						

REFERENCE DRAWINGS

GROUP	TECHNICAL NOTES	DESCRIPTION
G008		
G009		

REVISIONS

NO.	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED	REV	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED
1	26/04/22	ISSUED FOR CONSTRUCTION	CEN	SKC	DOE	DOE	DOE						
0	29/07/21	ISSUED FOR PERMITTING	CEN	SKC	DOE	DOE	DOE						

ISSUED FOR CONSTRUCTION

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BLACKWATER GOLD PROJECT

CONSTRUCTION MATERIAL GRADATIONS

Original signed by: **C. B. NIAMIR**

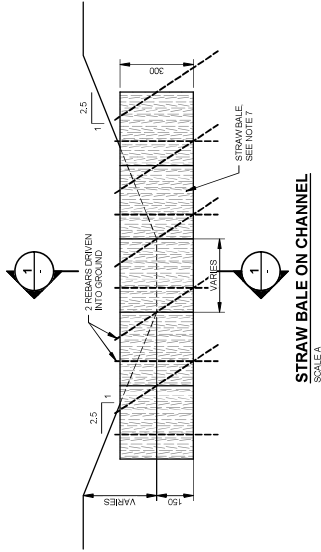
REVISIONS: **VA101-457/33**
DRAWING NO: **G0040**

ISSUED FOR CONSTRUCTION

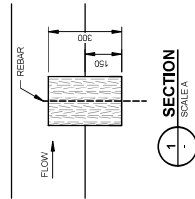
APPENDIX B

Sediment and Erosion Control BMP Figures

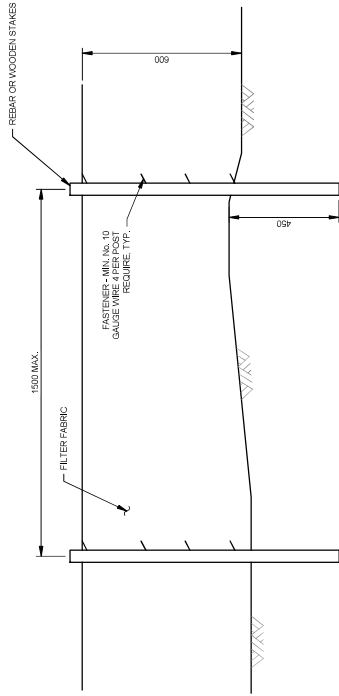
(Figures 1B to 2B)



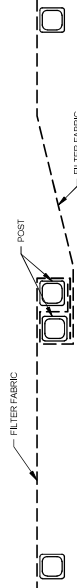
STRAW BALE ON CHANNEL
SCALE A



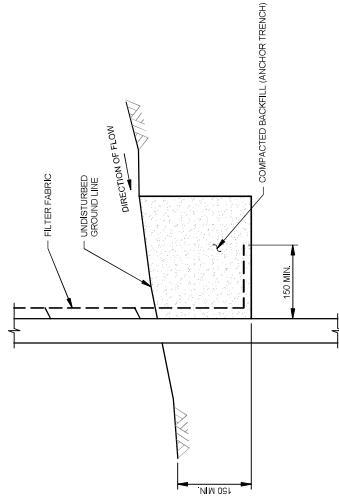
SECTION
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SILT FENCING PROFILE
SCALE A



SILT FENCES ATTACHMENT
SCALE B



SILT FENCING - CROSS SECTION
SCALE B

- NOTES :**
1. ALL DIMENSIONS ARE IN MILLIMETRES UNLESS NOTED OTHERWISE.
 2. BEST MANAGEMENT PRACTICES (BMP) FOR SEDIMENT AND EROSION CONTROL SHALL INCLUDE THE DESIGN, CONSTRUCTION AND OPERATION OF COLLECTION CHANNELS AND SEDIMENT CONTROL POND.
 3. FOUNDATION PREPARATION SHALL CONSIST OF REMOVAL OF VEGETATION, MUD, DEBRIS, AND SOFT AND DELETERIOUS MATERIAL.
 4. ALL SEDIMENT AND EROSION CONTROL MEASURES MUST BE CONSTRUCTED, STABILIZED AND FUNCTIONAL BEFORE SITE DISTURBANCE BEGINS.
 5. SITE GRADING SURFACE WATER RUNOFF TO BE DIRECTED TO THE COLLECTION CHANNELS AT ALL TIMES DURING SITE DISTURBANCE ACTIVITIES UNTIL FINAL STABILIZATION IS ACHIEVED.
 6. THE CONTRACTOR SHALL INSPECT ALL EROSION CONTROL MEASURES PERIODICALLY TO ENSURE THEY ARE MAINTAINED AND REPAIRS OR NECESSARY REPAIRS OR CLEANUP TO MAINTAIN THE EFFECTIVENESS OF THE EROSION CONTROL DEVICES SHALL BE MADE IMMEDIATELY.
 7. STRAW BALE SHALL BE IMPLEMENTED ON COLLECTION CHANNELS WHEN REQUIRED BY THE CONTRACTOR. TYPE OF CHANNELS MAY INCLUDE CHANNELS WITH STRAW BALE, CHANNEL THROUGH, ACCESS TROUGH, PERMANENT AND TEMPORARY CHANNELS.

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EROSION AND SEDIMENT CONTROL
TYPICAL SECTIONS AND DETAILS
SHEET 1 OF 2

REV. NO. 1
DATE 15/01/2022

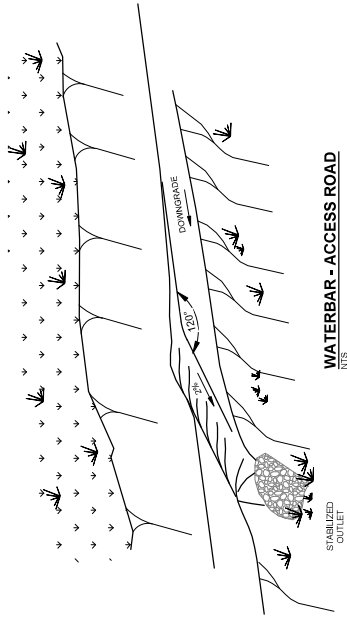
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DATE 15/01/2022

DESIGNED BY
CHECKED BY
DRAWN BY
REVISIONS

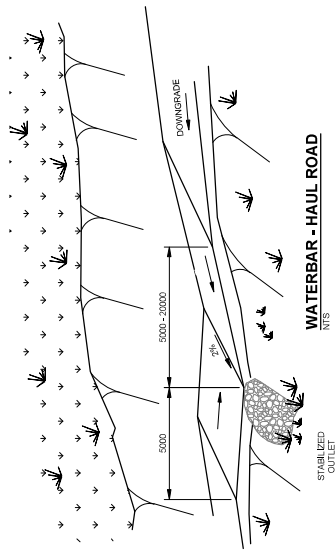
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DRAWING NO. VAI20-0058
SHEET NO. 01

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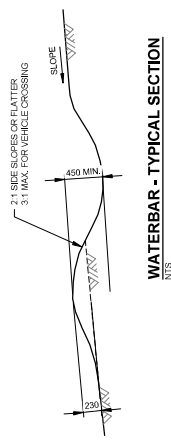
FIGURE 1B



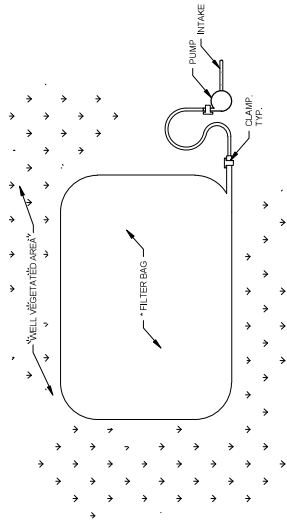
WATERBAR - ACCESS ROAD
NTS



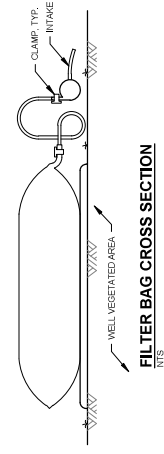
WATERBAR - HAUL ROAD
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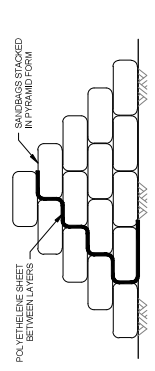
WATERBAR - TYPICAL SECTION
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FILTER BAG PLAN
NTS



FILTER BAG CROSS SECTION
NTS



TEMPORARY STREAM DIVERSION STRUCTURE
NTS

- NOTES:**
1. ALL SEDIMENT AND EROSION CONTROL MEASURES MUST BE CONSTRUCTED, STABILIZED AND FUNCTIONAL BEFORE SITE DISTURBANCE BEGINS.
 2. SURFACE WATER RUNOFF TO BE DIRECTED TO THE EROSION CONTROL STRUCTURE. THE DISTURBANCE ACTIVITIES UNTIL FINAL STABILIZATION IS ACHIEVED.
 3. THE CONTRACTOR SHALL INSPECT ALL EROSION CONTROL RIMS PERIODICALLY AND AFTER EACH RAINFALL-FOLLOWING RAINFALL EVENT. ANY DEFICIENCIES MUST BE IMMEDIATELY REPORTED TO THE EROSION CONTROL SPECIALIST TO BE MADE IMMEDIATELY.
 4. SAND BAGS SHOULD BE CHECKED FOR DEGRADATION WHEN IT HAS A MINIMUM UNIFORM 70% VEGETATIVE COVER OR OTHER PERMANENT NON-WEBER TIME COVER TO RESIST ACCELERATED SURFACE EROSION.
 5. DIVERSION STRUCTURE TO CONSIST OF SANDBAGS OR LUSHED METAL PLATE.

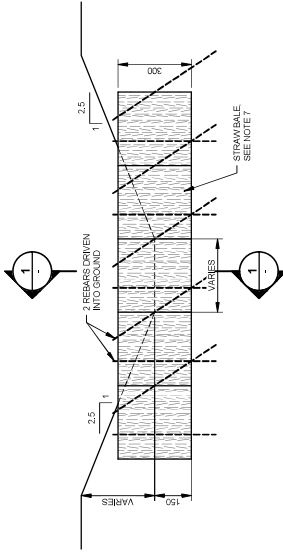
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EROSION AND SEDIMENT CONTROL	
TYPICAL SECTIONS AND DETAILS	
SHEET 2 OF 2	
DATE: 14/10/2022	ISSUED WITH MEMO
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PROJECT NO: VAD10-4517/36	ISSUE NO: 0
PROJECT ADDRESS: VAD10-4517/36	FIGURE NO: 2B

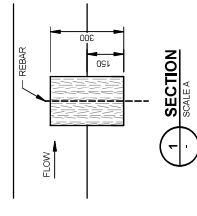
APPENDIX C

Drawings

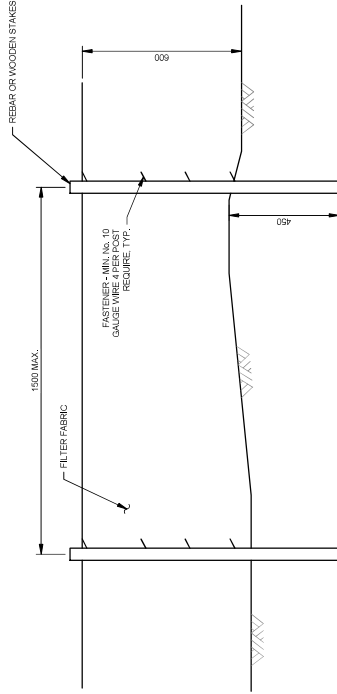
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C3802 Detailed Design – Not for Construction
C3803 Detailed Design – Not for Construction



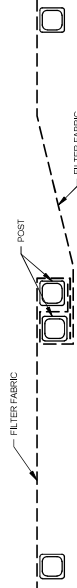
STRAW BALE ON CHANNEL
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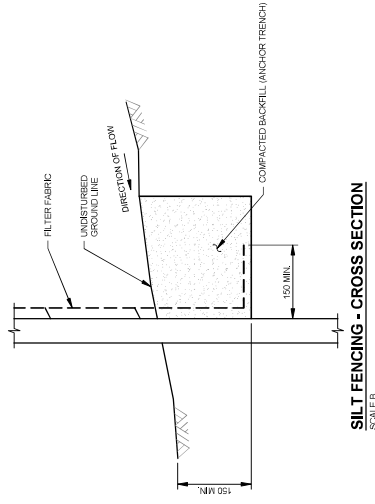
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SILT FENCING PROFILE
SCALE A



SILT FENCES ATTACHMENT
SCALE B

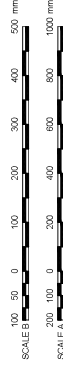


SILT FENCING - CROSS SECTION
SCALE B

NOTES :

1. ALL DIMENSIONS ARE IN MILLIMETRES UNLESS NOTED OTHERWISE.
2. BEST MANAGEMENT PRACTICES (BMP) FOR SEDIMENT AND EROSION CONTROL WILL BE APPLIED DURING CONSTRUCTION AND OPERATION OF COLLECTION CHANNELS AND SEDIMENT CONTROL POND.
3. FOUNDATION PREPARATION SHALL CONSIST OF REMOVAL OF VEGETATION, MUD, DEBRIS, AND SOFT AND DELICIOUS MATERIAL.
4. SEDIMENT AND EROSION CONTROL MEASURES MUST BE CONSTRUCTED AS SHOWN AND SHALL BE MAINTAINED THROUGHOUT CONSTRUCTION.
5. SITE EROSION CONTROL CHANNELS SHALL BE CONSTRUCTED AND STABILIZATION SHALL BE ACHIEVED.
6. THE CONTRACTOR SHALL INSPECT ALL EROSION CONTROL MEASURES PERIODICALLY AND AFTER EACH RAINFALL EVENT. ANY EROSION CONTROL DEVICES SHALL BE MADE IMMEDIATELY.
7. STRAWBALE SHALL BE IMPLEMENTED ON COLLECTION CHANNELS WHEN REQUIRED BY THE CONTRACTOR. TYPE OF CHANNELS MAY INCLUDE PERMANENT CHANNELS, ACCESS ROAD, CONTACT RUNOFF, ACCESS ROAD, PERMANENT AND TEMPORARY CHANNELS.

**DETAILED DESIGN
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CONSULTING**

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BLACKWATER GOLD PROJECT

**EROSION AND SEDIMENT CONTROL
TYPICAL SECTIONS AND DETAILS
SHEET 1**

REVISION
C3801
DRAWING NO.
VA101-457/33
PROJECT NO.

NO.	DATE	DESCRIPTION	BY	APPROVED	REVISIONS
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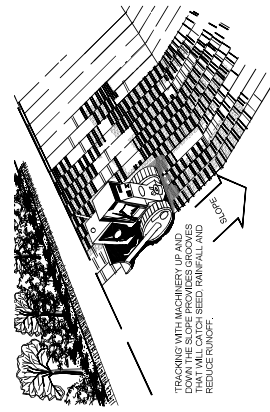
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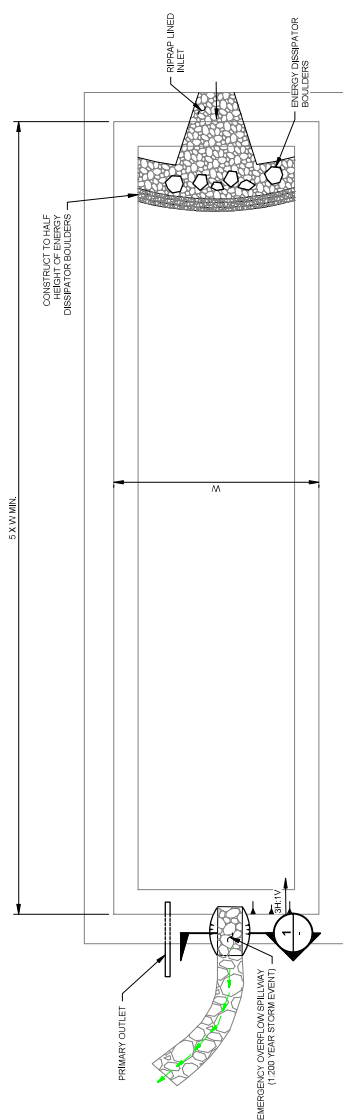
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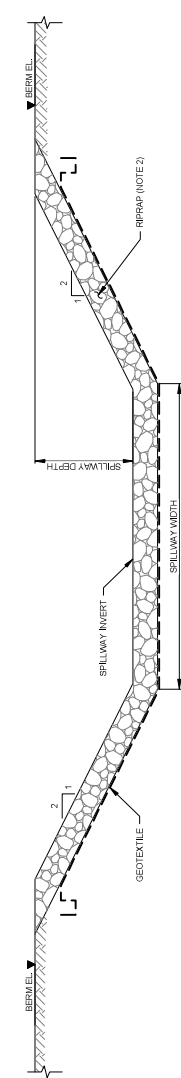
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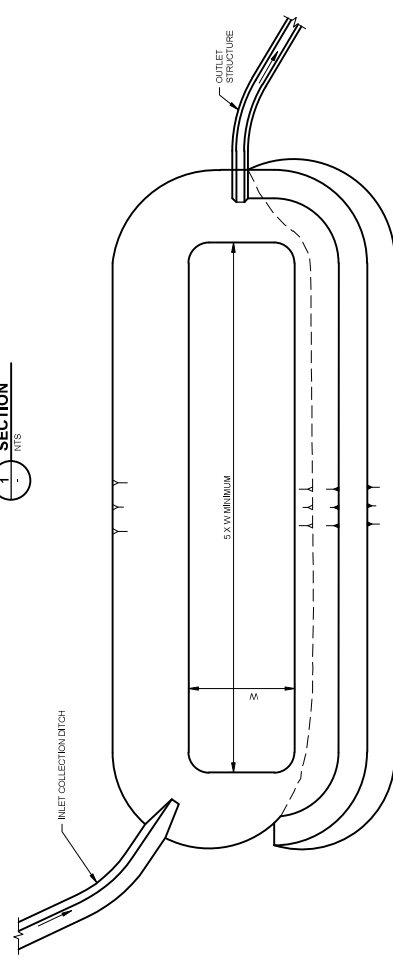
SLOPE ROUGHENING
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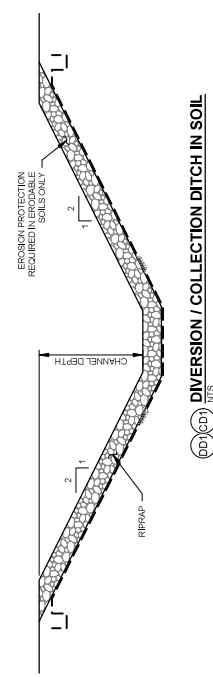
SP SEDIMENT POND
PLAN VIEW
SCALE: A



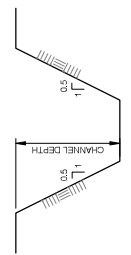
1 SECTION
NTS



SB SEDIMENT BASIN PLAN
NTS



DD DIVERSION / COLLECTION DITCH IN SOIL
NTS



DD DIVERSION / COLLECTION DITCH IN ROCK
NTS

- NOTES:**
1. SEDIMENT POND LINING REQUIREMENTS SUBJECT TO ENGINEERS REVIEW OF FOUNDATION MATERIAL.
 2. RIPRAP TO BE SPECIFIED FOR EACH INDIVIDUAL SEDIMENT POND DURING DETAILED DESIGN PHASE.
 3. DIMENSIONS AND ELEVATIONS ARE IN METRES UNLESS OTHERWISE NOTED.

**DETAILED DESIGN
NOT FOR CONSTRUCTION**

SCALE: 1:1000 0 10000 20000 30000 40000 50000mm

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BLACKWATER GOLD PROJECT
EROSION AND SEDIMENT CONTROL
TYPICAL SECTIONS AND DETAILS
SHEET 3

PROJECT NO.	VA101-457/33	REVISION NO.	0
DATE		REVISION DESCRIPTION	

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NO.	DATE	DESCRIPTION	DESIGNED	DRAWN	REVIEWED	APPROVED	REV	DATE	ISSUED FOR PERMITTING	REVISIONS
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4041-04-04